



DAVE JOHNSTON STEAM ELECTRIC PLANT

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November 9, 2007

Mr. Dave Finley, Administrator
Wyoming Division of Air Quality
122 West 25th Street
Herschler Building, 2nd Floor
Cheyenne, Wyoming 82002

Re: Dave Johnston Plant Chapter 6, Section 2 Construction Permit Application

Dear Mr. Finley:

PacifiCorp is planning to install between April 2007 and September 2012 air pollution control equipment on Dave Johnston units 3 and 4, along with other capital and O&M projects as specified in the attached Chapter 6, Section 2 construction permit application. The air pollution control equipment to be installed consists of flue gas desulfurization and low NO_x burners on units 3 and 4.

This application is submitted in accordance with the Wyoming Air Quality Standards and Regulations and requests a construction permit to be issued for the projects specified in the application.

PacifiCorp is requesting Plantwide Applicability Limitations for sulfur dioxide and nitrogen oxides and requests that these limitations be reflected in the construction permit.

Based on information and belief formed after reasonable inquiry, the statements and information in the construction permit application are true, accurate and complete.

If you have questions or require additional information, please contact Bill Lawson at (801) 220-4581 or Alan Dugan at (307) 436-2046.

Sincerely,

A handwritten signature in black ink, appearing to read "G. Hager", written over a light blue horizontal line.

Gregory L. Hager
Managing Director
Dave Johnston Plant

cc: Mike Mackey
Alan Dugan
Jim Doak
Bill Lawson

Dave Johnston Power Plant

Chapter 6, Section 2 Construction Permit Application

Submitted to the Wyoming Division of Air Quality
And Prepared by



1407 West North Temple
Salt Lake City, Utah 84116

November 2007

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1.0 Introduction

PacifiCorp proposes to add new pollution control devices that will significantly lower unit-specific emissions for sulfur dioxide (SO₂), nitrogen oxides (NO_x), and particulate matter (PM) at the Dave Johnston Power Plant located near Glenrock, in Converse County, Wyoming. The installation of this pollution control equipment, along with planned maintenance activities, requires an analysis of the air quality impacts of the planned projects and submittal of this Chapter 6, Section 2 construction permit application to the Wyoming Division of Air Quality. Through this application, PacifiCorp Energy is seeking to:

- Obtain a Chapter 6, Section 2 construction permit for the proposed addition of new pollution control devices and other projects.
- Establish plantwide applicability limits for SO₂ and NO_x. Plantwide applicability limits will allow the facility to conduct ongoing plant maintenance while ensuring the facility remains in compliance with new source review requirements.

The Dave Johnston facility currently operates under Title V operating permit #31-148. The operating permit has incorporated all applicable requirements contained in the following permits: MD-377, MD-682, and the June 10, 1993 Chapter 6, Section 2(k) permit waiver.

1.1 Existing Operations

PacifiCorp operates the Dave Johnston power plant located near Glenrock, Wyoming. The plant consists of four coal-fueled steam-electric generating units designated as units 1, 2, 3 and 4, respectively. Unit 1, rated at 106 net megawatts, began operation in 1958; unit 2, rated at 106 net megawatts, began operation in 1960; unit 3, rated at 220 net megawatts, began operation in 1964; and, unit 4, rated at 330 net megawatts, commenced operation in 1972. The facility operates in compliance with state and federal air emission requirements. The Dave Johnston Power Plant is an existing major stationary source of air emissions.

1.2 Emissions Consideration

The emission control projects included in this permit application will result in lower unit-specific SO₂, NO_x and PM emission rates for units 3 and 4.

To establish a clear baseline for determining when PSD requirements may be triggered in the future, PacifiCorp is proposing to establish plantwide applicability limits for SO₂ and NO_x that would limit plantwide emissions of these pollutants at the facility to the “past actual baseline emissions” as defined by the Environmental Protection Agency’s (EPA) “past actual to future actual emissions test.” The plantwide applicability limits would be in addition to the new, lower unit-specific limits to be established as a result of adding the proposed air pollution control devices. Establishing plantwide limits for SO₂ and NO_x will ensure that

any proposed project will not cause an associated emissions increase of these specific pollutants.

The installation of the advanced combustion controls to reduce NO_x emissions has the potential to increase carbon monoxide (CO) emissions from the facility. Therefore, PacifiCorp has included Best Available Control Technology (BACT) reviews for CO in this permit application. Also, to address concerns that the proposed air pollution control devices and other maintenance projects may be PSD triggering events for other PSD pollutants, this Chapter 6, Section 2 Permit Application includes a PSD evaluation for non-methane volatile organic compounds (VOCs), fluorides, particulate matter, sulfuric acid mist, and lead at the maximum possible operating rate to determine if significant net emissions increases of these pollutants might occur.

1.3 Prevention of Significant Deterioration Review

The facility is located in an area classified as attainment for all criteria pollutants [40 CFR 52.2320, including the 2002 amendments in FR 67 35444 and 67 44069] and is a listed PSD Source Category [40 CFR Part 52.21(b)(1)(i)(a)]; therefore, the requirements of the federal PSD program, as administered by the Wyoming Department of Environmental Quality and the Wyoming Division of Air Quality, will apply to the projects specified in this Chapter 6, Section 2 Permit Application.

As a result of the PSD review described in more detail below, PacifiCorp has concluded that there will not be a “significant” [40 CFR Part 52.21(b)(23) and WAQSR, Chapter 6, Section 4, “Significant” (i)] “net emissions increase” [40 CFR Part 52.21(b)(3) and WAQSR, Chapter 6, Section 4, “Significant emissions increase” (iii)] for SO₂ NO_x, PM, lead, sulfuric acid mist, or non-methane VOCs; therefore, a BACT review for these pollutants will not be required. PacifiCorp has included a BACT review for carbon monoxide.

1.4 Compliance with National Ambient Air Quality Standards for Class I and Class II Areas and NSPS

The facility, after completing the planned projects, will continue to meet all National Ambient Air Quality Standards (NAAQS) and the Class I and Class II PSD increments in the vicinity of the plant. A dispersion modeling analysis has been performed for CO which has the potential of a significant net emissions increase. At the request of the Wyoming Department of Environmental Quality a NAAQS impact analysis for all criteria pollutants has been performed. The facility will continue to meet the applicable New Source Performance Standards (NSPS) defined in the federal regulations at 40 CFR 60 Subpart D and Wyoming Air Quality Standard and Regulations Chapter 5, Section 2.

2.0 Project Description

PacifiCorp plans to install pollution control equipment and implement other plant projects between January 2008 and September 2012 as reflected in the project timeline shown in Table 2-1. These projects are listed in Appendices A through D. The projects identified are based on current plans and may be refined as overhaul schedules and equipment status change. As PacifiCorp further refines the project schedule and scope, additional information will be provided to the Wyoming Division of Air Quality.

The projects are summarized as follows:

Dave Johnston Unit 1

- Plant projects listed in Appendix A.

Dave Johnston Unit 2

- Plant projects listed in Appendix B.

Dave Johnston Unit 3

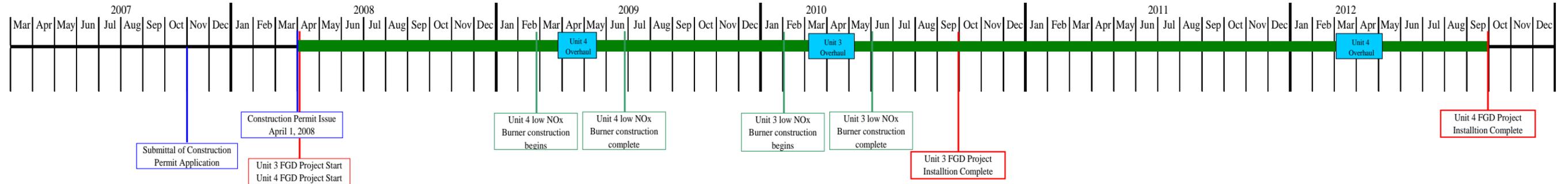
- Replacement of the existing cell burner configuration with low-NO_x burners.
- Installation of a spray dryer absorber flue gas desulfurization system.
- Installation of a baghouse.
- In-place abandonment of the existing electrostatic precipitator.
- Plant projects listed in Appendix C.

Dave Johnston Unit 4

- Replacement of the existing burners with a new Alstom LNCFS Level II low-NO_x firing system and the installation of one elevation of separated overfire air.
- Installation of a spray dryer absorber flue gas desulfurization system.
- Installation of a baghouse.
- Removal of the existing particulate matter wet venturi scrubber.
- Plant projects listed in Appendix D.

Table 2-1 Project Timeline

Dave Johnston Unit 3 Flue Gas Desulfurization / Low-NO_x Burners / Baghouse; Dave Johnston Unit 4 Flue Gas Desulfurization / Low-NO_x Burners / Baghouse and Other Plant Projects



2007 Activities

- 2007 U1 Coal load-in washdown system
- 2007 U1 Dust suppression for feeders 33 and 34
- 2007 U1 Replace DC90 baghouse bags
- 2007 U1 CEM replacement - units 1, 2 and 3
- 2007 U1 Mercury monitors
- 2007 U2 Replace reheater attemperator
- 2007 U2 Combustion optimization projects
- 2007 U2 Replace partial assemblies in reheater
- 2007 U2 Replace air heater baskets and sootblowers
- 2007 U2 Burner ignitor replacement
- 2007 U2 Replace waterwall inlet header tube stubs
- 2007 U2 Replace boiler expansion joints
- 2007 U2 #2 low pressure feedwater heater
- 2007 U2 #2 high pressure feedwater heater
- 2007 U2 Replace sootblowers
- 2007 U2 Burner nozzle replacement
- 2007 U2 Radial and circumferential. Seal replacement
- 2007 U2 Replace air heater seals
- 2007 U3 Replace flyash unloaders (2)
- 2007 U4 CEM replacement

2008 Activities

- 2008 U1 Replace baghouse at load-in with suppression
- 2008 U1 Eliminate tripper deck bag house U3 and 4A
- 2008 U1 Remove tripper deck cyclones - 2008
- 2008 U1 Baghouse bag changes - 2008
- 2008 U1 Replace 36 first pass membranes
- 2008 U1 Turbine/generator major LSB
- 2008 U1 Replace lower HPSH assemblies
- 2008 U1 Waterwall inlet header tube stub replacement
- 2008 U1 Unit 1 boiler waterwall tube replacement
- 2008 U1 Burner front elbow replacement
- 2008 U1 Burner management & mft cabinets replacement
- 2008 U1 Boiler asbestos replacement
- 2008 U1 Burner nozzle replacement
- 2008 U1 FD/ID fan damper drive replacement
- 2008 U1 Replace coal sweeps
- 2008 U1 Replace bottom ash hopper
- 2008 U1 Replace duct expansion joints
- 2008 U1 Replace feedwater heater controls
- 2008 U1 Unit 1 tripper transfer point passive dust control
- 2008 U1 Unit 1 - replace flyash unloaders
- 2008 U1 CO monitor
- 2008 U1 Coal feeder and VFD upgrade
- 2008 U1 Combustion optimization projects
- 2008 U1 Air heater seals replacement
- 2008 U1 Replace precipitator avc controls
- 2008 U1 Replace pulverizer hot air dampers
- 2008 U1 Secondary superheater pendant replacement
- 2008 U1 Turbine instrumentation upgrade
- 2008 U2 U2 turbine-generator refurbishment
- 2008 U2 Burner front elbow replacement
- 2008 U2 Generator field refurbishment
- 2008 U2 Bentley critical equipment monitoring
- 2008 U2 Burner management & mft cabinets replacement
- 2008 U2 Replace airheater pin racks
- 2008 U3 Tripper transfer point passive dust control
- 2008 U4 Reheat outlet header tube stub replacement
- 2008 U4 Tripper transfer point passive dust control
- 2008 U3/4 FGD Project

2009 Activities

- 2009 U1 Remove tripper deck cyclones - 2009
- 2009 U1 Baghouse bag changes - 2009
- 2009 U2 Control room hvac replacement
- 2009 U3 Boiler feed pump motor replacement - 2009
- 2009 U4 Low NO_x burners
- 2009 U4 Replace unit 4 controls
- 2009 U4 Replace low pressure feedwater heater
- 2009 U4 Replace low pressure feedwater heater tube bundle
- 2009 U4 Replace air heater baskets
- 2009 U4 Airheater sootblowers
- 2009 U4 Replace ignitors
- 2009 U4 Boiler waterwall tube panel replacement
- 2009 U4 Replace boiler coutant slope
- 2009 U4 Replace remaining 98 horizontal superheater assemblies
- 2009 U4 Replace reheater
- 2009 U4 High pressure/intermediate pressure turbine
- 2009 U4 Replace finishing superheat dissimilar metal welds in penthouse
- 2009 U4 Replace IK sootblowers
- 2009 U4 Water wall burner crotch tube replacement
- 2009 U4 Drag chain rebuild
- 2009 U4 Replace reheater loops 4-8
- 2009 U4 Cooling tower rebuild
- 2009 U4 Generator field refurbishment
- 2009 U3/4 FGD Project

2010 Activities

- 2010 U2 Clean air - NO_x
- 2010 U3 Hydrogen panel replacement
- 2010 U3 Boiler asbestos abatement
- 2010 U3 C mill PA flow replace
- 2010 U3 Generator stator rewedge
- 2010 U3 Replace twips controls
- 2010 U3 Replace burner impellers
- 2010 U3 Air preheater seal replacement
- 2010 U3 Boiler bifurcate tube replacement
- 2010 U3 Replace boiler/turbine controls
- 2010 U3 Economizer hoppers relocate - RES - SLC
- 2010 U3 Superheat assembly/header replacement
- 2010 U3 Turbine/generator major - 2009
- 2010 U3 Flue gas desulfurization system - spray dryer
- 2010 U3 Low NO_x burners
- 2010 U3 Replace front side slope boiler tubes
- 2010 U3 Replace boiler expansion joints
- 2010 U3 Boiler waterwall lagging supports
- 2010 U3 Waterwall tube replacement
- 2010 U3 Replace superheater tubing
- 2010 U3 Bottom ash hopper rebuild - 2010
- 2010 U3 Install economizer dry flight conveyor system
- 2010 U3 Replace superheater attemperator
- 2010 U3 CO monitor
- 2010 U3 Main transformer fire protection replacement
- 2010 U3 Replace safety valves - 2009
- 2010 U3/4 FGD Project

2011 Activities

- 2011 U2 Annunciator replacement
- 2011 U2 Boiler overhaul modifications
- 2011 U2 Boiler water wall tube replacement
- 2011 U2 Coal feeder replacement
- 2011 U2 HMI conversion
- 2011 U2 Replace high pressure superheater assemblies
- 2011 U2 Replace twips/feedwater level controls
- 2011 U2 Secondary superheater pendant replacement
- 2011 U4 FGD Project

2012 Activities

- 2012 U1 Boiler overhaul modifications
- 2012 U1 HMI conversion
- 2012 U1 Replace air heater baskets
- 2012 U1 Replace reheater header & terminal tubes
- 2012 U1 Replace battery bank/inverter
- 2012 U2 2.3 kv switch gear metering/project
- 2012 U2 Boiler asbestos abatement - 2012
- 2012 U2 CO monitor
- 2012 U2 Dcs component replacement
- 2012 U2 FD/ID fan damper drive replacement
- 2012 U2 Main transformer fire protection replacement
- 2012 U2 Replace air heater seals
- 2012 U2 Replace battery bank/inverter DCS
- 2012 U2 Replace mill damper drives
- 2012 U2 Turbine instrument upgrade
- 2012 U2 Replace reheater header & terminal tubes
- 2012 U4 Boiler overhaul modifications
- 2012 U4 DCS modifications
- 2012 U4 Platen secondary superheater replacement
- 2012 U4 Replace boiler upper arch tubes
- 2012 U4 Replace reheater & 1 superheater attemperators
- 2012 U4 Boiler waterwall tube panel replacement
- 2012 U4 Replace air heater seals
- 2012 U4 Replace burner nozzles
- 2012 U4 Replace finishing superheat dissimilar metal welds in penthouse
- 2012 U4 Replace PRV
- 2012 U4 Replace safety valve
- 2012 U4 Replace slag screen
- 2012 U4 Replace boiler upper arch refractory
- 2012 U4 FGD Project

Dave Johnston Unit 3 Flue Gas Desulfurization / Low-NO_x Burners / Baghouse; Dave Johnston Unit 4 Flue Gas Desulfurization / Low-NO_x Burners / Baghouse and Other Plant Projects

3.0 List of Potential Emission Points and Air Contaminants Emissions Summary

The Dave Johnston facility currently operates under Title V operating permit #31-148. The operating permit has incorporated all applicable requirements contained in the following permits: MD-377, MD-682, and the June 10, 1993 Chapter 6, Section 2(k) permit waiver. The facility's Title V permit identifies the facility's emission points and potential air contaminants. There may be additional emission sources at the facility following the pollution control equipment installation, including scrubber reagent baghouses, etc.

