

Project Method for 2010 Wind Integration Cost Study

Introduction

Traditionally, load and generation are balanced using dynamic operations in a straightforward manner – load is uncontrollable and variable, and generation is dispatched subject to its dispatch limitation (be it hydro, thermal, or other sources) to match variable load. The integration of significant amount of non-dispatchable wind generation has introduced a new variable to the operation of the existing power systems.

The total installed capacity of wind generation in PacifiCorp’s balancing authority areas (east and west) in 2000 was 33 MW. As of April 2010, there is approximately 1,400 MW, or roughly 10% of the total installed capacity on the system. By 2017, it could be more than 2,200 MW. Given the growth of wind in PacifiCorp’s portfolio, it is increasingly important to understand its impact on the overall operations of the system. While there are costs and operational challenges associated with large scale wind penetration, there are also benefits, which would include a cleaner energy resource mix and fuel diversification for customers.

To understand the costs of integrating wind, this paper contemplates the analysis and valuation of operational changes required to manage variable wind generation at different levels of penetration while maintaining reliability. The approach outlined herein will be used to estimate the amount of Operating Reserves (power generation plants operating on less than full or variable capacity with flexible output capabilities) needed to manage fluctuations in load and fluctuations in wind within PacifiCorp’s balancing authority areas. The Operating Reserves discussed here are limited to Spinning Reserves and Non-Spinning Reserves; and the flexible services provided are broken into Regulation, Load Following, and Contingency. For purposes of this paper, Regulation refers to variability of load and wind generation output managed within ten minute real timeframes, and Load Following represents the variability as measured in hourly real timeframes. Contingency reserves, although mentioned, are supplied in accordance with WECC standards.

Once the amount of Operating Reserves is established for different levels of wind penetration, the cost of holding these reserves on PacifiCorp’s system will be calculated using the Planning and Risk (PaR) model. In addition to using PaR for evaluating Operating Reserve costs, the PaR model will also be used to estimate wind integration costs associated with day-to-day rebalancing of the system. These system balancing costs result from the unpredictable nature of

wind generation on a day-ahead basis and can be characterized as system costs born from committing generation resources against a forecast of load and wind generation and then dispatching generation resources under actual load and wind conditions. These services are compared to the Wind Integration Cost terms in the 2008 Integrated Resource Plan update in Table 1:

Table 1. Index of new Wind Integration Cost components to components previously published in the PacifiCorp 2008 IRP, Appendix F.

2008 IRP Description	Methodology Description
Day Ahead Forecast Variaton	System Balancing
Hour Ahead Forecast Variaton	
Actual Forecast Variation	Load Following
Regulate Up	Regulation
Regulate Down	

Method

In analyzing the effect of wind generation on PacifiCorp’s system operations in the east and west balancing authority areas, the analysis team has two key objectives:

- Beginning with wind generation and load data, apply current power system operational practice to develop a methodology for estimating how wind generation would affect the need for incremental physical Operating Reserves for PacifiCorp’s system under a set of wind capacity penetration scenarios.
- Use existing production cost models to isolate the cost of holding incremental Operating Reserves and to establish costs for system balancing created by day-ahead forecast errors associated with load and wind generation.

The first objective focuses on the alteration of the physical Operating Reserves position estimated in ten-minute and hourly timeframes, and will be calculated seasonally for application in the production cost simulations. The second objective represents the key stage of the analysis, for it will not only evaluate the cost of the marginal reserves position established to manage the wind position in real time, it will also assess costs resulting from wind variability in the day-ahead timeframe. In other words, each hour features a need to set aside increased Operating Reserves (both spinning and non-spinning reserves), in addition to those set aside explicitly to cover load and contingency events which are inherent to the PacifiCorp system with or without wind. The cost to hold additional hourly operating reserves can be calculated in the production cost simulation, as can the system cost of day-to-day rebalancing induced by the unpredictable nature of wind generation on a day-ahead basis. Estimation of such rebalancing costs will be



achieved by allowing the PaR model to establish unit commitment choices under a forecast of wind, while being faced with dispatch decisions against actual system conditions. In aggregate, the cost of holding reserves and the cost of rebalancing will produce an estimate of the wind integration costs specific to PacifiCorp’s system.

Calculating Incremental Operating Reserve Requirements

PacifiCorp makes the calculation for existing Operating Reserve requirements starting with load and production data for the 2007-2009 period (the Initial Term), as represented by Figure 1. Both the load and generation data are available on ten-minute intervals for the Initial Term. PacifiCorp chose to use this data because it represented the best base of observed data available within the company, which includes significant concurrent load and wind generation data, and includes more than just one year’s variation of weather and other affective variables on load.

Figure 1. Historical production and load data available to PacifiCorp Wind Integration study.

	Plant name	Size, MW	Data to be Developed															
			2007				2008				2009				2010			
Timeline			Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4
Wind	Foote Creek	45	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Stateline*	175	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Combine Hills	41	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Leaning Juniper	99	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Wolverine Creek	64.5	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Marengo	140	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Goodnoe Hills	94	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Marengo II	70.2	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Mountain Wind I	60.9	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Spanish Fork	19	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Mountain Wind II	79.8	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Rolling Hills	99	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Glenrock	99	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Glenrock III	39	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Seven Mile Hill	99	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Seven Mile Hill II	20	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	High Plains	99	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	McFadden Ridge I	28.5	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Three Buttes	99	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	Dunlap I	111	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
Rock River	50	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	
Composite of Small Projects	81	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	
Top of the World	201.5	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	
Load	PACW Load		■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■
	PACE Load		■	■	■	■	■	■	■	■	■	■	■	■	■	■	■	■

Key
 = Internal fine resolution data (10-min, 1-hour)
 = Data to be developed by technical advisor
 * Capacity represents portion of the plant occurring in PAC Control area.

The figure also contemplates the unavailability of certain wind data germane to the study. PacifiCorp desires to use as much real, observed, concurrent data as possible, owing to the very unpredictable nature of wind generation output as well as the many fine variations available in real load data not always found in simulated data. As a result, the technical advisor procured by PacifiCorp to assist with the study, The Brattle Group, will fill in the missing wind data pertaining to the Initial Term by using statistical methods and simulating the needed wind data where historical observed data is unavailable or insufficient. The Brattle Group is currently developing the specific methodology necessary to derive the statistical parameters that describe the wind variability from the available wind data and through those statistical parameters, simulate the missing wind data.

Broadly, the missing wind data can be segmented into two groups. The first group consists of wind sites for which partial data is available and the second group consists of wind sites for which no historical data is available. Based on the map of the wind farms locations in the PacifiCorp's service areas,¹ it appears (and we assume) that in both the PacifiCorp's East and West control areas, at least one or more wind sites is located in close proximity to sites with partial or no historical wind data.

In the discussion to follow, W_{pd} refers to a wind site with incomplete/partial data available, W_{fd} refers to a wind site with full data availability, and, W_{nd} refers to a wind site with no historical data available.

To simulate the wind data for sites W_{pd} (partial historical data available), Brattle proposes to perform the following steps: First, *Brattle* estimates an econometric model that quantifies the relationship between data from a W_{fd} wind site and data from a nearby W_{pd} site. Effectively, the data from W_{fd} would be used as a predictor of the W_{pd} , or the site with partially-available historical data while preserving the temporal relationship between the two data sets and controlling for various measures of seasonality (time of day, season of year, etc.).

Second, Brattle would use the resulting estimated coefficients in the regression model to apply to the remaining data from W_{fd} to simulate values for W_{pd} over the missing period. Since those predicted values for W_{pd} will be estimates of the mean values, an addition of stochastic noise will

¹ Map provided available at: http://www.pacificorp.com/content/dam/pacificorp/doc/Energy_Sources/12-35_PC_RenewableEnergyFlyer.pdf

be used to augment the simulated wind generation values. Using the augmented predicted values, the regression will be estimated again over the full period, resulting in a new set of regression coefficient estimates. This full regression estimation process will be repeated until there is a convergence in the regression estimates. This approach is a simplified version of the Expectation Maximization (EM) algorithm. The specification of the regression model would need to be developed through an exploratory process of the available data set. It is likely that the model will be a variation of a distributed lag specification to represent the dynamics of wind generation.

Third, a simulated profile will be generated for the missing period, which, in addition to the partially available actual data, will result in a complete wind profile over the time period of interest for a W_{pd} site.

To simulate the wind data for sites where no historical data is available, Brattle will rely on existing data for a nearby site W_{fd} . Given the increased complexity of this task (compared to filling a partially available data set), the general approach described here might require adjustments, particularly by supplementing the econometric assumptions and techniques to reach converging results. The approach proposed for simulating wind data where no historical data is available assumes that once we establish a relationship between two full profiles that are part of two groups of wind sites located in two distinct areas, the relationship is representative for corresponding pairs of wind sites from those two geographic groups.