4.0 Evaluation of Historic and Future Emissions

4.1 Estimate of Emission Rates

This section presents the method for conducting various PSD evaluations, including:

- A determination of baseline actual emissions for SO₂, NO_x, PM, CO, ozone (as non-methane VOCs), fluoride (as hydrogen fluoride), lead, and sulfuric acid mist.
- A determination of projected actual emissions of CO, PM, VOCs, fluorides, lead, and sulfuric acid mist. (No such determination is needed for SO₂ or NO_x because the plantwide applicability limits cap future emissions at past actual baseline emission rates).
- A comparison between the CO, PM, VOCs, fluorides, lead, and sulfuric acid mist past actual baselines and future potential emissions to determine if PSD significance levels are triggered.

This section also sets forth the proposed plantwide applicability limits for SO₂ and NO_x.

4.2 Baseline Actual Emissions

The pollutants of interest for this review are SO₂, NO_x, PM, CO, VOCs, fluorides, lead, and sulfuric acid mist.

4.2.1 Calculation of baseline actual emissions

40 CFR 52.21(b)(48)(i) describes baseline actual emissions for the Dave Johnston plant as follows:

Baseline actual emissions means the rate of emissions, in tons per year, of a regulated NSR pollutant, as determined in accordance with paragraphs (b)(48)(i) through (iv) of this section.

- (i) For any existing electric utility steam generating unit, baseline actual emissions means the average rate, in tons per year, at which the unit actually emitted the pollutant during any consecutive 24-month period selected by the owner or operator within the 5-year period immediately preceding when the owner or operator begins actual construction of the project. The Administrator shall allow the use of a different time period upon a determination that it is more representative of normal source operation.

(a) The average rate shall include fugitive emissions to the extent quantifiable, and emissions associated with startups, shutdowns, and malfunctions.

(b) The average rate shall be adjusted downward to exclude any non-compliant emissions that occurred while the source was operating above any emission limitation that was legally enforceable during the consecutive 24-month period.

(c) For a regulated NSR pollutant, when a project involves multiple emissions units, only one consecutive 24-month period must be used to determine the baseline actual emissions for the emissions units being changed. A different consecutive 24-month period can be used for each regulated NSR pollutant.

(d) The average rate shall not be based on any consecutive 24-month period for which there is inadequate information for determining annual emissions, in tons per year, and for adjusting this amount if required by paragraph (b)(48)(i)(b) of this section.

To identify and calculate baseline actual emissions, PacifiCorp has used data from the EPA Clean Markets Division's emissions data base. In order to comply with the EPA's acid rain program, PacifiCorp utilizes continuous emissions monitors (CEMs) to report hourly SO₂ and NO_x emissions for each unit at the Dave Johnston facility. CEMs are also used to obtain and report the hourly heat input into each unit's boiler. The hourly emissions and heat input data is submitted to the EPA on a quarterly basis and is readily available on EPA's website located at <http://cfpub.epa.gov/gdm/>. For purposes of this review the 5-year evaluation period is October 2002 through September 2007. The baseline actual emissions are summarized in Table 4-1.

SO₂ Emissions:

Appendix E, Table DJ-1 identifies the monthly SO₂ emissions for the relevant time period. This data was obtained from the Environmental Protection Agency's (EPA) Acid Rain Emissions data base.

NO_x Emissions:

Appendix E, Table DJ-2 identifies the monthly NO_x emissions for the relevant time period. This data was obtained from the Environmental Protection Agency's (EPA) Acid Rain Emissions data base.

Heat Input and Coal Burned Data:

Heat input to the boilers and/or the tons of coal consumed are used to calculate PM, CO, hydrogen fluoride, lead and sulfuric acid mist emissions. Appendix E, Table DJ-3 identifies the monthly heat input for the evaluation period. This data was obtained from the Environmental Protection Agency's (EPA) Acid Rain Emissions data base. Monthly coal-burned data was obtained from the Department of Energy's EIA 767 report, and the results are contained in Appendix E, Table DJ-4.

Particulate Matter Emissions:

Plant particulate matter emissions consist of particulate emissions from the boiler stacks and small point and fugitive sources. Stack particulate emission rates are determined by annual particulate matter stack tests, using EPA reference methods, multiplied by monthly boiler heat input identified in the EPA's Acid Rain Emissions data base. The results are contained in Appendix E, Table DJ-5.

Emissions from small point sources and fugitive/area sources are obtained from the annual emissions inventories for the facility. The results are contained in Appendix E, Table DJ-6.

Carbon Monoxide Emissions:

Carbon monoxide emissions have been determined by multiplying the past annual coal consumption (Appendix E, Table DJ-4) by the AP-42 emission factor for carbon monoxide emissions from coal fueled boilers. The results are contained in Appendix E, Table DJ-7.

Volatile Organic Compounds:

Volatile organic compound emissions have been determined by multiplying the past annual coal consumption (Appendix E, Table DJ-4) by the AP-42 emission factor for volatile organic compounds emissions from coal fueled boilers. The results are contained in Appendix E, Table DJ-8.

Lead Emissions:

Lead emissions have been determined from the lead concentration in the coal, the PM emission rate (Appendix E, Table DJ-5), the boiler heat input (Appendix E, Table DJ-3) and the Method specified in AP-42 for determining lead emissions from coal fueled boilers. The results are contained in Appendix E, Table DJ-9.

Fluoride Emissions:

Fluoride emissions, as hydrogen fluoride, have been determined from the historical fluorine concentration in the coal, the past actual tons of coal burned (Appendix E, Table DJ-4) and the Method specified in AP-42 for determining fluoride emissions from coal fueled boilers. The results are contained in Appendix E, Table DJ-10.

Sulfuric Acid Mist Emissions:

Sulfuric acid mist emissions are calculated using past SO₂ emissions (Appendix E, Table DJ-1) and Electric Power Research Institute's "*Estimating Total Sulfuric Acid Emissions from Stationary Power Plants*, Technical Update, April 2007." The results are contained in Appendix E, Table DJ-11.

Table 4-1 Summary of Baseline Actual Emissions

Dave Johnston	SO₂ tons/yr	NO_x tons/yr	PM tons/yr	VOC tons/yr	CO tons/yr	H₂SO₄ tons/yr	Lead tons/yr	Fluorides tons/yr
Stack Emissions	21,956	15,838	2,049	121	1,008	21.8	0.32	81.0
Non-stack Emissions ¹	-	-	310	-	-	-	-	-
Baseline Actual Emissions	21,969	15,838	2,359	121	1,008	21.8	0.32	81.0

¹Maximum past non-stack PM emissions from 2002-2006 emissions inventories

4.3 Method for Determining Projected Actual Emissions for Prevention of Significant Deterioration Pollutants

The next step in evaluating projected actual emission increases is to determine the projected actual emissions for each pollutant. This is accomplished by determining the projected actual emissions based on coal quality, unit utilization, addition of pollution controls and expected emission rates.

Projected actual emissions are defined as follows:

40 CFR 52.21(b)(41)(i) *Projected actual emissions* means the maximum annual rate, in tons per year, at which an existing emissions unit is projected to emit a regulated NSR pollutant in any one of the 5 years (12-month period) following the date the unit resumes regular operation after the project, or in any one of the 10 years following that date, if the project involves increasing the emissions unit’s design capacity or its potential to emit that regulated NSR pollutant and full utilization of the unit would result in a significant emissions increase or a significant net emissions increase at the major stationary source.

(ii) In determining the projected actual emissions under paragraph (b)(41)(i) of this section (before beginning actual construction), the owner or operator of the major stationary source:

(a) Shall consider all relevant information, including but not limited to, historical operational data, the company’s own representations, the company’s expected business activity and the company’s highest projections of business activity, the company’s filings with the State or Federal regulatory authorities, and compliance plans under the approved State Implementation Plan; and

(b) Shall include fugitive emissions to the extent quantifiable and emissions associated with startups, shutdowns, and malfunctions; and

(c) Shall exclude, in calculating any increase in emissions that results from the particular project, that portion of the unit's emissions following the project that an existing unit could have accommodated during the consecutive 24-month period used to establish the baseline actual emissions under paragraph (b)(48) of this section and that are also unrelated to the particular project, including any increased utilization due to product demand growth; or

(d) In lieu of using the method set out in paragraphs (a)(41)(ii)(a) through (c) of this section, may elect to use the emissions unit's potential to emit, in tons per year, as defined under paragraph (b)(4) of this section.

PacifiCorp has proposed to accept plantwide applicability limits for SO₂ and NO_x which are based on the Dave Johnston facility's past actual baseline emissions. With these caps in place there is no potential that future emissions will be greater than past actual emissions, and no additional evaluation of future emissions is required.

4.3.1 Projected Actual Emissions for Particulate Matter, Carbon Monoxide, Ozone (as volatile organic compounds), Lead and Fluorides (as hydrogen fluoride), and Sulfuric Acid Mist

Under the provisions of 40 CFR 52.21(b)(41)(ii)(d) PacifiCorp has elected to determine the future emissions of PM, CO, VOCs, lead, fluoride, and sulfuric acid mist based on the facility's potential to emit these pollutants. In order to determine the projected actual emissions, the baseline actual emissions are adjusted to reflect operation at 100% capacity and 8,760 operating hours per year. Emissions of CO, VOCs, lead and fluorides are determined by multiplying the annual coal consumption or heat input by EPA determined emission factors as specified in EPA's "Clearinghouse for Inventories & Emissions Factors."

Heat Input and Coal Burned Data:

The potential heat input to the boilers and potential coal burn are determined by adjusting the past heat input and coal consumption to reflect operation at 100 percent capacity factor. The projected actual heat input and coal consumption values are used to calculate PM, CO, VOCs, fluorides, lead, and sulfuric acid mist emissions. The results are contained in Appendix E, Table DJ-6 (Heat Input) and Table DJ-7 (Coal Consumed).

Particulate Matter Emissions:

Projected actual particulate matter emissions determination:

Unit 1 and 2:

Projected actual particulate matter stack emissions for Units 1 and 2 are obtained by multiplying the unit-specific maximum hourly heat input values adjusted for 100% capacity factor (Appendix E, Table DJ-12) by the maximum unit-specific particulate matter emission rates determined from test results (Appendix E, Table DJ-14) and by a total annual operating time of 8,760 hours per year. The results are contained in Appendix E, Table DJ-14.

Unit 3 and 4:

Projected actual particulate matter stack emissions for Units 3 and 4 are obtained by multiplying the maximum hourly heat input values by a 0.015 lb/mmBtu PM emission factor by a total annual operating time of 8,760 hours per year. The results are contained in Appendix E, Table DJ-14.

The Projected actual non-stack emissions are evaluated at the maximum past actual non-stack emission rate identified in Appendix D, Table DJ-6. The future stack, non-stack and total annual particulate matter emission values are identified in Appendix D, Table DJ-5. There may be additional emission sources at the facility following the pollution control equipment installation, including potential scrubber reagent baghouses, etc.

Carbon Monoxide Emissions:

Projected actual emissions of carbon monoxide determination:

Unit 1 and 2:

Projected actual carbon monoxide emissions for Units 1 and 2 are obtained by multiplying the projected actual coal consumption (Appendix E, Table DJ-13) by the AP-42 emission factor for carbon monoxide. The results are contained in Appendix E, Table DJ-7.

Unit 3 and 4:

Projected actual carbon monoxide emissions for Units 3 and 4 are obtained by multiplying the maximum hourly heat input values by a 0.25 lb/mmBtu (Unit 3) or 0.20 lb/mmBtu (Unit 4) emission factor by a total annual operating time of 8,760 hours per year. The results are contained in Appendix E, Table DJ-7.

Volatile Organic Compounds:

Projected actual emissions of volatile organic compounds are determined by multiplying the projected annual coal consumption (Appendix E, Table DJ-13) by the AP-42 emission factor for volatile organic compound emissions from coal fueled boilers. The results are contained in Appendix E, Table DJ-8.

Lead Emissions:

Projected actual emissions of lead emissions determination:

Unit 1 and 2:

Projected actual emissions of lead determined using the method specified in AP-42 for coal fueled boilers. Multiplying the historical lead concentration in the coal by the maximum unit-specific particulate matter emission rates determined from test results (Appendix E, Table DJ-14), and by the 100% capacity factor heat input adjusted to the projected annual coal consumption (Appendix E, Table DJ-12). The results are contained in Appendix E, Table DJ-9.

Unit 3 and 4:

Projected actual emissions of lead determined using the method specified in AP-42 for coal fueled boilers. The method includes multiplying the historical lead concentration in the coal by the specific particulate matter emission rates, and by the maximum hourly heat input. The results are contained in Appendix E, Table DJ-9.

Fluoride Emissions:

Projected actual emissions of fluoride, as hydrogen fluoride, are determined from the historical fluorine concentration in the coal, the projected annual coal consumption (Appendix E, DJ-13), and the Method specified in AP-42 for determining fluoride emissions from coal fueled boilers. The results are contained in Appendix E, Table DJ-16.

Sulfuric Acid Mist Emissions:

Projected actual sulfuric acid mist emissions are calculated using Electric Power Research Institute's "*Estimating Total Sulfuric Acid Emissions from Stationary Power Plants*, Technical Update, April 2007."

Unit 1 and 2:

Projected actual emissions for Units 1 and 2 are obtained by using the past CEM-SO₂ emissions adjusted for 100% capacity factor (Appendix E, Table DJ-17). The results are contained in Appendix E, Table DJ-11.

Unit 3 and 4:

Projected actual emissions for Units 3 and 4 are obtained by using the projected annual coal consumption (Appendix E, Table DJ-13) and the maximum annual weight percent of sulfur in coal (Appendix E, Table DJ-11). The results are contained in Appendix E, Table DJ-11.

Identifying Emissions that "could have been accommodated" Prior to the Change:

The preamble to the Federal Register / Vol. 67, No. 251 / Tuesday, December 31, 2002 / Rules and Regulations page 80194 states, "If you are an existing emissions unit (including EUSGUs) you will estimate post-change emissions (projected actual emissions), in tons per year, to reflect any increase in annual emissions that may result from the proposed change. You should exclude, in calculating any increase in emissions that results from the project, that portion of the unit's emissions following the project that an existing unit could have accommodated during the baseline period and that is also unrelated to the particular project, including any increased utilization due to product demand growth."