The steps would involve the following: If an area **A** has at least one wind site with full dataset (W_{fd_areaA}) located in proximity to the site with no historical data (W_{nd_areaA}), we would estimate a regression model using (W_{fd_areaA}) as a dependent variable. The explanatory/independent variables in this regression would come from the distributed lags of another full data wind site in a different area, **B**, (W_{fd_areaB1}). Having obtained the estimated regression coefficients, we would apply those coefficients to data from a third wind site that has a full data span and is also located in area **B** (W_{fd_areaB2}) to estimate data for output from W_{nd_areaA} . Then, a properly distributed stochastic noise would be added to simulate the wind data for W_{nd_areaA} . W_{fd_areaB2} could be a wind site that had a pre-existing full data set available or a site with partial data set for which we previously had estimated a full-period wind profile (as outlined in the EM algorithm approach above).

For those wind generation sites where there is no data available in the Initial Term, the Brattle

Group will generate the missing data by using production estimates generated in the project review to seed the back-simulation.

Once a dense data set is created, the interval data drives the calculation of the marginal reserves requirement in two components; *Regulation*, which is developed using the ten-minute interval data, and *Load Following*, which is calculated using the same data but estimated using the hourly variability.

Regulation and Load Following

The approach for calculating incremental Operating Reserves necessary to supply adequate capacity for regulation and load following at levels required to maintain current control performance was based on merging current operational practice with a survey of papers on wind integration, as well as advisory from the Brattle Group. PacifiCorp will employ Initial Term (2007-09, inclusive) load data as the baseline case (zero wind generation) in each scenario. Coincident wind data (as observed, plus that generated by the Brattle Group per Figure 1) will be added in increasing levels of wind penetration capacity to gauge the change in operating reserves demand. For purposes of this study, the Regulation calculation compares observed ten-minute interval load and wind generation production to a ten minute interval estimate, and Load Following compares observed hourly averages to an average forecast. The estimation of Regulation and Load Following reserve capacity requirements, and their combination into a single reserve capacity position may be done seasonally, and is discussed in detail below.

Regulation

With no sub-hourly clearing market, PacifiCorp must meet sub-hourly load (and load net of wind) deviations with system resources. This includes automatic generation control (AGC), demand side management (DSM), and the ramping of flexible generation units in real time operations, which represents a draw on Operating Reserves. Wind variability among ten-minute intervals can represent a quantity of generation required to ramp up or down to maintain system stability. To parse the ten-minute interval variability from the ensuing load following analysis, a persistence forecast of the rolling prior 60 minutes will be used to analyze the variation of each ten minute interval. The actual load in each ten minute interval will be subtracted from the rolling average of the prior 6 ten minute intervals, and the standard deviation will be computed for each seasonal period. This approach follows the one used by the National Renewable Energy

Laboratory (NREL) for its recent “Eastern Wind Integration and Transmission Study”.²

$$\sigma_{wind10min} = \sqrt{\frac{1}{(N-1)} \sum_{i=1}^N \left(Wind_i^\varepsilon - \overline{Wind_i^\varepsilon} \right)^2}$$

Where:

N = number of ten-minute intervals in the “bin” of interest (i.e. season, peak, off-peak, or load state bin)

$Wind_{10-min-forecast}$ = the rolling average of the wind generation in prior 6 ten minute intervals

$Wind_{Actual10min}$ = the observed wind generation for a given ten minute interval

$Wind_i^\varepsilon$ = the wind forecast error defined as ($Wind_{10-min-forecast} - Wind_{Actual10min}$)

$\overline{Wind_i^\varepsilon}$ = the mean of the wind forecast error in the “bin” of interest

Similarly, the load variability is also analyzed with the actual ten-minute interval load being subtracted from the rolling sixty minute average.

$$\sigma_{load10min} = \sqrt{\frac{1}{(N-1)} \sum_{i=1}^N \left(Load_i^\varepsilon - \overline{Load_i^\varepsilon} \right)^2}$$

As the ten minute load and wind errors each represent unpredictable change in the need for dispatchable generation, their variability can be assessed separately and combined. The standard deviation of load net wind generation, which is the basis for the regulating reserve, can be computed assuming fast variations in load are not correlated with changes in aggregate wind generation output:

$$\mathbf{Regulation}_{10min} = \sqrt{\sigma_{Load10min}^2 + \sigma_{Wind10min}^2}$$

Figures 2 and 3 illustrate the difference between observed ten minute interval load and wind data from the rolling average.

² NREL, *Eastern Wind Integration and Transmission Study*, prepared by EnerNex Corporation, (January 10, 2010), p. 143. The report is available for download from the following hyperlink: http://www.nrel.gov/wind/systemsintegration/pdfs/2010/ewits_final_report.pdf

Figure 2. A one-day plot of the rolling 60-minute average ten-minute load estimate plotted against observed system load. The data used for Figure 3 is highlighted.

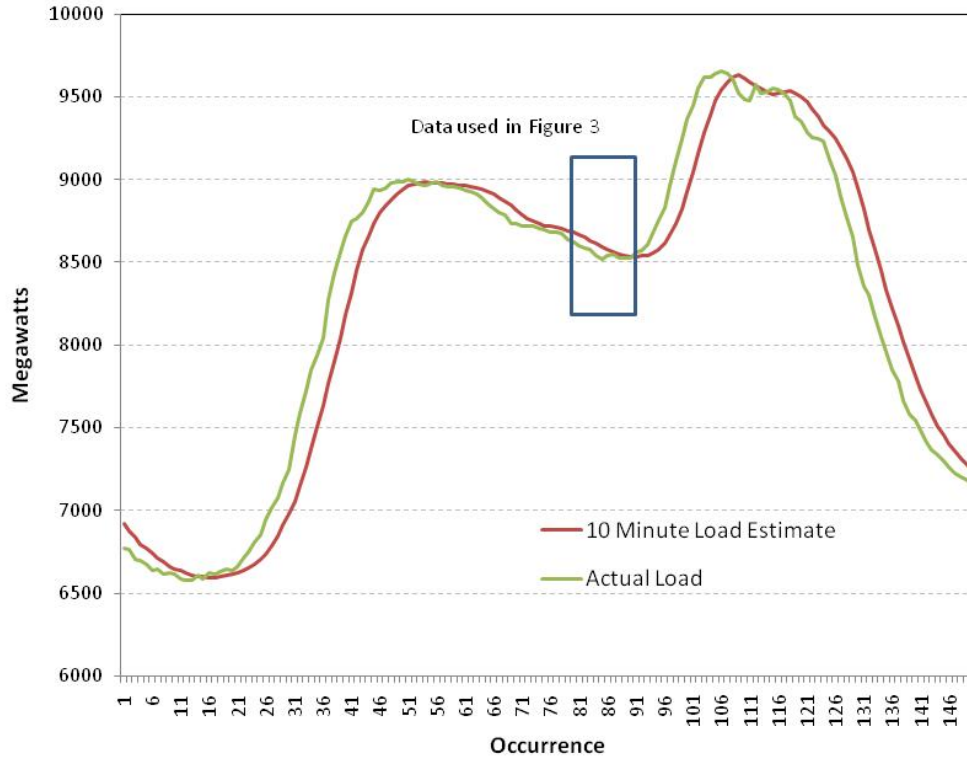
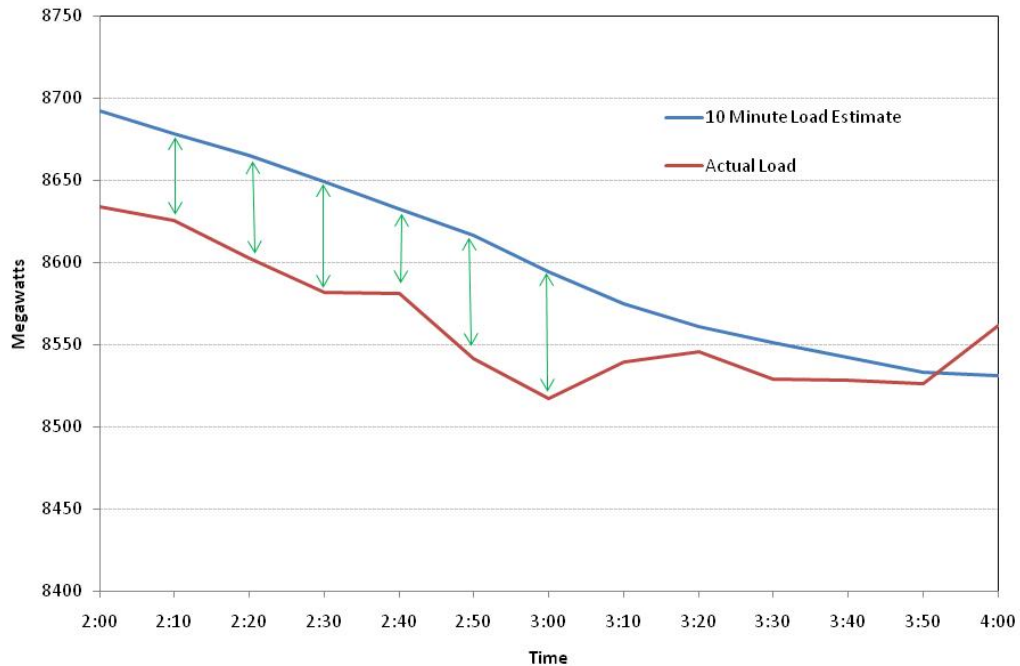
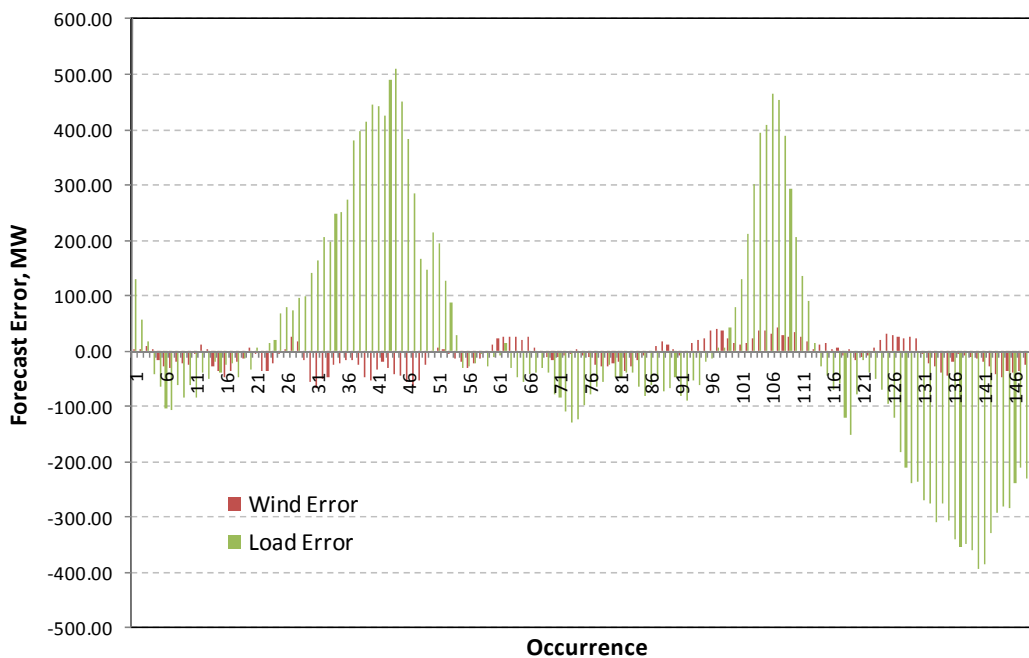