Demand Growth Adjustment (Equivalent Availability Adjustment):

In the electric utility industry, data is regularly collected and reported to the National Electric Reliability Council (NERC) that is useful in making this calculation. The two values that are of interest for determining the load a unit could have accommodated are the unit's capacity factor and equivalent availability. The unit's capacity factor represents the unit's actual output as a percent of what its output would have been if the unit had operated at 100% of its capacity over the period being evaluated. The equivalent availability represents what the output of the unit could have provided if there had been demand for the unit's output.

To make the adjustment to account for demand growth, a ratio is created by dividing the equivalent availability by the capacity factor. The baseline actual emissions are then multiplied by the results of this calculation to determine what the actual emissions would have been if the unit had been fully utilized during this time period [40 CFR 52.41(ii)(c)(xii)(A) and 40 CFR

51.165(a)(xxviii)(A), WAQSR Chapter 6, Section 4]. The difference is then taken to identify the additional emissions associated with the demand growth that “could have been accommodated”.

Table 4-2 Summary of Projected Actual Emissions

	PM tons/yr	VOC tons/yr	CO tons/yr	H ₂ SO ₄ tons/yr	Lead tons/yr	Fluorides tons/yr
Baseline Actual Emissions (Not-Including Non-Stack Sources)	2,049	121	1,008	21.8	0.32	81.0
Potential to Emit (Not Including Non-Stack Sources) ^b	2,105	125	1,042	22.6	0.33	83.9
Projected Actual Emissions (Not Including Non-Stack Sources) ^b	1,562	139	7,500	10	0.21	53.1
Capable of Accommodating Adjustment (Potential to Emit – Past Actual)	56	4	34	0.8	0.01	2.9
Projected Actual Emissions minus “what the unit was capable of accommodating”	1,506	135	7,466	9.2	0.2	50.2

4.3.2 Prevention of Significant Deterioration Significance Determination

In order to determine if a Prevention of Significant Deterioration significance level has been reached the past actual baseline emissions adjusted for demand growth for each pollutant is subtracted from the projected annual emissions. If a significance level has been exceeded for a pollutant then a Prevention of Significant Deterioration review must be done for that pollutant.

As noted in Section 1.0, PacifiCorp intends to limit annual emissions of SO₂ and NO_x to the historical emissions as defined by the “past actual to future potential actual” emissions test specified in the December 2002 revisions to the New Source Review rules. PacifiCorp is requesting a Plantwide Applicability Limitation (PAL) for SO₂ and NO_x for the plant [40 CFR 52.21(aa) and WAQSR Chapter 6, Section 4]. These plantwide annual emissions limits will be imposed to assure, through federal enforceability, that the future Potential to Emit for the plant, as a whole, will be no greater than historical emissions. Therefore, there will be no net emissions increase of sulfur dioxide or nitrogen oxides as defined as “significant” [40 CFR 52.21(b)(23)] with respect to PSD review of these pollutants under the provisions of a PSD “major modification” [40 CFR 52.21(b)(2)(i)]. PSD review will apply to the other regulated pollutants for which there is a net increase defined as significant [40 CFR 52.21(b)(23)].

In order to determine if a Prevention of Significant Deterioration significance level has been reached the past actual baseline emissions adjusted for demand growth for each pollutant is subtracted from the projected annual emissions. If a significance level has been exceeded for a pollutant then a Prevention of Significant Deterioration review must be performed for that pollutant.

4.3.3 Contemporaneous Period and Pre-Project Actual Emissions

4.3.3.1 Definition of a “Major Modification”

An existing major source is subject to Prevention of Significant Deterioration review only if it undertakes a “major modification” [40 CFR 52.21(b)(2)(i)] and WAQSR Chapter 6, Section 2]. “Major modification” is defined as “any physical change in or change in the method of operation of a major stationary source that would result in a significant net emissions increase of any pollutant subject to regulation under Clean Air Act”. [40 CFR 52.21(b)(23) and WAQSR Chapter 6, Section 2]. A major modification does not include: routine maintenance, repair and replacement [40 CFR 52.21(b)(2)(iii)(a) and WAQSR Chapter 6, Section 2] or an increase in the hours of operation or in the production rate [40 CFR 52.21(b)(2)(iii)(f) and WAQSR Chapter 6, Section 2].

To determine if a Prevention of Significant Deterioration significance level has been reached the baseline actual emissions are subtracted from the projected actual emissions. The results of this evaluation for each pollutant are shown in Table 4-3.

Table 4-3 Evaluation of significance levels by pollutant

	Projected Actual minus Baseline Actual tons/year	PSD Review Significance Level tons/year	Emission Increase Greater than Significance Level
CO	6492	100	Yes
Ozone (as VOC)	18	40	No
Particulate Matter	- 487	25	No
Fluoride (as HF)	- 27.9	3	No
Lead	- 0.11	0.6	No
Sulfuric acid mist	- 11.8	7	No

4.3.3.2 Projects are a Major Modification Only for Carbon Monoxide

Although the proposed projects may constitute a physical change at the plant, they will **not** result in significant net emissions increases of lead, particulate matter, non-methane volatile organic compounds, sulfuric acid mist, or fluorides, and therefore are not major modifications for these pollutants. The results of the emissions evaluation indicate that future potential emissions of CO may increase above the PSD significance level.

4.4 Requested Emission Rate Limits

The following emission rates are requested for Unit 3:

Particulate matter \leq 10 microns (filterable):

- 42 lb/hr, annual average (2,800 MMBtu/hr x 0.015 lb/ MMBtu)

This limit will go into effect after the flue gas desulfurization system has been completed and deemed commercial. The expected commercial date is September 2010. After successful testing the equipment will be deemed commercial

Sulfur dioxide:

- 0.15 lb/MMBtu, annual average
- 420 lb/hr, 24-hr average (2,800 MMBtu/hr x 0.15 lb/ MMBtu)
- 1.2 lb/MMBtu, 2-hr average

This limit will go into effect after the flue gas desulfurization system has been completed and deemed commercial. The expected commercial date is September 2010. After successful testing the equipment will be deemed commercial

Nitrogen oxides:

- 0.28 lb/MMBtu, annual average

This limit will go into effect after the low NO_x burners have been installed, tested and deemed commercial. The expected installation date is May 2010, with performance testing to be completed by September of 2010. After successful testing the equipment will be deemed commercial.

Carbon monoxide:

- 0.25 lb/MMBtu, 30 day average

This limit will go into effect after the low NO_x burners have been installed, tested and deemed commercial. The expected installation date is May 2010, with performance testing to be completed by September of 2010. After successful testing the equipment will be deemed commercial.

The following emission rate is requested for Unit 4:

Particulate matter \leq 10 microns (filterable):

- 71 lb/hr, annual average (4,700 MMBtu/hr x 0.015 lb/ MMBtu)

This limit will go into effect after the flue gas desulfurization system has been completed and deemed commercial. The expected commercial date is September 2010. After successful testing the equipment will be deemed commercial

Sulfur dioxide:

- 0.15 lb/MMBtu, annual average
- 705 lb/hr, 24-hr average (4,700 MMBtu/hr x 0.15 lb/ MMBtu)
- 1.2 lb/MMBtu, 3-hr average

This limit will go into effect after the flue gas desulfurization system has been completed and deemed commercial. The expected commercial date is September 2012. After successful testing the equipment will be deemed commercial

Nitrogen oxides:

- 0.17 lb/MMBtu, annual average

This limit will go into effect after the low NO_x burners have been installed, tested, and deemed commercial. The expected installation date is September 2009 with performance testing to be completed by September 2009. After successful testing the equipment will be deemed commercial.

Carbon monoxide:

- 0.20 lb/MMBtu, 30-day average

This limit will go into effect after the low NO_x burners have been installed, tested, and deemed commercial. The expected installation date is September 2009 with performance testing to be completed by September 2009. After successful testing the equipment will be deemed commercial.

The following federally enforceable annual plantwide emission limits are requested for SO₂ and NO_x. These limits are based the highest 24 consecutive month average in the previous 60 month period plus the prevention of significant deterioration threshold.

Sulfur Dioxide: 22,009 tons/year annual plantwide emission limit

Nitrogen Oxides: 15,878 tons/year annual plantwide emission limit

5.0 Description of Pollution Control Equipment

5.1 Sulfur Dioxide

5.1.1 Unit 3 - Flue Gas Desulfurization (FGD)

Dave Johnston unit 3 is currently uncontrolled for sulfur dioxide. A new dry flue gas desulfurization system utilizing lime as a reagent is anticipated to remove approximately 80 percent of the inlet sulfur dioxide concentration. Flue gas is treated in a spray dryer absorber (SDA) by mixing the gas stream concurrently with atomized lime slurry droplets. The lime slurry is atomized through rotary cup spray atomizers or through dual fluid nozzles. Some of the water in the spray droplets evaporates, cooling the gas at the inlet from temperatures ranging from approximately 300-350°F to an outlet temperature ranging from 160-180°F, depending on the relationship between approach to saturation and removal efficiency. The droplets absorb SO₂ from the gas and react with the lime in the slurry. The desulfurized flue gas, along with reaction products, non-reacted lime, and fly ash, flow out of the dry scrubber to the electrostatic precipitator. The removal efficiency of the spray dryer is limited by the need to maintain flue gas exit temperatures above the acid dew point to prevent condensation of sulfuric acid in the fabric filter baghouse. A portion of the desulfurization system waste product is recycled back to the process to increase efficiency and minimize reagent use.

5.1.2 Unit 4 - Flue Gas Desulfurization (FGD)

Dave Johnston unit 4 is currently equipped with a CHEMICO wet venture particulate scrubber modified with the lime injection for sulfur dioxide control. A new dry flue gas desulfurization system utilizing lime as a reagent is anticipated to remove approximately 80 percent of the inlet sulfur dioxide concentration. Flue gas is treated in a spray dryer absorber (SDA) by mixing the gas stream concurrently with atomized lime slurry droplets. The lime slurry is atomized through rotary cup spray atomizers or through dual fluid nozzles. Some of the water in the spray droplets evaporates, cooling the gas at the inlet from temperatures ranging from approximately 300-350°F to an outlet temperature ranging from 160-180°F, depending on the relationship between approach to saturation and removal efficiency. The droplets absorb SO₂ from the gas and react with the lime in the slurry. The desulfurized flue gas, along with reaction products, non-reacted lime, and fly ash, flow out of the dry scrubber to the electrostatic precipitator. The removal efficiency of the spray dryer is limited by the need to maintain flue gas exit temperatures above the acid dew point to prevent condensation of sulfuric acid in the fabric filter baghouse. A portion of the desulfurization system waste product is recycled back to the process to increase efficiency and minimize reagent use.

5.2 Nitrogen Oxides

5.2.1 Unit 3 Low NOX Burners

Dave Johnston unit 3 has a Babcock & Wilcox cell-fired boiler that utilizes a non-typical three-cell burner configuration. The existing burners will be replaced with low NO_x burners and overfire air or a booster overfire air (BOFA) system. The final design of the low NO_x burners remains to be determined.

5.2.2 Unit 4 Low NOX Burners

Unit 4 has a dry-bottom, tangentially-fired Combustion Engineering (CE) boiler. PacifiCorp is proposing to install an Alstom LNCFS Level II low-NO_x firing system with one elevation of separated overfire air. The new low NO_x burners that will be installed are state-of-the-art burners offered by Alstom that will be installed in modified windboxes and include one elevation of separated overfire air ports.

5.3 Particulate Matter

5.3.1 Units 3 - Baghouse

PacifiCorp is proposing to install a fabric filter dust collector with multiple compartments. The filter dust collector will be designed for on-line cleaning of the filter bags. In addition, individual compartments can be removed from service to facilitate maintenance while remaining compartments remain in service.

5.3.2 Units 4 - Baghouse

PacifiCorp is proposing to install a fabric filter dust collector with multiple compartments. The filter dust collector will be designed for on-line cleaning of the filter bags. In addition, individual compartments can be removed from service to facilitate maintenance while remaining compartments remain in service.

5.4 Carbon Monoxide and Volatile Organic Compounds

Carbon monoxide (CO) and non-methane volatile organic compounds (VOCs) are formed from the incomplete combustion of the coal in the boiler. The formation of CO and VOCs is limited by controlling the combustion of the fuel and providing adequate oxygen for complete combustion. However, emissions of CO and VOCs may be increased with the installation of combustion modifications to reduce NO_x emissions (low NO_x burners). In order to reduce the formation of thermal NO_x in the combustion process, low NO_x burners rely on a staged combustion of the fuel. This may lead to a slight increase of CO under some boiler operating conditions. Good combustion control and tuning to reduce NO_x emissions while minimizing CO emissions are the techniques to be used to limit CO and VOC emissions.

6.0 Best Available Control Technology Determination

The Clean Air Act's PSD program provides that a Best Available Control Technology analysis must be conducted if a proposed project will result in a significant increase of a PSD pollutant.

6.1 Applicability

PacifiCorp has determined that the projects proposed for the Dave Johnston facility may result in a significant increase (as determined by the thresholds established in the regulations) of CO and sulfuric acid mist. Therefore, PacifiCorp has conducted a Best Available Control Technology analysis for CO and sulfuric acid mist.

The EPA has developed a process for conducting Best Available Control Technology analyses. This method is referred to as the "top-down" method. The steps to conducting a "top-down" analysis are listed in Environmental Protection Agency's *New Source Review Workshop Manual* Draft, October 1990. The steps are:

- Step 1 – Identify All Control Technologies
- Step 2 – Eliminate Technically Infeasible Options
- Step 3 – Rank Remaining Control Technologies by Control Effectiveness
- Step 4 – Evaluate Most Effective Controls and Document Results
- Step 5 – Select Best Available Control Technology

6.1.1 Carbon Monoxide Best Available Control Technology Analysis

Combustion controls designed to reduce NO_x emissions may increase carbon monoxide by creating oxygen deficient combustions zones in the boiler. These controls are balanced to provide the maximum NO_x reduction while minimizing carbon monoxide emission increases.

6.1.1.1 Step 1 - Identify All Control Technologies

Only two control technologies have been identified for control of carbon monoxide.

- Catalytic oxidation
- Combustion controls

The catalytic oxidation is a post-combustion control device that would be applied to the combustion system exhaust, while combustion controls are part of the combustion system design of the boiler.

6.1.1.2 Step 2 - Eliminate Technically Infeasible Options

Catalytic oxidation has been used to obtain the most stringent control of carbon monoxide emissions from combustion turbines firing natural gas. This alternative, however, has never been applied to a coal-fired boiler and has not been demonstrated to be a practical technology in this application.

For sulfur-containing fuels such as coal, an oxidation catalyst will convert SO₂ to SO₃, resulting in unacceptable levels of corrosion to the flue gas system as SO₃ is converted to H₂SO₄. Generally, oxidation catalysts are designed for a maximum particulate loading of 50 milligrams per cubic meter. Dave Johnston units 1, 2, 3 and 4 have particulate matter loadings upstream of their respective particulate matter control devices in excess of 5,000 milligrams per cubic meter. In addition, trace elements present in coal, particularly chlorine, are poisonous to oxidation catalysts. Catalysts have not been developed that have or can be applied to coal-fired boilers due to the high levels of particulate matter and trace elements present in the flue gas.

Although the catalyst could be installed downstream of the particulate matter pollution control devices (unit 3 electrostatic precipitator and unit 4 wet venturi scrubber), the flue gas temperature at that point will be approximately 300° F, which is well below the minimum temperature required (600°F) for the operation of the oxidation catalyst. Utilization of a catalyst would require the flue gas to be reheated, resulting in significant negative energy and economic impacts.

For these reasons, as well as the low levels of CO in coal-fired units, no pulverized-coal-fired boilers have been equipped with oxidation catalysts. Use of an oxidation catalyst system is thus

considered technically infeasible and this system cannot be considered to represent Best Available Control Technology for control of carbon monoxide.

6.1.1.3 Step 3 - Rank Remaining Control Technologies by Control Effectiveness

Based on the Step 2 analysis, combustion control is the only remaining technology for this application.

6.1.1.4 Step 4 - Evaluate Most Effective Controls and Document Results

There are no environmental or energy costs associated with combustion controls.

6.1.1.5 Step 5 - Select Best Available Control Technology

The EPA New Source Review, RACT, BACT, LAER Clearinghouse database for comparable sources related to CO is shown in Appendix F, Table F-1. The final step in the top-down Best Available Control Technology analysis process is to select Best Available Control Technology. Based on the above analysis, good combustion control for CO is chosen as Best Available Control Technology for these projects. Because there is a balance between reducing NO_x emissions with advanced combustion controls and increasing CO emissions, i.e., the lower the NO_x emissions the greater the potential for an increase in CO emissions, an annual emission limit of 0.25 lb/MMBtu for CO is recommended for Unit 3 and a CO limit of 0.20 lb/MMBtu for Unit 4.

7.0 Regulatory Review

This section provides a regulatory review of the applicability of state and federal air quality permitting requirements for the addition of the emission controls and other plant projects.

7.1 State of Wyoming Air Permitting Requirements

The State of Wyoming has been granted authority to implement and enforce the federal Clean Air Act [pursuant to the State Implementation Plan review and approval process] and federal air permitting requirements which are embodied within the state rules. The plant is a major stationary source of air emissions, as defined within the Wyoming Air Quality Standards and Regulations, Chapter 6, Section 4, 40 CFR 70 (Title V Operating Permits) and 40 CFR Part 52.21 (Prevention of Significant Deterioration Program Requirements). The Wyoming Department of Environmental Quality, Air Quality Division, has previously issued permits and permit revisions as appropriate for the existing Plant facilities. The general requirements for permits and permit revisions are codified under the state environmental protection regulations Wyoming Air Quality Standards and Regulations.

7.1.1 Wyoming Air Quality Standards and Regulations, Chapter 6, Permitting Requirements

The replacement, addition or upgrade of existing emissions controls will result in a potential increase of some air pollutant emissions, necessitating the issuance of a Chapter 6, Section 2 construction permit from the State of Wyoming, Department of Environmental Quality. PacifiCorp is required by the Wyoming Air Quality Standards and Regulations, Chapter 6, Section 2 to submit to the Air Quality Division of the Wyoming Department of Environmental Quality an application and obtain a Chapter 6, Section 2 construction permit prior to initiation of construction activities associated with the proposed projects.

7.1.2 Operating Permit Requirements, Wyoming Air Quality Standards and Regulations Chapter 6, Section 3

The federal operating permit program (Title V) is implemented by regulations codified at 40 CFR Part 70 and 71. The State of Wyoming has been granted authority to implement and enforce the federal Title V program through state regulations outlined under Wyoming Air Quality Standards and Regulations, Chapter 6, Section 3. PacifiCorp currently has Wyoming Department of Environmental Quality issued Chapter 6, Section 3 Operating Permit 31-148 for the Dave Johnston power plant. The replacement, addition of, or upgrade to existing air emissions controls and other plant projects constitute a significant modification to the plant and will therefore require a modification of the existing Title V permit.

7.1.3 Prevention of Significant Deterioration (Prevention of Significant Deterioration) Wyoming Air Quality Standards and Regulations, Chapter 6, Section 4

Within the federal New Source Review regulations, a subset of rules, which apply to major sources and major modifications within attainment areas, is referred to as the Prevention of Significant Deterioration program. Since the planned projects are at a current PSD source, located in an area classified as attainment for all criteria pollutants, the PSD program will apply to the permitting of these projects. The Wyoming Division of Air Quality has been delegated full authority from the EPA for administering the federal PSD rules; consequently, these requirements are codified within the state's permitting rules at WAQSR Chapter 6, Section 4.

The PSD program defines a major stationary source as:

- Any source type belonging to one of the 28 listed source categories that have a potential to emit of 100 tons per year or more of any criteria pollutant regulated under the Clean Air Act, or
- Any other (non-categorical) source type with a potential to emit of 250 tons per year of any pollutant regulated under the Clean Air Act.

The Dave Johnston facility is a fossil fueled steam electric plant of more than 250 million Btu/hr heat input and is considered an existing major stationary source because of the potential to emit for sulfur dioxide, nitrogen oxides, particulate matter, carbon monoxide, volatile organic compounds, and hydrogen fluoride all exceed the limits listed in this section.

Modifications to an existing major source are considered major and subject to PSD review if the resulting potential net emissions increase is equal to or greater than the corresponding significant emissions increase threshold for each respective pollutant. A net emissions increase includes both of the following:

- The potential increase in emissions due to the modifications itself; and
- Contemporaneous net emissions increases and decreases of regulated air pollutants, under the PSD program

An emissions increase is considered significant if emissions meet or exceed any of the following rates:

- Carbon monoxide, 100 tons per year
- NO_x, 40 tons per year
- SO₂, 40 tons per year
- PM₁₀, 15 tons per year
- Particulate matter, 25 tons per year

- Ozone, 40 tons per year of VOCs
- Lead, 0.6 tons per year
- Sulfuric acid mist, 7 tons per year
- Fluorides, 3 tons per year
- Hydrogen sulfide, 10 tons per year

The basic PSD permitting requirements and conditions for issuing a construction permit that must be met for a major modification include:

- The degree of pollution control for emissions, to include fugitive emissions and fugitive dust, is at least BACT, except as otherwise provided in Chapter 6, Section 2 [WAQSR Chapter 6, Section 2(c)(v)]
- Performing ambient air quality impacts analysis – air dispersion modeling [WAQSR Chapter 6, Section 4(b)(i)(A)(I)]
- Analysis of impact to soils, vegetation, and visibility
- Analysis of Class I area impacts

The results of the PSD review for the Dave Johnston pollution control equipment projects are identified in Table 4-3. The PSD evaluation indicates that there may be a net increase of carbon monoxide emissions following completion of the planned projects. The potential carbon monoxide increase can be attributed to the units 3 and 4 low-NO_x control projects.

8.0 Appendix A

Dave Johnston Unit 1 Capital and O&M Projects

Year	Project	Description
2007	Coal load-in washdown system	Install a washdown system on the coal load-in
2007	Dust suppression for feeders 33 and 34	Install dust suppression on coal feeders 33 and 34
2007	Replace DC90 baghouse bags	Replace bags on DC90 baghouse in the coal yard
2007	CEM replacement - units 1, 2 and 3	Replace the continuous emissions monitor
2007	Mercury monitors	Install mercury monitors
2008	Replace baghouse at load-in with suppression	Replace existing baghouse at coal load-in with dust suppression
2008	Eliminate tripper deck bag house U3 and 4A	Eliminate the tripper deck baghouses U3 and 4A
2008	Remove tripper deck cyclones - 2008	Remove the tripper deck cyclones
2008	Baghouse bag changes - 2008	Replace baghouse bags
2008	Replace 36 first pass membranes	Replace 36 of the first pass membranes (water treatment)
2008	Turbine/generator major LSB	Turbine-generator overhaul
2008	Replace lower HPSH assemblies	Replace lower high pressure super heaters assemblies
2008	Waterwall inlet header tube stub replacement	Replace waterwall inlet header tube stubs
2008	Unit 1 boiler waterwall tube replacement	Replace worn and eroded waterwall tubes
2008	Burner front elbow replacement	Replace worn out coal elbows.
2008	Burner management & mft cabinets replacement	Replace relays and cabinets.
2008	Boiler asbestos replacement	Replace asbestos containing insulation on boiler.
2008	Burner nozzle replacement	Replace worn out coal burner nozzles.
2008	FD/ID fan damper drive replacement	Replace old worn out damper drives.
2008	Replace coal sweeps	Replace coal piping.
2008	Replace bottom ash hopper	Replace worn out bottom ash hopper.
2008	Replace duct expansion joints	Replace worn out expansion joints.
2008	Replace feedwater heater controls	Replace old outdated feedwater controls.
2008	Unit 1 tripper transfer point passive dust control	Install tripper transfer point passive dust control
2008	Unit 1 - replace flyash unloaders	Replace flyash unloaders
2008	CO monitor	Install a carbon monoxide monitor

Year	Project	Description
2008	Coal feeder and VFD upgrade	Upgrade existing coal feeders and variable frequency drives
2008	Combustion optimization projects	Boiler combustion optimization projects
2008	Air heater seals replacement	Replace air preheater seals
2008	Replace precipitator avc controls	Replace automatic voltage controllers.
2008	Replace pulverizer hot air dampers	Replace pulverizer hot air dampers.
2008	Secondary superheater pendant replacement	Replace boiler superheater tubing.
2008	Turbine instrumentation upgrade	Replace existing turbine instruments with new technology.
2009	Remove tripper deck cyclones - 2009	Remove the tripper deck cyclones
2009	Baghouse bag changes - 2009	Baghouse bag replacement
2012	Boiler overhaul modifications	Standard repairs/replacements conducted during 30-day overhaul.
2012	HMI conversion	Replace plant data control system with new technology.
2012	Replace air heater baskets	Replace worn out air heater components.
2012	Replace reheater header & terminal tubes	Replace worn out boiler tube components.
2012	Replace battery bank/inverter	Replace emergency backup DC power source.

9.0 Appendix B

Dave Johnston Unit 2 Capital and O&M Projects

Year	Project	Description
2007	Replace reheater attemperator	Replace reheat attemperator
2007	Combustion optimization projects	Boiler combustion optimization projects
2007	Replace partial assemblies in reheater	Replace worn and eroded tube assemblies in the reheater
2007	Replace air heater baskets and sootblowers	Replace worn air preheater baskets and air preheater sootblowers
2007	Burner ignitor replacement	Replace existing burner igniters
2007	Replace waterwall inlet header tube stubs	Replace waterwall inlet header tube tubes
2007	Replace boiler expansion joints	Replace boiler expansion joints
2007	#2 low pressure feedwater heater	Replace the #2 low pressure feedwater heater
2007	#2 high pressure feedwater heater	Replace the #2 high pressure feedwater heater
2007	Replace sootblowers	Replace sootblowers
2007	Burner nozzle replacement	Replace coal burner nozzles
2007	Radial and circumferential. Seal replacement	Replace radial and circumferential seals on the air preheater
2007	Replace air heater seals	Replace air preheater seals
2008	U2 turbine-generator refurbishment	Inspect and repair unit 2 turbine components.
2008	Burner front elbow replacement	Replace worn out coal pipe components.
2008	Generator field refurbishment	Repair generator field.
2008	Bentley critical equipment monitoring	Replace critical equipment instrumentation.
2008	Burner management & mft cabinets replacement	Replace relays and cabinets.
2008	Replace airheater pin racks	Replace worn out pin rack.
2009	Control room HVAC replacement	Replace worn out control room HVAC equipment.
2010	Clean air - NOX	Investigate and install low NOx modifications.
2011	Annunciator replacement	Replace old worn out annunciator panel.
2011	Boiler overhaul modifications	Standard repairs/replacements conducted during 30-day overhaul.
2011	Boiler water wall tube replacement	Replace worn out boiler tubing.
2011	Coal feeder replacement	Replace coal feeders with new style.
2011	HMI conversion	Replace plant data control system with new technology.
2011	Replace high pressure superheater assemblies	Replace both upper and lower worn out tube assemblies in the boiler.

Year	Project	Description
2011	Replace twips/feedwater level controls	Replace turbine protection equipment.
2011	Secondary superheater pendant replacement	Replace boiler superheater tubing.
2012	2.3 kv switch gear metering/project	Replace electrical metering equipment.
2012	Boiler asbestos abatement - 2012	Replace asbestos containing insulation on boiler.
2012	CO monitor	Install a new CO monitor on the boiler outlet.
2012	Dcs component replacement	Replace worn out components on the Data Control System.
2012	FD/ID fan damper drive replacement	Replace old worn out damper drives.
2012	Main transformer fire protection replacement	Install new fire protection equipment on the main transformer.
2012	Replace air heater seals	Replace the worn out air heater seals.
2012	Replace battery bank/inverter DCS	Replace emergency backup DC power source.
2012	Replace mill damper drives	Replace worn out mill damper drives.
2012	Turbine instrument upgrade	Replace old turbine instrumentation.
2012	Replace reheater header & terminal tubes	Replace worn out boiler tube components.

10.0 Appendix C

Dave Johnston Unit 3 Capital and O&M Projects

Unit	Project	Description
2007	Replace flyash unloaders (2)	Replace two fly ash unloaders
2008	Tripper transfer point passive dust control	Install passive dust control on tripper transfer point
2009	Boiler feed pump motor replacement - 2009	Replace boiler feed pump motors
2010	Hydrogen panel replacement	Replace worn out hydrogen control panel.
2010	Boiler asbestos abatement	Replace asbestos containing insulation.
2010	C mill PA flow replace	Replace flow monitoring equipment.
2010	Generator stator rewedge	Replace wedging in generator stator.
2010	Replace twips controls	Replace turbine protection controls.
2010	Replace burner impellers	Replace coal burner impellers
2010	Air preheater seal replacement	Replace air preheater seals
2010	Boiler bifurcate tube replacement	Replace bifurcating tubes in the boiler
2010	Replace boiler/turbine controls	Replace boiler and turbine controls
2010	Economizer hoppers relocate - RES – SLC	Relocate economizer hoppers
2010	Superheat assembly/header replacement	Replace superheat tubes assembly/header
2010	Turbine/generator major - 2009	Turbine/generator overhaul
2010	Flue gas desulfurization system – spray dryer	Install a flue gas desulfurization system to remove approximately 80% of the sulfur dioxide in the flue gas
2010	Low NO _x burners	Install low NO _x burners and combustion controls to reduce NO _x emissions
2010	Replace front side slope boiler tubes	Replace front side slope boiler tubes
2010	Replace boiler expansion joints	Replace boiler expansion joints
2010	Boiler waterwall lagging supports	Replace boiler waterwall lagging supports
2010	Waterwall tube replacement	Replace worn and eroded waterwall tubes
2010	Replace superheater tubing	Replace superheat tubes
2010	Bottom ash hopper rebuild – 2010	Rebuild bottom ash hopper
2010	Install economizer dry flight conveyor system	Install economizer dry flight ash conveyor system
2010	Replace superheater attemperator	Replace the superheater attemperator
2010	CO monitor	Install carbon monoxide monitor
2010	Main transformer fire protection replacement	Replace fire protection system on main transformer
2010	Replace safety valves - 2009	Replace safety valves on boiler

11.0 Appendix D

Dave Johnston Unit 4 Capital and O&M Projects

Unit	Project	Description
2009	Low NO _x burners	Install low NO _x burners and combustion controls to reduce NO _x emissions
2009	Replace unit 4 controls	Replace boiler controls
2009	Replace low pressure feedwater heater	Replace low pressure feedwater heater
2009	Replace low pressure feedwater heater tube bundle	Replace low pressure feedwater heater tube bundle
2009	Replace air heater baskets	Replace air preheater baskets
2009	Airheater sootblowers	Replace air preheater sootblowers
2009	Replace ignitors	Replace boiler igniters
2009	Boiler waterwall tube panel replacement	Replace waterwall tube panels
2009	Replace boiler coutant slope	Replace boiler coutant slope (waterwall)
2009	Replace remaining 98 horizontal superheater assemblies	Replace remaining 98 horizontal superheater assemblies
2009	Replace reheater	Replace reheater
2009	High pressure/intermediate pressure turbine	High pressure/intermediate pressure turbine overhaul
2009	Replace finishing superheat dissimilar metal welds in penthouse	Replace finishing superheater dissimilar metal welds in penthouse
2009	Replace IK sootblowers	Replace 1k sootblowers
2009	Water wall burner crotch tube replacement	Replace waterwall burner crotch tubes
2008	Reheat outlet header tube stub replacement	Replace reheater outlet header tube stubs
2007	CEM replacement	Replace the continuous emissions monitor
2009	Drag chain rebuild	Rebuild the existing drag chain conveyor
2009	Replace reheater loops 4-8	Replace reheater loops
2008	Tripper transfer point passive dust control	Install passive dust control on tripper transfer point
2009	Cooling tower rebuild	Rebuild Unit 4 Cooling Tower.
2009	Generator field refurbishment	Repair generator field.
2012	Boiler overhaul modifications	Standard repairs/replacements conducted during 30-day overhaul.
2012	DCS modifications	Modifications to the new DCS System.
2012	Platen secondary superheater replacement	Replace superheater tubing.
2012	Replace boiler upper arch tubes	Replace boiler upper arch area tubes.
2012	Replace reheater & 1 superheater	Replacement of two attemperators.