Figure 3. Highlighted data showing variability between ten-minute persistence forecast and observed load. Several example errors between the estimate and actual data are highlighted with green arrows.



A sample of the errors logged for the same period, for load and wind, are shown in Figure 4. The independence of the forecast errors for wind and load, can be assumed. Given that the amount of wind used in the sample data is minimal, wind forecast errors for the sampled time period (and the assumed wind penetration level) is small relative those for load.

Figure 4. Independent forecast errors in short term load and wind generation used to assess the regulation position. The data in this figure comes from December 2008, and so reflects only roughly 6% wind capacity penetration.



Load Following

In addition to the 10-minute interval services provided by Regulation described above, PacifiCorp maintains system balance by optimizing its operations to an hourly forecast with changes in generation and market activity. This planning interval represents hourly changes in generation which are assessed within roughly 20 minutes each hour to account for a bottom-of-the-hour (:30 after) scheduling deadline. Taking into account the conditions of the present and the expected load and wind generation, PacifiCorp must schedule generation to meet demands with an expectation of how much higher or lower system load (net of wind generation) may be.

Hourly Forecasting

PacifiCorp's real-time desk updates the next hours system load forecast forty minutes prior to each operating hour. This forecast is created by comparing the current hour load to the load of a

similar-load-shaped day. The hour-to-hour change in load from the similar day and hours (the load delta) is applied to the current hour load and the sum is used as the forecast for the ensuing hour. For example, on a given Monday the PacifiCorp operator may be forecasting hour to hour changes in system load by referencing the hour to hour changes on the prior Monday, a similar-load-shaped day. If the hour to hour load change between the prior Monday's like hours was 100 MW, the operator will use a 100 MW change in load as the next hour forecast.

While operational short term wind forecasting includes qualitative analysis, the 20th minute persistence forecast is what can be quantitatively modeled at this time, and is a reasonable approximation of operational practice. As modeled here, hourly wind forecasting is done by persistence; applying the instantaneous sample of the wind generation output 20 minutes past the current hour to the next hour as a forecast and balancing the system to that point.

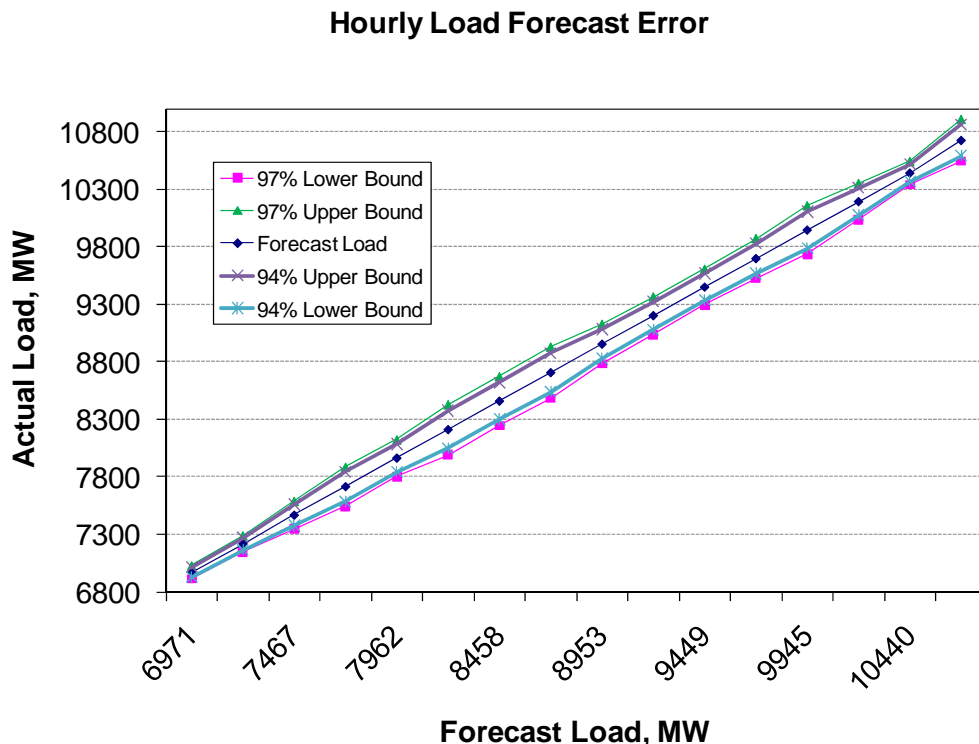
The resulting operational process therefore goes as follows; at the top of the hour, wind generation output, dispatchable generation output, and load values are summarized, and trended using the methods above. The result is compared to the next hour's schedule for gaps as soon as possible, with the generation and load values updated at roughly the 20th minute past the hour. This result is then balanced through a combination of market transactions and scheduling adjustments to PacifiCorp resources to produce a balanced schedule for the ensuing hour, with all transactions having to be complete by the 30th minute past the hour. For purposes of the calculation made in this exercise, the hourly wind forecast will consist of the 20th minute output from the prior hour, and the load forecast will be modeled per the approximation described above with a shaping factor calculated using the day from one week prior, and applying a prior Sunday to shape any NERC holiday schedules.

Analysis

Using the Initial Term data for PacifiCorp's balancing authority areas, a comparison of the load and wind forecasts will be implemented to measure the seasonal or annual trends in the variability between the hourly interval load and wind forecasts and the observed average hourly load and wind generation values. These differences will be culled into bins by load magnitude (or by load magnitude and wind generation magnitude) using load and wind data. An example of load data segmented into bins appears in Figure 5. With probabilities implied by the population of each bin, representing the expected amount of time spent in each load state, as represented by the historical data alone. The percentile equivalent to the historical Control

Performance 2 (CPS2)³ performance of PacifiCorp will be sampled above and below the median of each of the bins. The average CPS2 performance for PacifiCorp’s east and west balancing authority areas is just below 97%. As the goal of this method is to incorporate wind integration in PacifiCorp’s current operations, the CPS2 target of 97% will be emphasized in these calculations. Indicative incremental reserves changes can be calculated for varying target CPS2 scores. However, overall system power quality is a much larger issue than simply of wind integration. The difference between the CPS2 percentiles and the median of the bins will represent the implied incremental Operating Reserves position within that bin. This reserves position will be adjusted downward by the system L₁₀ for the each balancing authority area, as defined by NERC^{4,5}. As each respective bin will also have an implied probability by the number of data points falling within it, averaging the volumetric position over the study period will be a simple matter of integration.