Unit	Project	Description
	attemperators	
2012	Boiler waterwall tube panel replacement	Replace waterwall tube panels
2012	Replace air heater seals	Replace the worn out seals in the air heater.
2012	Replace burner nozzles	Replace worn out burner nozzles.
2012	Replace finishing superheat dissimilar metal welds in penthouse	Replace finishing superheater dissimilar metal welds in penthouse
2012	Replace PRV	Replace the Pressure Reducing Valve,
2012	Replace safety valve	Replace worn out safety valves.
2012	Replace slag screen	Replace worn out slag screen.
2012	Replace boiler upper arch refractory	Replace worn out refractory on upper arch.

12.0 Appendix E

Emissions Calculations

**Table DJ - 1
Dave Johnston SO₂ Emissions Evaluation**

PAST ACTUAL MONTHLY SO2 EMISSIONS FROM CEM - TONS

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
313	318	311	321	330	279	317	327	256	336	356	341	339
313	336	330	310	317	265	19	141	335	368	376	396	395
724	780	763	797	657	664	774	653	669	617	667	604	670
491	435	522	521	535	377	459	540	542	560	513	573	386
1841	1869	1926	1949	1839	1585	1568	1661	1803	1881	1913	1914	1790

BASELINE ACTUAL SO2 BASED ON ROLLING 24-MONTH PERIOD - TONS

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
3,500	3,549	3,576	3,591	3,626	3,644	3,657	3,705	3,691	3,762	3,770	3,800	3,842
3,531	3,598	3,638	3,667	3,696	3,713	3,588	3,536	3,550	3,586	3,607	3,649	3,704
8,334	8,356	8,344	8,373	8,379	8,367	8,353	8,305	8,640	8,713	8,691	8,608	8,624
5,175	5,229	5,340	5,420	5,508	5,480	5,470	5,675	5,742	5,800	5,820	5,835	5,786
20,539	20,732	20,898	21,051	21,209	21,204	21,067	21,221	21,622	21,861	21,888	21,892	21,956
Maximum 12 month ave based on 24-month period												21,956

CAPACITY FACTOR % (represents unit's output as a percent of what it's output would have been if the unit had operated at 100% of its cap)

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
91.22	86.57	87.59	94.23	96.10	92.71	93.71	93.96	65.11	88.87	88.25	88.84	90.02
89.11	89.58	89.29	88.25	87.60	83.49	4.84	37.02	84.59	94.50	94.61	94.61	96.30
88.83	93.06	96.47	96.90	84.71	90.89	95.89	96.32	89.11	86.18	91.27	84.56	90.17
89.14	70.79	89.22	86.25	86.57	70.46	82.79	93.54	90.49	90.73	87.85	82.50	64.74

EQUIVALENT AVAILABILITY % (represents what the output of the unit could have provided if there had been demand for the unit's output)

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
95.56	89.69	92.47	96.99	98.32	96.34	96.49	96.31	68.17	92.97	92.32	92.98	93.18
93.85	93.62	94.18	91.76	91.36	88.75	5.47	39.84	87.02	97.57	98.10	98.19	99.10
93.38	94.43	99.49	99.07	87.52	93.26	97.75	98.30	93.21	91.43	95.08	87.64	93.47
91.52	74.04	91.30	88.52	88.72	72.81	85.49	94.97	91.96	92.78	90.07	84.48	68.36

DEMAND GROWTH ADJUSTMENT (Equivalent Availability/Capacity Factor)

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
1.048	1.036	1.056	1.029	1.023	1.039	1.030	1.025	1.047	1.046	1.046	1.047	1.035
1.053	1.045	1.055	1.040	1.043	1.063	1.131	1.076	1.029	1.032	1.037	1.038	1.029
1.051	1.015	1.031	1.022	1.033	1.026	1.019	1.021	1.046	1.061	1.042	1.036	1.037
1.027	1.046	1.023	1.026	1.025	1.033	1.033	1.015	1.016	1.023	1.025	1.024	1.056

MONTHLY SO2 EMISSIONS (capable of accomodating) - TONS

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
328	329	328	330	338	290	327	335	268	352	372	357	351
330	351	348	323	330	282	21	152	345	380	390	411	406
761	791	787	815	679	682	789	667	700	654	695	626	694
504	455	534	534	548	390	474	548	551	573	526	587	408
1,923	1,927	1,997	2,002	1,896	1,643	1,610	1,702	1,865	1,959	1,984	1,981	1,859

ANNUAL SO2 BASED ON ROLLING 24-MONTH PERIOD (capable of accomodating) - TONS

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
3,606	3,657	3,692	3,710	3,745	3,765	3,778	3,825	3,807	3,883	3,893	3,927	3,972
3,703	3,773	3,819	3,851	3,883	3,905	3,757	3,707	3,720	3,755	3,772	3,812	3,867
8,670	8,677	8,669	8,695	8,693	8,678	8,661	8,605	8,955	9,032	9,007	8,913	8,925
5,303	5,367	5,484	5,567	5,661	5,639	5,631	5,836	5,906	5,967	5,988	6,005	5,961
21,282	21,474	21,665	21,823	21,982	21,987	21,826	21,974	22,388	22,636	22,660	22,658	22,724
Maximum 12 month ave based on 24-month period												22,724

DEMAND GROWTH ADJUSTMENT (ANNUAL CAPABLE OF ACCOMODATING HEAT INPUT MINUS PAST ACTUAL HEAT INPUT)

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
251	251	251	251	251	251	251	251	251	251	251	251	251
169	169	169	169	169	169	169	169	169	169	169	169	169
30	30	30	30	30	30	30	30	30	30	30	30	30
262	262	262	262	262	262	262	262	262	262	262	262	262
712	712	712	712	712	712	712	712	712	712	712	712	712
Maximum 12 month ave based on 24-month period												712

**Table DJ - 2
Dave Johnston NOx Emissions Evaluation**

PAST ACTUAL MONTHLY NOx EMISSIONS FROM CEM - TONS

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
203	200	189	220	220	185	212	194	147	193	191	200	194
201	205	186	203	200	167	12	77	179	206	213	213	212
441	477	489	498	423	414	479	459	447	419	446	402	415
543	465	600	606	616	464	357	361	359	317	288	288	212
1389	1346	1464	1526	1459	1230	1060	1091	1133	1135	1138	1102	1032

BASELINE ACTUAL NOx BASED ON ROLLING 24-MONTH PERIOD - TONS

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
2,307	2,332	2,331	2,337	2,343	2,347	2,356	2,362	2,345	2,382	2,379	2,391	2,404
2,316	2,338	2,332	2,347	2,348	2,349	2,266	2,212	2,204	2,222	2,226	2,229	2,237
4,866	4,915	4,933	4,975	4,990	4,991	4,992	4,997	5,221	5,281	5,299	5,267	5,297
5,794	5,790	5,845	5,931	6,008	6,006	5,949	6,065	6,032	5,953	5,836	5,733	5,614
15,283	15,375	15,440	15,589	15,689	15,694	15,562	15,636	15,802	15,838	15,740	15,620	15,553
Maximum 12 month ave based on 24-month period												15,838

CAPACITY FACTOR % (represents unit's output as a percent of what it's output would have been if the unit had operated at 100% o

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
91.22	86.57	87.59	94.23	96.10	92.71	93.71	93.96	65.11	88.87	88.25	88.84	90.02
89.11	89.58	89.29	88.25	87.60	83.49	4.84	37.02	84.59	94.50	94.61	94.61	96.30
88.83	93.06	96.47	96.90	84.71	90.89	95.89	96.32	89.11	86.18	91.27	84.56	90.17
89.14	70.79	89.22	86.25	86.57	70.46	82.79	93.54	90.49	90.73	87.85	82.50	64.74

EQUIVALENT AVAILABILITY % (represents what the output of the unit could have provided if there had been demand for the unit

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
95.56	89.69	92.47	96.99	98.32	96.34	96.49	96.31	68.17	92.97	92.32	92.98	93.18
93.85	93.62	94.18	91.76	91.36	88.75	5.47	39.84	87.02	97.57	98.10	98.19	99.10
93.38	94.43	99.49	99.07	87.52	93.26	97.75	98.30	93.21	91.43	95.08	87.64	93.47
91.52	74.04	91.30	88.52	88.72	72.81	85.49	94.97	91.96	92.78	90.07	84.48	68.36

DEMAND GROWTH ADJUSTMENT (Equivalent Availability/Capacity Factor)

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
1.048	1.036	1.056	1.029	1.023	1.039	1.030	1.025	1.047	1.046	1.046	1.047	1.035
1.053	1.045	1.055	1.040	1.043	1.063	1.131	1.076	1.029	1.032	1.037	1.038	1.029
1.051	1.015	1.031	1.022	1.033	1.026	1.019	1.021	1.046	1.061	1.042	1.036	1.037
1.027	1.046	1.023	1.026	1.025	1.033	1.033	1.015	1.016	1.023	1.025	1.024	1.056

MONTHLY NOx EMISSIONS (capable of accomodating) - TONS

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
213	207	200	227	225	192	218	198	154	202	200	209	201
212	214	196	211	209	178	13	83	184	212	221	221	218
463	484	505	509	437	425	489	468	468	444	465	416	430
558	486	614	622	631	479	368	367	364	324	295	295	223
1,446	1,391	1,514	1,568	1,502	1,274	1,088	1,116	1,171	1,183	1,181	1,141	1,072

ANNUAL NOx BASED ON ROLLING 24-MONTH PERIOD (capable of accomodating) - TONS

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
2,376	2,402	2,406	2,413	2,419	2,424	2,433	2,438	2,418	2,457	2,456	2,470	2,484
2,427	2,451	2,447	2,464	2,467	2,470	2,372	2,319	2,310	2,326	2,328	2,329	2,336
5,060	5,102	5,123	5,164	5,175	5,175	5,173	5,175	5,409	5,472	5,489	5,451	5,480
5,936	5,941	6,003	6,093	6,176	6,182	6,125	6,241	6,208	6,129	6,010	5,906	5,789
15,800	15,896	15,979	16,135	16,237	16,251	16,104	16,172	16,345	16,385	16,283	16,156	16,088
Maximum 12 month ave based on 24-month period												16,385

DEMAND GROWTH ADJUSTMENT (ANNUAL CAPABLE OF ACCOMODATING HEAT INPUT MINUS PAST ACTUAL HEAT

Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
69	70	75	77	76	77	77	76	73	75	77	79	80
111	113	116	117	118	121	106	107	106	104	102	100	99
194	187	190	189	185	184	181	178	188	191	190	185	183
142	151	158	163	169	176	176	176	176	177	175	173	174
516	521	539	546	548	558	542	536	542	547	543	536	535
Maximum 12 month ave based on 24-month period												558

**Table DJ - 4
Coal Burn Adjusted for Equivalent Availability**

MONTHLY ACTUAL COAL BURN (EIA 767) - TONS

Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
45,099	48,903	48,909	45,716	49,295	48,776	35,398	46,861	48,895	49,889	48,173
46,861	48,903	48,909	46,480	2,455	20,077	44,007	46,926	50,043	51,591	50,367
110,701	115,357	100,416	96,652	113,229	106,343	101,930	96,848	104,836	99,237	98,468
148,086	150,881	148,957	111,067	142,659	155,903	152,176	147,093	151,928	145,638	110,130
350,747	364,044	347,191	299,915	307,638	331,098	333,511	488,037	488,037	488,037	488,037

BASELINE ACTUAL COAL BURN BASED ON 24-MONTH ROLLING AVERAGE - TONS

Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
574,940	574,199	574,039	574,480	574,547	575,435	569,167	577,317	574,815	573,802	574,659
564,366	567,652	568,367	569,847	549,164	535,417	532,116	531,876	532,455	534,293	536,594
1,146,177	1,155,406	1,163,072	1,161,962	1,168,204	1,171,878	1,222,843	1,235,999	1,239,640	1,237,472	1,243,998
1,626,212	1,634,781	1,639,161	1,623,583	1,624,308	1,683,040	1,687,581	1,685,743	1,684,307	1,680,900	1,668,119
3,911,694	3,932,038	3,944,638	3,929,872	3,916,223	3,965,770	4,011,708	4,030,935	4,031,217	4,026,467	4,023,370
Maximum 12 month ave based on 24-month period										4,031,217

CAPACITY FACTOR %

Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
87.59	94.23	96.10	92.71	93.71	93.96	65.11	88.87	88.25	88.84	90.02
89.29	88.25	87.60	83.49	4.84	37.02	84.59	94.50	94.61	94.61	96.30
96.47	96.90	84.71	90.89	95.89	96.32	89.11	86.18	91.27	84.56	90.17
89.22	86.25	86.57	70.46	82.79	93.54	90.49	90.73	87.85	82.50	64.74

EQUIVALENT AVAILABILITY %

Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
92.47	96.99	98.32	96.34	96.49	96.31	68.17	92.97	92.32	92.98	93.18
94.18	91.76	91.36	88.75	5.47	39.84	87.02	97.57	98.10	98.19	99.10
99.49	99.07	87.52	93.26	97.75	98.30	93.21	91.43	95.08	87.64	93.47
91.30	88.52	88.72	72.81	85.49	94.97	91.96	92.78	90.07	84.48	68.36

DEMAND GROWTH ADJUSTMENT (Equivalent Availability/Capacity Factor)

Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
1.056	1.029	1.023	1.039	1.030	1.025	1.047	1.046	1.046	1.047	1.035
1.055	1.040	1.043	1.063	1.131	1.076	1.029	1.032	1.037	1.038	1.029
1.031	1.022	1.033	1.026	1.019	1.021	1.046	1.061	1.042	1.036	1.037
1.023	1.026	1.025	1.033	1.033	1.015	1.016	1.023	1.025	1.024	1.056

MONTHLY COAL (CAPABLE OF ACCOMODATING) - TONS

Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
47,615	50,335	50,041	47,510	50,759	49,995	37,061	49,021	51,152	52,214	49,864
49,427	50,848	51,010	49,409	2,775	21,607	45,274	48,449	51,885	53,543	51,831
114,164	117,941	103,753	99,174	115,425	108,529	106,619	102,752	109,221	102,852	102,072
151,533	154,846	152,651	114,771	147,303	158,287	154,653	150,419	155,778	149,133	116,288
362,739	373,969	357,454	310,864	316,262	338,419	343,608	350,642	368,036	357,742	320,055
Maximum 12 month ave based on 24-month period										373,969