Figure 5. Example graph of bin analysis for load following reserve for system load. Note the state variable is system load, and the reserves required are the difference between the upper and lower curves about the median. CPS2 targets of 97% and 94% are presented for comparison to illustrate sensitivity to the CPS2 score targeted.



³ The Control Performance 2 is a reliability standard is maintained by the North American Electric Reliability Corporation. A definition is available on page 3of the document at the following hyperlink: http://www.nerc.com/files/Reliability_Standards_Complete_Set_2010Jan25.pdf

⁴ The L₁₀ standard is a reliability standard component maintained by the North American Electric Reliability Corporation. A definition is available on page 1 of the document at the following hyperlink: http://www.nerc.com/files/Reliability_Standards_Complete_Set_2010Jan25.pdf

⁵ The L₁₀ for PacifiCorp’s east and west balancing areas is 49.53MW and 36.92MW respectively.

Per the illustration in Figure 5, the Load Following reserves position for the bin centered on a system load forecast 8,458 MW would be calculated by subtracting the lower bound value (roughly 8,244 MW) from the upper bound value (roughly 8,671 MW) for an estimate of 427 MW. Subtracting a hypothetical system L_{10} of 50 MW (doubled to account for its bidirectional nature), yields a reserves requirement of 327 MW for the load state defined by 8,458 MW of system load. Integrating this process through each bin will yield a composite position for the system control area. Wind generation can be analyzed in exactly the same procedure, but with generation output representing the individual state variable. As per the Regulation calculation, the wind and load reserves positions would be combined using the root sum square calculation, assuming their variability in the short term is independent.

$$\mathbf{Reserves}_{LoadFollowing} = \sqrt{\sigma_{LoadReserves}^2 + \sigma_{WindReserves}^2}$$

Operating Reserves Capacity Allocation

The method used to price the expense of maintaining additional Operating Reserves for increased wind penetration in this study using a production cost simulation, which dispatches plants hourly against load simulation with an assumed wind generation profile. Given the hourly-only granularity of these computations, and the fact that real-time operations must deal with sub-hourly variations, many details of real-time operation cannot be simulated in the production cost model, which may underestimate the cost of additional Operating Reserves. In this method, the most granular approximation of these services is the ten-minute interval calculation for Regulation. Given the limitations inherent in the data available, it is understood that other costs may be determined later to cover the expenses required to maintain this additional flexibility.

Another key feature of the production cost modeling is the requirement to separate Spinning Operating Reserves from Non-Spinning Operating Reserves.⁶ Similar to the approach used for the NREL Eastern Wind and Transmission Integration Study, PacifiCorp breaks out the service of the reserves position as follows in Table 2:

⁶ Spinning Operating Reserve is defined as unloaded generation which is synchronized, ready to serve additional demand and able to reach reserve amount within 10 minutes. Non-spinning Operating Reserve is defined as unloaded generation which is non-synchronized and able to reach required generation amount within 10 minutes.

Table 2. Allocation of Reserve Capacity to spinning and non-spinning positions for production cost modeling.⁷⁸

Reserve Service	Spinning Operating Reserve	Non-Spinning Operating Reserve
Regulation	4 * (Regulation _{10Min})	0
Load Following	0.5*(Load Following Reserves)	0.5*(Load Following Reserves)
Contingency	0.5*(5% of Hydro + 7% of Thermal generation output)	0.5*(5% of Hydro + 7% of Thermal generation output)
Total	Sum of the above	Sum of the above

Allotting the seasonally calculated reserves differential (under *Regulation* and *Load Following* sections above) results in a seasonal or annual schedule of additional spinning and non-spinning operational reserves required for the studied wind penetration level, ready to incorporate in PacifiCorp’s Planning and Risk (PaR) model, which calculates the production costs resulting from each wind penetration scenario, as described in the following section.

Production Cost Modeling

PacifiCorp’s PaR model, developed and licensed by Ventyx Energy LLC, uses the PROSYMchronological unit commitment and dispatch production cost simulation engine, which commits and dispatches the thermal resources by looking ahead for a week at a time. The Company will use the PaR model in deterministic mode to estimate the two types of wind integration costs contemplated in this study – wind integration costs associated with Operating Reserves and wind integration costs associated with system balancing. The former reflects integration costs that arise from short-term (within the hour and hour ahead) variability in wind generation and the latter reflects integration costs that arise from errors in forecasting wind generation on a day-ahead basis. Both types of wind integration costs will be estimated under a range of wind penetration scenarios as identified in Table 3.

⁷ The multiplier on Regulation services is consistent with previous studies and background information provided by Oak Ridge National Laboratory, per *Operational Impacts of Integrating Wind Generation into Idaho Power’s Existing Resource Portfolio*, p.49.