ANNUAL COAL BURN BASED ON 24-MONTH ROLLING AVERAGE (CAPABLE OF ACCOMODATING) - TONS

Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
593,380	593,044	592,690	593,426	593,484	593,926	586,846	595,481	593,327	592,672	593,779
592,400	596,042	597,028	599,405	574,964	561,297	557,698	556,917	556,902	558,297	560,361
1,189,993	1,198,905	1,205,768	1,204,347	1,210,271	1,213,177	1,266,486	1,280,319	1,283,669	1,280,484	1,286,515
1,668,898	1,678,439	1,684,201	1,670,125	1,671,710	1,730,582	1,735,465	1,734,370	1,733,177	1,730,056	1,718,818
4,044,671	4,066,429	4,079,688	4,067,302	4,050,429	4,098,982	4,146,495	4,167,087	4,167,075	4,161,508	4,159,473
Maximum 12 month ave based on 24-month period										4,167,087

DEMAND GROWTH ADJUSTMENT (ANNUAL CAPABLE OF ACCOMODATING MINUS PAST ACTUAL TONS)

Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
18,440	18,844	18,651	18,946	18,937	18,490	17,679	18,164	18,512	18,869	19,120
28,035	28,390	28,662	29,558	25,800	25,880	25,582	25,041	24,447	24,005	23,767
43,816	43,499	42,696	42,385	42,067	41,299	43,643	44,320	44,029	43,011	42,518
42,686	43,658	45,041	46,542	47,402	47,542	47,884	48,627	48,870	49,156	50,698
132,977	134,391	135,050	137,430	134,207	133,212	134,788	136,152	135,858	135,041	136,103
Maximum 12 month ave based on 24-month period										137,430

**Table DJ - 5
Dave Johnston PM Emissions Evaluation**

PAST ACTUAL MONTHLY Heat Input from CEM- MMBtu

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
882,222	669,094	843,247	871,993	887,351	857,352
373,565	850,987	908,999	950,525	959,272	935,049
1,816,071	1,777,689	1,666,793	1,844,154	1,702,079	1,738,721
3,140,705	3,116,798	2,958,429	2,966,380	2,877,134	1,985,973
6,212,563	6,414,568	6,377,468	6,633,051	6,425,837	5,517,095

MONTHLY PM EMISSION RATES lb/MMBtu (average 1999-2006 Method 5 te

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
0.005	0.005	0.005	0.005	0.005	0.005
0.005	0.002	0.002	0.002	0.002	0.002
0.005	0.013	0.013	0.013	0.013	0.013
0.081	0.081	0.081	0.081	0.098	0.098

BASELINE ACTUAL PM EMISSIONS (calculated by multiplying monthly HI by

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
2	2	2.1	2	2	2
1	1	1	1	1	1
5	12	11	12	11	11
127	126	120	120	141	97
135	140	134	135	155	112

PAST ACTUAL ANNUAL PM EMISSIONS - TONS (24-month average div

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
124	115	110	100	92	83
29	28	27	25	24	23
79	85	86	87	87	87
1,149	1,159	1,159	1,155	1,185	1,197
1,381	1,386	1,382	1,368	1,387	1,391

Maximum 12 month ave based on 24-month period 2,049

CAPACITY FACTOR % (represents unit's output as a percent of what it's

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
93.96	65.11	88.87	88.25	88.84	90.02
37.02	84.59	94.50	94.61	94.61	96.30
96.32	89.11	86.18	91.27	84.56	90.17
93.54	90.49	90.73	87.85	82.50	64.74

EQUIVALENT AVAILABILITY % (represents what the output of the unit cc

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
96.31	68.17	92.97	92.32	92.98	93.18
39.84	87.02	97.57	98.10	98.19	99.10
98.30	93.21	91.43	95.08	87.64	93.47
94.97	91.96	92.78	90.07	84.48	68.36

DEMAND GROWTH ADJUSTMENT (Equivalent Availability/Capacity Facto

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
1.025	1.047	1.046	1.046	1.047	1.035
1.076	1.029	1.032	1.037	1.038	1.029
1.021	1.046	1.061	1.042	1.036	1.037
1.015	1.016	1.023	1.025	1.024	1.056

MONTHLY PM EMISSIONS (CAPABLE OF ACCOMODATING) - TONS

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
2	2	2	2	2	2
1	1	1	1	1	1
5	12	11	12	11	12
129	128	123	123	144	103
137	143	137	139	159	118

ANNUAL PM EMISSIONS (CAPABLE OF ACCOMODATING) - TONS

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
127	118	112	102	93	85
30	29	28	27	25	24
82	88	90	90	89	90
1,181	1,191	1,192	1,188	1,219	1,233
1,420	1,425	1,421	1,407	1,427	1,433

Maximum Demand Growth Adjustment 2,105

DEMAND GROWTH ADJUSTMENT (ANNUAL CAPABLE OF ACCOMODAT

Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
3	3	2	2	2	2
1	1	1	1	1	1
3	3	3	3	3	3
32	32	33	33	34	36
39	39	40	39	40	41

Maximum Demand Growth Adjustment 58

Table DJ-6 Dave Johnston Non-Stack PM₁₀ Emission

Data from 2002-2006 Emissions Inventories submitted to Wyoming DEQ

	2002	2003	2004	2005	2006
Description of Emission Unit	(tons/yr)	(tons/yr)	(tons/yr)	(tons/yr)	(tons/yr)
1R Feeder, 1 & 11 Conveyors (#1 Track Hopper)	0.0	0.0			
25 Feeder & 25 Conveyor (#2 Track Hopper)	0.0	0.0			
31 & 32 Conveyors, 31 Feeder (#1 Ready Pile)	0.0	0.0			
34 & 34 Conveyors, 33 Feeder (#2 Ready Pile)	0.3	0.2	0.2	0.2	0.18
35 Conveyor, 35 Feeder (#3 Ready Pile)	0.0	0.0	0.0	0.0	0.0
1A Tripper Deck Dust Collector	0.0	0.0	0.0	0.0	0.03
1B Tripper Deck Dust Collector	0.0	0.0	0.0	0.0	0.03
2A Tripper Deck Dust Collector	0.0	0.0	0.0	0.0	0.02
2B Tripper Deck Dust Collector	0.0	0.0	0.0	0.0	0.01
3 Tripper Deck, Conveyor 53	0.4	0.4	0.4	0.4	0.40
3 Tripper Deck, Conveyor 43 discharge & Conveyor 53	1.4	1.5	1.5	1.4	1.59
4A Tripper Deck, Conveyor 55A & Coal Silos	1.8	1.6	1.9	1.9	1.94
4B Tripper Deck, Conveyor 55B, 54B & Coal Silos	1.4	1.2	1.4	1.4	1.46
4 Tripper Deck, Feeders & Conveyors 54A, 54B & 55A	5.8	5.0	6.1	6.1	6.17
Rail Car Load-In Facility (East baghouse)	1.14	1.03	0.99	1.13	1.18
Rail Car Load-In Facility (West baghouse)	1.45	1.30	1.25	1.43	1.49
Overland Conveyor	0.00	0.00	0.00	0.00	0.00
Radial Stacker	0.00	0.00	0.00	0.00	0.00
Coal conveyors & transfer fugitive emissions	0.1	0.0	0.0	0.1	0.05
Active Coal piles fugitive emissions	24.8	24.8	24.8	31.1	31.06
Inactive Coal piles fugitive emissions	19.9	19.9	19.9	24.8	24.85
Fly ash silo truck loading	0.2	0.2	0.1	0.1	0.13
Ash haul road	2.8	2.7	1.9	1.8	1.99
Ash dumping at landfill	0.2	0.2	0.1	0.1	0.13
Ash landfill, wind erosion	56.8	56.8	56.8	71.0	70.99
Cooling tower Units 1,2,3	15.1	14.8	14.9	15.9	16.46
Cooling tower Unit #4	145.4	125.0	146.0	143.4	149.35
Unit 4 Lime Silo Baghouse	0.7	0.6	0.7	0.7	0.72
Emergency diesel generator Units 1, 2, & 3	0.03	0.03	0.03	0.06	0.06
Emergency diesel generator Units 4	0.02	0.02	0.02	0.05	0.05
Scrubber emergency diesel generator Unit 4	0.02	0.02			
Diesel fire water booster pump	0.01	0.01	0.01	0.01	0.01
Total PM₁₀	280	257	279	303	310
Maximum Non-stack PM₁₀	310				

Table DJ-7
Dave Johnston CO Emissions Evaluation

Carbon Monoxide emission Factor AP-42, Table 1.1-3, 9/98 0.5 lb/ton
 CO emissions (tons/year) = EPA emission factor * coal consumption

CO Emissions (tons/year)

Baseline Actual annual coal consumption (based on past actual annual coal consumption, Table DJ-4)	4,031,217	Past Actual CO Emissions	1,008	tons/year
Potential to Emit coal consumption (based on potential past actual annual coal consumption, Table DJ-4))	4,167,087	Potential to Emit CO Emissions	1,042	tons/year

	Projected Actual coal consumption (based on coal burned adjusted for 100% capacity factor, Table DJ-7)	Maximum Hourly Heat Input	Projected CO Emission Rate lb/MMBtu	Projected CO Emission, tons/yr
Dave Johnston 1	629,819	--- calculated using AP-42 Emission factor --->		157
Dave Johnston 2	637,664	--- calculated using AP-42 Emission factor --->		159
Dave Johnston 3		2,800	0.25	3,066
Dave Johnston 4		4,700	0.20	4,117
Dave Johnston total				7,500

Table DJ-8
Dave Johnston VOC Emissions Evaluation

VOC emission Factor AP-42, Table 1.1-3, 9/98 0.06 lb/ton
 VOC emissions (tons/year) = EPA emission factor * coal consumption

Equation for Calculating Plant VOC Emissions:

(AP-42 VOC Emission Factor (lbs VOC/tons of coal burned))*(tons of coal burned/year)*(1 ton/2000 lbs) = tons of VOC emitted/year

Past VOC Emissions (tons/year)

Baseline Actual annual coal consumption (based on past actual annual coal consumption, Table DJ-4)	4,031,217	Past Actual VOC Emissions	121	tons/year
Potential to Emit annual coal consumption (based on potential past actual annual coal consumption, Table DJ-4)	4,167,087	EA adjusted VOC Emissions	125	tons/year
Projected Actual annual coal consumption (based on coal burned adjusted for 100% capacity factor, Table DJ-13)	4,635,894	EA adjusted VOC Emissions	139	tons/year

Table DJ-9 Dave Johnston Lead Emissions Evaluation

Lead emissions calculated using AP-42 Table 1.1-16 9/98

$$\text{Lead emissions (lb/year)} = 3.4 * (C/A * PM)^{0.80} * HI$$

C = 2.33 milligrams/kilogram (lead concentration in coal) (Coal trace element analyses, 2003)

A = 5% (percent ash in coal) (Coal trace element analyses, 2003)

PM = Average particulate matter emission rate (DJ-5)

HI = heat input (DJ-3)

Baseline Actual (tons/year)

Plant Name	Heat Input MMBtu/year ¹	lbs/yr	tons/yr
Dave Johnston 1	10,289,006	120	0.06
Dave Johnston 2	9,794,125	41	0.02
Dave Johnston 3	20,865,552	109	0.05
Dave Johnston 4	34,666,434	364	0.18
Dave Johnston total	75,615,117	635	0.32

Average PM ₁₀ Emission Rates for Highest Heat Input 24 month period (DJ-5)
0.100
0.028
0.037
0.088

¹ DJ-3 Heat Input

Potential to Emit (tons/year)

Plant Name	Heat Input MMBtu/year ²	lbs/yr	tons/yr
Dave Johnston 1	10,619,911	123	0.06
Dave Johnston 2	10,242,581	43	0.02
Dave Johnston 3	21,612,788	113	0.06
Dave Johnston 4	35,675,919	375	0.19
Dave Johnston total	78,151,199	655	0.33

Average PM ₁₀ Emission Rates for Highest Heat Input 24 month period (DJ-5)
0.100
0.028
0.037
0.088

² DJ-3 Heat Input, Capable of Accomodating

Projected Actual (tons/year)

	Projected Actual Heat Input at 100% Capacity Factor MMBtu/yr	lbs/yr	tons/yr
Dave Johnston 1 ³	11,340,026	169	0.08
Dave Johnston 2 ³	11,780,692	79	0.04
Dave Johnston 3 ⁴	24,528,000	63	0.03
Dave Johnston 4 ⁵	41,172,000	105.11	0.05
Dave Johnston total	88,820,719	415.4	0.21

Predicted PM Emission Rate lb/MMBtu ^a (U1/2-Max PM from Testing) (U3/4-Predicted PM)
0.136
0.050
0.015
0.015

³ Table DJ-6, Heat Input at 100% Capacity Factor

⁴ Maximum Heat Input = 2800 MMBtu/hr

⁵ Maximum Heat Input = 4700 MMBtu/hr

Table DJ - 10
Dave Johnston Fluoride Emissions Evaluation

$$M_{HF} = F_{comb} \times 2000 \text{ lb/ton} \times C_{HF} \times 1/10^6 \times F_{acid}$$

Where:

M_{HF} =	Manufacture of Hydrogen Fluoride, lb/year	
F_{comb} =	Coal combustion, tons/year	
F_{comb} =	574,815 tons/year (Unit 1)	Note: Maximum annual coal burn rates Table DJ-4
F_{comb} =	532,455 tons/year (Unit 2)	
F_{comb} =	1,239,640 tons/year (Unit 3)	
F_{comb} =	1,684,307 tons/year (Unit 4)	
C_{HF} =	60.33	Fluoride concentration in coal, ppm (concentration occurring during maximum coal consumption period)
F_{acid} =	M_{HF}/M_F	Acid conversion factor: ratio of molecular weights, compound/parent chemical
M_F =	18.9984	Molecular weight of fluorine
M_{HF} =	20.0063	Molecular weight of hydrogen fluoride
F_{acid} =	1.053053932	
AR =	Annual release of hydrogen fluoride, lb/year	
E_{HF} =	90%	HF emission factor for bituminous coal
E_{FGD} =	6%	HF emission factor for FGD systems
$E_{No FGD}$ =	50%	HF emission factor without FGD, sub bituminous
$AR_{FGD \text{ Removal}}$ =	$(1.0 - F_{Bypass}) \times E_{FGD} \times M_{HF}$	
AR_{Bypass} =	$F_{Bypass} \times E_{No FGD} \times M_{HF}$	
AR_{Total} =	$AR_{FGD \text{ Removal}} + AR_{Bypass}$	

Historical Coal Fluoride Concentrations (Parts Per Million)
(From Emission Tables)

	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	Highest 1996-2006 Fluoride Concentration (ppm)
DJ-1				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-2				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-3				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-4				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33

Calculation Method:

EPRI LARK-TRIPP *Calculation and Methods for Threshold Determination and Release Estimates*
HF Emission Factor with FGD System: 6%
Bituminous Coal Emission Factor: 90%
(Table 5-1 Emission Factors for HCL and HF)

Maximum Annual Coal Burn Rate

	Annual Coal Burn Rate
DJ-1	574,815
DJ-2	532,455
DJ-3	1,239,640
DJ-4	1,684,307

Note: Maximum annual coal burn rates
Table DJ-4

U1: F_{Bypass} =	0.00	(0% Scrubber Bypass)
U2: F_{Bypass} =	0.00	(0% Scrubber Bypass)
U3: F_{Bypass} =	0.00	(0% Scrubber Bypass)
U4: F_{Bypass} =	0.00	(0% Scrubber Bypass)