⁸ Contingency Reserves are specified by the Western Electricity Coordinating Council in per <http://www.nerc.com/files/BAL-STD-002-0.pdf>.

Table 3. Wind Penetration (on a Capacity Basis) scenarios planned for production cost analysis.

Representative Timing	Baseline	EOY 2007	EOY 2009	EOY 2011
Installed Wind Capacity	0	400	1400	1750
Wind Penetration	0%	3%	10%	12%

Calculating Operating Reserve Wind Integration Costs

PacifiCorp’s Initial Term data will serve as the basis for estimating the cost of Operating Reserve wind integration costs, and the calculation period will cover the 2011-13 forecast period (the Term) using the Company’s 2010 business plan resource portfolio.⁹ This calculation method aims to combine the benefits of using actual system data available for the three year period defined by the Initial Term with current forward price curves pertinent to setting the cost for wind integration service (including Regulation and Load Following services described above) on a forward basis.

To assess the effects of various levels of wind capacity added to the balancing authority areas, each of the penetration scenarios will be simulated in PaR using both *ideal* and *actual* wind profiles.¹⁰ Simulations with the ideal wind profile assumes all the wind energy is delivered in a shaped profile having the same amount of energy as the actual wind profile, but without hour-to-hour variability that defines actual wind generation. Such a profile would require no additional operating reserves to support wind generation variability, and as such, the PaR simulation will only be required to hold Operating Reserves consistent with load variability. The actual wind profile will reflect the 2007-09 observed and developed wind data in accordance with the data section above. These actual wind profiles will contain the variability used to derive the incremental Operating Reserve requirements, and consequently, the incremental reserve demand will be input into the PaR simulation. In both the ideal and actual PaR simulations, we will assume there is no day-ahead forecast error. The system cost differences between these two simulations will be divided by the total volume of wind generation contemplated for each penetration scenario to derive the wind integration costs associated with having to hold incremental Operating Reserves.

⁹ The 2010 business plan resource portfolio and its derivation are documented in the 2008 Integrated Resource Update report, filed with the state utility commissions on March 31, 2010. The report is available for download from PacifiCorp’s IRP Web page using the following hyperlink: http://www.pacificorp.com/content/dam/pacificorp/doc/Energy_Sources/Integrated_Resource_Plan/2008IRPUpdate/PacifiCorp-2008IRPUpdate_3-31-10.pdf

¹⁰ At least one high-end wind capacity penetration scenario will be simulated, which will be defined after preliminary portfolio development for the 2011 Integrated Resource Plan has been completed.

Calculating System Balancing Wind Integration Costs

Another series of PaR simulations will be completed to estimate day-to-day system balancing wind integration costs consistent with the wind penetration scenarios identified in Table 3. In this phase of the analysis, PacifiCorp generation assets will be committed consistent with a day-ahead *forecast* of wind and load, but dispatched against *actual* wind and load. To simulate this operational behavior, two PaR runs are necessary for each scenario. The first PaR run determines the unit commitment state of generation assets given the forecast of wind and load. The second PaR run uses the unit commitment state from the first PaR run, but dispatches units based on actual wind and load, which will be identical to the actual wind and load inputs used to derive Operating Reserve wind integration costs as described above. In both PaR simulations, the amount of incremental reserves required for each penetration scenario will be applied. The change in system costs from this second PaR simulation as compared to the system costs from the *actual wind* simulation already produced in the estimation of Operating Reserves will isolate the wind integration cost due to system balancing. Dividing the change in system costs by the volume of wind in each penetration scenario will yield system balancing integration costs on a \$/MWh basis. Table 4 summarizes how the various PaR simulations will be structured.

Table 4. PaR simulations that will be completed for each wind penetration scenario.

PaR Simulation	Forward Term	Load	Wind	Incremental Reserves	Day-Ahead Forecast Error
1	2011 - 2013	Initial Term - Actual	Initial Term - Perfect Shape	None	None
2	2011 - 2013	Initial Term - Actual	Initial Term - Actual	Yes	None
3	2011 - 2013	Initial Term - Day Ahead Forecast	Initial Term - Day Ahead Forecast	Yes	None
4	2011 - 2013	Initial Term - Actual	Initial Term - Actual	Yes	Yes (Commitment from PaR Simulation 3)

Operating Reserve Integration Costs = system costs from PaR simulation 2 less system costs from PaR simulation 1.

System Balancing Integration Costs = system costs from PaR simulation 4 less system costs from PaR simulation 2.