M_{HF} =	36.5	tons/year (Unit 1 HF manufacture)
M_{HF} =	33.8	tons/year (Unit 2 HF manufacture)
M_{HF} =	78.8	tons/year (Unit 3 HF manufacture)
M_{HF} =	107.0	tons/year (Unit 3 HF manufacture)

$$AR_{No FGD \text{ Removal}} = (1.0 - F_{Bypass}) \times E_{No FGD} \times M_{HF}$$

$$AR_{FGD \text{ Removal}} = (1.0 - F_{Bypass}) \times E_{FGD} \times M_{HF}$$

$AR_{No FGD \text{ Removal}}$ =	18.3	tons/year Unit 1 stack air release
$AR_{No FGD \text{ Removal}}$ =	16.9	tons/year Unit 2 stack air release
$AR_{No FGD \text{ Removal}}$ =	39.4	tons/year Unit 3 stack air release
$AR_{FGD \text{ Removal}}$ =	6.4	tons/year Unit 4 stack air release

AR_{Total} = 81.0 tons/year (Baseline Actual Hydrogen Fluoride Emissions)

DJ-11
Dave Johnston H2SO4 Emissions Evaluation
Baseline Actual

Facility: Dave Johnston																									
Emission Unit: Steam generating unit (primary fuel, coal)																									
ID # : 1, 2, 3, & 4																									
<table border="1"> <thead> <tr> <th colspan="3">H₂SO₄ Summary</th> </tr> <tr> <th></th> <th>(lbs/yr)</th> <th>(tons/yr)</th> </tr> </thead> <tbody> <tr> <td>Unit 1</td> <td>8,659</td> <td>4.3</td> </tr> <tr> <td>Unit 2</td> <td>8,349</td> <td>4.2</td> </tr> <tr> <td>Unit 3</td> <td>19,438</td> <td>9.7</td> </tr> <tr> <td>Unit 4</td> <td>7,145</td> <td>3.6</td> </tr> <tr> <td>Total</td> <td>43,591</td> <td>21.8</td> </tr> </tbody> </table>					H ₂ SO ₄ Summary				(lbs/yr)	(tons/yr)	Unit 1	8,659	4.3	Unit 2	8,349	4.2	Unit 3	19,438	9.7	Unit 4	7,145	3.6	Total	43,591	21.8
H ₂ SO ₄ Summary																									
	(lbs/yr)	(tons/yr)																							
Unit 1	8,659	4.3																							
Unit 2	8,349	4.2																							
Unit 3	19,438	9.7																							
Unit 4	7,145	3.6																							
Total	43,591	21.8																							
	Unit 1	Unit 2	Unit 3	Unit 4																					
SO ₂ from CEM, tons (SO ₂ emissions from DJ-1)	3,841.7	3,704.4	8,624.1	5,785.8																					
SCR	N	N	N	N																					
FGC SO ₃ Injection	N	N	N	N																					
Next use Eqn. 5-8 to determine the total quantity of H ₂ SO ₄ manufactured from combustions, E1 Fuel Impact Factors, F1, are obtained from Table 1 of Appendix B.																									
E1 = K x F1 x E2																									
K, molecular weight and units conversion constant	3063	3063	3063	3063																					
F1 _{coal} , Sub. PC Boiler	0.0018	0.0018	0.0018	0.0018																					
E2, Sulfur dioxide emissions, CEM	3,841.7	3,704.4	8,624.1	5,785.8																					
E1_{total}	21,181.1	20,423.8	47,548.0	31,899.2																					
Next use Eqn. 5-9 to determine the quantity of H ₂ SO ₄ released, E1' Technology Impact Factor, F2, are found in Table 3 of Appendix B.																									
E1' _{comb} = K x F1 x E2 x F2 _x																									
F2 _x , F2 for applicable F2 _s other than scrubber																									
F2 _x for Air preheater - wstrn sub	0.56	0.56	0.56	0.56																					
F2 _x for Cold Side ESP	0.73	0.73	0.73	1																					
F2 _x for Wet Spray Tower, PRB, Lignite	1	1	1	0.4																					
E1'_{comb}	8,658.8	8,349.3	19,437.6	7,145.4																					

DJ-11
Dave Johnston H2SO4 Emissions Evaluation
Potential to Emit

Facility: Dave Johnston																									
Emission Unit: Steam generating unit (primary fuel, coal)																									
ID # : 1, 2, 3, & 4																									
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H ₂ SO ₄ Summary																									
	(lbs/yr)	(tons/yr)																							
Unit 1	8,952	4.5																							
Unit 2	8,716	4.4																							
Unit 3	20,115	10.1																							
Unit 4	7,362	3.7																							
Total	45,145	22.6																							
	Unit 1	Unit 2	Unit 3	Unit 4																					
SO ₂ from CEM, tons(SO ₂ emissions from DJ-1)	3,971.7	3,867.2	8,924.6	5,961.0																					
SCR	N	N	N	N																					
FGC SO ₃ Injection	N	N	N	N																					
Next use Eqn. 5-8 to determine the total quantity of H ₂ SO ₄ manufactured from combustions, E1 Fuel Impact Factors, F1, are obtained from Table 1 of Appendix B.																									
E1 = K x F1 x E2																									
K, molecular weight and units conversion constant	3063	3063	3063	3063																					
F1 _{coal} , Sub. PC Boiler	0.0018	0.0018	0.0018	0.0018																					
E2, Sulfur dioxide emissions, CEM	3,971.7	3,867.2	8,924.6	5,961.0																					
E1_{total}	21,897.4	21,321.3	49,205.0	32,865.3																					
Next use Eqn. 5-9 to determine the quantity of H ₂ SO ₄ released, E1' Technology Impact Factor, F2, are found in Table 3 of Appendix B.																									
E1' _{comb} = K x F1 x E2 x F2 _x																									
F2 _x , F2 for applicable F2 _s other than scrubber																									
F2 _x for Air preheater - wstrn sub	0.56	0.56	0.56	0.56																					
F2 _x for Cold Side ESP	0.73	0.73	0.73	1																					
F2 _x for Wet Spray Tower, PRB, Lignite	1	1	1	0.4																					
E1'_{comb}	8,951.7	8,716.2	20,115.0	7,361.8																					

DJ-11
Dave Johnston H2SO4 Emissions Evaluation
Projected Actual

Facility: Dave Johnston																									
Emission Unit: Steam generating unit (primary fuel, coal)																									
ID # : 1, 2, 3, & 4																									
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H ₂ SO ₄ Summary																									
	(lbs/yr)	(tons/yr)																							
Unit 1	9,560	5																							
Unit 2	9,955	5																							
Unit 3	322	0																							
Unit 4	422	0																							
Total	20,259	10																							
	Unit 1	Unit 2	Unit 3	Unit 4																					
E2, SO ₂ from CEM, tons (DJ-17, SO ₂ Emissions adjusted for 100%	4,241.6	4,416.9	-	-																					
SO ₂ Production Estimated from Fuel Burn Data																									
E2=K1 x K2 x C1 x S1																									
C1=Fuel Burn, tons/yr (DJ-13, Coal burned, adjusted for 100% C	-	-	1,370,479	1,997,932																					
S1=Fuel sulfur weighted average, %	-	-	0.40	0.36																					
K1=Molecular weight, 0.02	-	-	0.02	0.02																					
K2=Sulfur Conversion to SO ₂ for Bituminous coals	-	-	0.95	0.95																					
E2=SO ₂ from Coal Burned tons	-	-	10,415.64	13,665.85																					
SCR	N	N	N	N																					
FGC SO ₃ Injection	N	N	Y	Y																					
Next use Eqn. 5-8 to determine the total quantity of H ₂ SO ₄ manufactured from combustions, E1 Fuel Impact Factors, F1, are obtained from Table 4-1.																									
E1 = K x F1 x E2																									
K, molecular weight and units conversion constant	3063	3063	3063	3063																					
F1 _{coal} , Sub. PC Boiler	0.0018	0.0018	0.0018	0.0018																					
E2, Sulfur dioxide emissions	4,241.6	4,416.9	10,415.6	13,665.9																					
E1_{total}	23,385.4	24,352.1	57,425.6	75,345.3																					
Next use Eqn. 5-9 to determine the quantity of H ₂ SO ₄ released, E1' Technology Impact Factor, F2, are found in Table 3 of Appendix B.																									
E1' _{comb} = [SBf + (1 - SBf) x F2s] x K x F1 x E2 x F2 _x																									
SB _f , FGD Bypass, fraction	1	1	1	1																					
F2 _s , F2 for Scrubber	0.5	0.5	0.5	0.5																					
F2 _x , F2 for applicable F2 _s other than scrubber																									
F2 _x for Air preheater - wstrn sub	0.56	0.56	0.56	0.56																					
F2 _x for Cold Side ESP	0.73	0.73	1	1																					
F2 _x for Dry FGD and Baghouse	1	1	0.01	0.01																					
F2 _x for Wet Scrubber	1	1	1	1																					
E1'_{comb}	9,559.9	9,955.1	321.6	421.9																					

Weight percent sulfur in coal, %	Emission Data Summary Sheets					
	2002	2003	2004	2005	2006	Maximum
Unit 3	0.33	0.37	0.4	0.4	0.4	0.4
Unit 4	0.34	0.35	0.32	0.36	0.36	0.36

PAST ACTUAL MONTHLY Heat Input from CEM- MMBtu

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	856,431	844,024	859,980	796,191	771,495	830,992	794,081	790,058	755,565	705,789	814,907	636,508	64,361	865,233	898,989	850,065	839,265	889,113	761,050	854,608	510,887	768,919
Dave Johnston 2	795,108	865,625	896,770	893,942	822,671	876,102	850,915	870,506	818,261	865,149	824,134	852,348	727,099	807,422	780,342	853,560	805,081	847,368	490,199	891,457	830,876	823,457
Dave Johnston 3	1,804,474	1,821,648	1,715,572	1,778,662	1,644,492	1,132,635	1,422,374	1,099,774	1,822,212	1,763,400	1,701,982	1,755,382	1,852,475	1,765,454	1,792,281	1,728,809	1,704,463	983,972	1,590,540	1,621,163	1,767,719	1,700,796
Dave Johnston 4	2,410,268	2,165,148	2,641,791	2,893,136	2,067,922	1,900,922	0	1,718,614	1,766,980	2,387,031	2,211,376	2,809,332	2,851,882	2,595,128	2,876,375	2,518,036	2,581,635	2,869,238	2,678,826	2,500,662	2,286,693	2,235,030
Dave Johnston Totals	5,866,281	5,696,445	6,114,113	6,361,931	5,306,580	4,740,651	3,067,370	4,478,952	5,163,018	5,721,369	5,552,399	6,053,570	5,495,817	6,033,237	6,347,987	5,950,470	5,930,444	5,589,691	5,520,615	5,867,890	5,396,175	5,528,202

PAST ACTUAL ANNUAL HEAT INPUT(based on 24-Month Rolling Average) - MMBtu

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 2	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 3	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 4	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston Totals																						

CAPACITY FACTOR % (represents unit's output as a percent of what it's output would have been if the unit had operated at 100% of its capacity over the period being evaluated)

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	91.60	93.95	92.29	84.38	91.11	89.77	89.23	84.36	85.65	76.40	87.32	78.84	5.83	99.99	99.41	92.62	97.68	97.80	86.75	92.41	60.20	88.96
Dave Johnston 2	94.78	94.78	94.14	93.07	94.59	91.36	92.33	87.90	91.23	89.38	84.09	92.28	79.72	94.76	94.05	92.38	90.96	93.03	55.12	96.31	94.01	88.75
Dave Johnston 3	95.34	98.78	87.94	91.77	94.80	57.59	77.31	56.25	96.07	89.22	86.37	93.57	96.63	95.78	91.95	88.74	94.47	49.16	83.47	81.95	93.12	84.27
Dave Johnston 4	80.32	71.23	83.82	92.10	71.58	58.10	-0.27	55.90	60.72	80.43	67.90	94.44	93.23	89.00	92.83	78.96	89.19	96.56	93.55	85.16	77.37	74.63

CORRECTION TO 100% CAPACITY FACTOR [(1/CAPACITY FACTOR)*100]

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	1.09	1.06	1.08	1.19	1.10	1.11	1.12	1.19	1.17	1.31	1.15	1.27	17.15	1.00	1.01	1.08	1.02	1.02	1.15	1.08	1.66	1.12
Dave Johnston 2	1.06	1.06	1.06	1.07	1.06	1.09	1.08	1.14	1.10	1.12	1.19	1.08	1.25	1.06	1.06	1.08	1.10	1.07	1.81	1.04	1.06	1.13
Dave Johnston 3	1.05	1.01	1.14	1.09	1.05	1.74	1.29	1.78	1.04	1.12	1.16	1.07	1.03	1.04	1.09	1.13	1.06	2.03	1.20	1.22	1.07	1.19
Dave Johnston 4	1.25	1.40	1.19	1.09	1.40	1.72	-370.73	1.79	1.65	1.24	1.47	1.06	1.07	1.12	1.08	1.27	1.12	1.04	1.07	1.17	1.29	1.34

MONTHLY HEAT INPUT (100% CAPACITY FACTOR) - MMBtu

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	934,975	898,346	931,818	943,584	846,766	925,654	889,923	936,513	882,155	923,794	933,202	807,337	1,103,711	865,290	904,344	917,796	859,167	909,078	877,247	924,829	848,624	864,384
Dave Johnston 2	838,918	913,300	952,574	960,554	869,689	958,944	921,646	990,343	896,930	967,981	980,028	923,642	912,093	852,069	829,705	924,011	885,142	910,857	889,334	925,623	883,859	927,849
Dave Johnston 3	1,892,603	1,844,117	1,950,751	1,938,085	1,734,762	1,966,770	1,839,861	1,955,281	1,896,815	1,976,413	1,970,646	1,875,957	1,917,075	1,843,148	1,949,097	1,948,142	1,804,218	2,001,647	1,905,521	1,978,290	1,898,299	2,018,345
Dave Johnston 4	3,000,888	3,039,612	3,151,818	3,141,311	2,889,017	3,271,630	0	3,074,548	2,910,202	2,967,803	3,256,678	2,974,786	3,059,054	2,915,916	3,098,394	3,188,814	2,894,528	2,971,545	2,863,615	2,936,552	2,955,547	2,994,938
Dave Johnston Totals	6,667,385	6,695,376	6,986,961	6,983,534	6,340,234	7,122,998	3,651,430	6,956,686	6,586,103	6,835,990	7,140,555	6,581,722	6,991,934	6,476,422	6,781,540	6,978,764	6,443,055	6,793,127	6,535,716	6,765,294	6,586,330	6,805,517

ANNUAL HEAT INPUT (100% CAPACITY FACTOR) - MMBtu

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 2	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 3	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 4	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston Totals																						

Table DJ - 13

Dave Johnston Coal Burn Adjusted for 100% Capacity Factor

PAST ACTUAL MONTHLY COAL BURN from CEM- MMBtu

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	51,837	50,275	51,063	49,092	47,399	48,817	46,448	46,420	43,570	41,192	48,151	38,260	4,636	48,907	51,396	46,875	47,460	49,313	42,774	48,697	30,351	47,522
Dave Johnston 2	52,512	50,920	52,195	55,255	49,171	50,611	47,845	48,372	45,762	47,028	44,884	46,786	40,194	45,595	47,527	46,675	45,042	45,703	27,493	49,720	47,789	47,165
Dave Johnston 3	102,041	103,313	94,331	101,430	93,019	60,860	75,434	58,487	98,129	105,220	101,300	101,476	112,414	107,172	100,185	94,867	100,518	57,289	87,027	94,042	97,711	94,639
Dave Johnston 4	129,795	110,857	136,111	150,726	101,328	92,278	0	92,864	91,297	123,755	106,820	143,721	148,054	130,220	142,954	118,440	127,425	149,676	140,930	136,329	119,004	124,604
Dave Johnston Totals	336,185	315,365	333,700	356,503	290,917	252,565	169,727	246,144	278,758	317,195	301,155	330,243	305,298	331,894	342,062	306,858	320,445	301,981	298,224	328,788	294,855	313,930

PAST ACTUAL ANNUAL COAL BURN (based on 24-Month Rolling Average) - MMBtu

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 2	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 3	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 4	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston Totals																						

CAPACITY FACTOR % (represents unit's output as a percent of what it's output would have been if the unit had operated at 100% of its capacity over the period being evaluated)

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	91.60	93.95	92.29	84.38	91.11	89.77	89.23	84.36	85.65	76.40	87.32	78.84	5.83	99.99	99.41	92.62	97.68	97.80	86.75	92.41	60.20	88.96
Dave Johnston 2	94.78	94.78	94.14	93.07	94.59	91.36	92.33	87.90	91.23	89.38	84.09	92.28	79.72	94.76	94.05	92.38	90.96	93.03	55.12	96.31	94.01	88.75
Dave Johnston 3	95.34	98.78	87.94	91.77	94.80	57.59	77.31	56.25	96.07	89.22	86.37	93.57	96.63	95.78	91.95	88.74	94.47	49.16	83.47	81.95	93.12	84.27
Dave Johnston 4	80.32	71.23	83.82	92.10	71.58	58.10	-0.27	55.90	60.72	80.43	67.90	94.44	93.23	89.00	92.83	78.96	89.19	96.56	93.55	85.16	77.37	74.63

CORRECTION TO 100% CAPACITY FACTOR [(1/CAPACITY FACTOR)*100]

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	1.09	1.06	1.08	1.19	1.10	1.11	1.12	1.19	1.17	1.31	1.15	1.27	17.15	1.00	1.01	1.08	1.02	1.02	1.15	1.08	1.66	1.12
Dave Johnston 2	1.06	1.06	1.06	1.07	1.06	1.09	1.08	1.14	1.10	1.12	1.19	1.08	1.25	1.06	1.06	1.08	1.10	1.07	1.81	1.04	1.06	1.13
Dave Johnston 3	1.05	1.01	1.14	1.09	1.05	1.74	1.29	1.78	1.04	1.12	1.16	1.07	1.03	1.04	1.09	1.13	1.06	2.03	1.20	1.22	1.07	1.19
Dave Johnston 4	1.25	1.40	1.19	1.09	1.40	1.72	-370.73	1.79	1.65	1.24	1.47	1.06	1.07	1.12	1.08	1.27	1.12	1.04	1.07	1.17	1.29	1.34

MONTHLY COAL BURN (100% CAPACITY FACTOR) - MMBtu

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	56,591	53,511	55,329	58,180	52,024	54,378	52,054	55,026	50,870	53,915	55,141	48,528	79,502	48,910	51,702	50,610	48,585	50,420	49,305	52,698	50,415	53,422
Dave Johnston 2	55,405	53,724	55,443	59,372	51,982	55,396	51,822	55,031	50,162	52,618	53,374	50,699	50,420	48,116	50,533	50,528	49,522	49,128	49,879	51,626	50,836	53,144
Dave Johnston 3	107,025	104,587	107,262	110,521	98,125	105,680	97,575	103,984	102,147	117,930	117,291	108,446	116,334	111,888	108,951	106,903	106,401	116,540	104,261	114,759	104,929	112,309
Dave Johnston 4	161,600	155,630	162,389	163,655	141,561	158,817	0	166,132	150,365	153,865	157,313	152,185	158,809	146,317	153,988	149,991	142,869	155,013	150,652	160,092	153,812	166,969
Dave Johnston Totals	380,621	367,453	380,423	391,729	343,691	374,271	201,451	380,172	353,544	378,328	383,119	359,859	405,065	355,231	365,175	358,032	347,377	371,101	354,096	379,175	359,993	385,844

ANNUAL COAL BURN (100% CAPACITY FACTOR) - MMBtu

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04	Jul-04
Dave Johnston 1	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 2	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 3	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston 4	This is based on a 24-month rolling average so there are no valid averages until September 2004																					
Dave Johnston Totals																						

Table DJ - 13

Dave Johnston Coal Burn Adjusted for 100% Capacity Factor

PAST ACTUAL MONTHLY COAL BURN from CEM- MMBtu

PAST ACTUAL MONTHLY COAL BURN from CEM- MMBtu

Table with 17 columns (months May-06 to Sep-07) and 5 rows of monthly coal burn data from May-06 to Sep-06.

PAST ACTUAL ANNUAL COAL BURN (based on 24-Month Rolling Average) - MMBtu

PAST ACTUAL ANNUAL COAL BURN (based on 24-Month Rolling Average) - MMBtu

Table with 17 columns (months May-06 to Sep-07) and 5 rows of annual coal burn data from May-06 to Sep-06.

Maximum 12 month ave based on 24-month period 4,031,217

CAPACITY FACTOR % (represents unit's output as a percent of what it's output would have been if the unit had operated at 100% of its capacity over the period being evaluated)

Table with 17 columns (months May-06 to Sep-07) and 5 rows of capacity factor data from May-06 to Sep-06.

CAPACITY FACTOR % (represents unit's output as a percent of what it's output would have been if the unit had operated at 100% of its capacity over the period being evaluated) CORRECTION TO 100% CAPACITY FACTOR [(1/CAPACITY FACTOR)*100]

Table with 17 columns (months May-06 to Sep-07) and 5 rows of capacity factor correction data from May-06 to Sep-06.

MONTHLY COAL BURN (100% CAPACITY FACTOR) - MMBtu

MONTHLY COAL BURN (100% CAPACITY FACTOR) - MMBtu

Table with 17 columns (months May-06 to Sep-07) and 5 rows of monthly coal burn data at 100% capacity factor from May-06 to Sep-06.

Maximum monthly ave based on 24-month period 404,574

ANNUAL COAL BURN (100% CAPACITY FACTOR) - MMBtu

ANNUAL COAL BURN (100% CAPACITY FACTOR) - MMBtu

Table with 17 columns (months May-06 to Sep-07) and 5 rows of annual coal burn data at 100% capacity factor from May-06 to Sep-06.

Maximum 12 month ave based on 24-month period 4,635,894

Table DJ - 14
Dave Johnston Projected Actual PM Emissions

Plant Name	Maximum Hourly Heat Input MMBtu/hour	Maximum Annual Unit Operating Time Hours/Year	Predicted PM Emission Rate lb/MMBtu^a (U1/2-Max PM from Testing) (U3/4-Predicted PM)	Predicted PM tons/year (Using Max PM for U1/2)
Dave Johnston 1	1,300	8,760	0.136	774.3
Dave Johnston 2	1,345	8,760	0.050	294.6
Dave Johnston 3	2,800	8,760	0.015	184.0
Dave Johnston 4	4,700	8,760	0.015	308.8
Stack Totals				1,562

**Table DJ - 15
Potential to Emit Fluoride Emissions**

$$M_{HF} = F_{comb} \times 2000 \text{ lb/ton} \times C_{HF} \times 1/10^6 \times F_{acid}$$

Where:

M_{HF} =	Manufacture of Hydrogen Fluoride, lb/year	
F_{comb} =	Coal combustion, tons/year	
F_{comb} =	629,819 tons/year (Unit 1)	Note: Maximum annual coal burn rates Table DJ-7
F_{comb} =	637,664 tons/year (Unit 2)	
F_{comb} =	1,370,479 tons/year (Unit 3)	
F_{comb} =	1,997,932 tons/year (Unit 4)	
C_{HF} =	60.33	Fluoride concentration in coal, ppm (concentration occurring during maximum coal consumption period)
F_{acid} =	M_{HF}/M_F	Acid conversion factor: ratio of molecular weights, compound/parent chemical
M_F =	18.9984	Molecular weight of fluorine
M_{HF} =	20.0063	Molecular weight of hydrogen fluoride
F_{acid} =	1.053053932	
AR =	Annual release of hydrogen fluoride, lb/year	
E_{HF} =	90%	HF emission factor for bituminous coal
E_{FGD} =	6%	HF emission factor for FGD systems
$E_{No FGD}$ =	50%	HF emission factor without FGD, sub bituminous
$AR_{FGD \text{ Removal}}$ =	$(1.0 - F_{Bypass}) \times E_{FGD} \times M_{HF}$	
AR_{Bypass} =	$F_{Bypass} \times E_{No FGD} \times M_{HF}$	
AR_{Total} =	$AR_{FGD \text{ Removal}} + AR_{Bypass}$	

Historical Coal Fluoride Concentrations (Parts Per Million)
(From Emission Tables)

	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	Highest 1996-2006 Fluoride Concentration (ppm)
DJ-1				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-2				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-3				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-4				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33

Calculation Method:

EPRI LARK-TRIPP *Calculation and Methods for Threshold Determination and Release Estimates*
 HF Emission Factor with FGD System: 6%
 Bituminous Coal Emission Factor: 90%
 (Table 5-1 Emission Factors for HCL and HF)

Maximum Annual Coal Burn Rate

	Annual Coal Burn Rate
DJ-1	595,481
DJ-2	556,917
DJ-3	1,280,319
DJ-4	1,734,370

Note: Maximum annual coal burn rates
Table DJ-7

U1: F_{Bypass} =	0.00	(0% Scrubber Bypass)
U2: F_{Bypass} =	0.00	(0% Scrubber Bypass)
U3: F_{Bypass} =	0.00	(0% Scrubber Bypass)
U4: F_{Bypass} =	0.00	(0% Scrubber Bypass)

M_{HF} =	37.8	tons/year (Unit 1 HF manufacture)
M_{HF} =	35.4	tons/year (Unit 2 HF manufacture)
M_{HF} =	81.3	tons/year (Unit 3 HF manufacture)
M_{HF} =	110.2	tons/year (Unit 3 HF manufacture)

$$AR_{No FGD \text{ Removal}} = (1.0 - F_{Bypass}) \times E_{No FGD} \times M_{HF}$$

$$AR_{FGD \text{ Removal}} = (1.0 - F_{Bypass}) \times E_{FGD} \times M_{HF}$$

$AR_{No FGD \text{ Removal}}$ =	18.9	tons/year Unit 1 stack air release
$AR_{No FGD \text{ Removal}}$ =	17.7	tons/year Unit 2 stack air release
$AR_{No FGD \text{ Removal}}$ =	40.7	tons/year Unit 3 stack air release
$AR_{FGD \text{ Removal}}$ =	6.6	tons/year Unit 4 stack air release

AR_{Total} = 83.9 tons/year (Potential to Emit Hydrogen Fluoride Emissions)

Table DJ - 16
Projected Actual Fluoride Emissions

$$M_{HF} = F_{comb} \times 2000 \text{ lb/ton} \times C_{HF} \times 1/10^6 \times F_{acid}$$

Where:

M_{HF} =	Manufacture of Hydrogen Fluoride, lb/year
F_{comb} =	Coal combustion, tons/year
F_{comb} =	629,819 tons/year (Unit 1)
F_{comb} =	637,664 tons/year (Unit 2)
F_{comb} =	1,370,479 tons/year (Unit 3)
F_{comb} =	1,997,932 tons/year (Unit 4)
C_{HF} =	60.33 Fluoride concentration in coal, ppm (concentration occurring during maximum coal consumption period)
F_{acid} =	M_{HF}/M_F Acid conversion factor: ratio of molecular weights, compound/parent chemical
M_F =	18.9984 Molecular weight of fluorine
M_{HF} =	20.0063 Molecular weight of hydrogen fluoride
F_{acid} =	1.053053932
AR =	Annual release of hydrogen fluoride, lb/year
E_{HF} =	90% HF emission factor for bituminous coal
EF_{FGD} =	6% HF emission factor for FGD systems
$EF_{No FGD}$ =	50% HF emission factor without FGD, sub bituminous
$AR_{FGD \text{ Removal}}$ =	$(1.0 - F_{Bypass}) \times E_{FGD} \times M_{HF}$
AR_{Bypass} =	$F_{Bypass} \times EF_{No FGD} \times M_{HF}$
AR_{Total} =	$AR_{FGD \text{ Removal}} + AR_{Bypass}$

Note: Maximum annual coal burn rates
Table DJ-7

Historical Coal Fluoride Concentrations (Parts Per Million)
 (From Emission Tables)

	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	Highest 1996-2006 Fluoride Concentration (ppm)
DJ-1				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-2				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-3				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33
DJ-4				18.85	18.85	18.85	18.85	18.85	60.33	60.33	60.33	60.33

Calculation Method:
 EPRI LARK-TRIPP *Calculation and Methods for Threshold Determination and Release Estimates*
 HF Emission Factor with FGD System: 6%
 Bituminous Coal Emission Factor: 90%
 (Table 5-1 Emission Factors for HCL and HF)

Maximum Annual Coal Burn Rate

	Annual Coal Burn Rate
DJ-1	629,819
DJ-2	637,664
DJ-3	1,370,479
DJ-4	1,997,932

Note: Maximum annual coal burn rates
Table DJ-7

U1: F_{Bypass} = 0.00 (0% Scrubber Bypass)
 U2: F_{Bypass} = 0.00 (0% Scrubber Bypass)
 U3: F_{Bypass} = 0.00 (0% Scrubber Bypass)
 U4: F_{Bypass} = 0.00 (0% Scrubber Bypass)

M_{HF} = 40.0 tons/year (Unit 1 HF manufacture)
 M_{HF} = 40.5 tons/year (Unit 2 HF manufacture)
 M_{HF} = 87.1 tons/year (Unit 3 HF manufacture)
 M_{HF} = 126.9 tons/year (Unit 3 HF manufacture)

$$AR_{No FGD \text{ Removal}} = (1.0 - F_{Bypass}) \times EF_{No FGD} \times M_{HF}$$

$$AR_{FGD \text{ Removal}} = (1.0 - F_{Bypass}) \times EF_{FGD} \times M_{HF}$$

$AR_{No FGD \text{ Remov}}$ = 20.0 tons/year Unit 1 stack air release
 $AR_{No FGD \text{ Remov}}$ = 20.3 tons/year Unit 2 stack air release
 $AR_{FGD \text{ Removal}}$ = 5.2 tons/year Unit 3 stack air release
 $AR_{FGD \text{ Removal}}$ = 7.6 tons/year Unit 4 stack air release

AR_{Total} = 53.1 tons/year (Projected Actual Hydrogen Fluoride Emissions)

Table DJ - 17

Dave Johnston Projected Actual SO₂ Emissions Evaluation

Baseline Actual Monthly SO₂ Emissions from CEMs - Tons/Month

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04
Dave Johnston 1	377	376	373	355	340	369	332	339	327	281	296	215	16	277	270	289	308	323	255	263	158
Dave Johnston 2	362	414	421	427	376	391	356	372	365	354	298	283	232	248	224	278	291	304	164	276	257

Capacity Factor % (represent's unit's output as a percentage of what its output would have been if the unit had operated at 100% of its capacity over the time period being evaluated)

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04
Dave Johnston 1	91.60	93.95	92.29	84.38	91.11	89.77	89.23	84.36	85.65	76.40	87.32	78.84	5.83	99.99	99.41	92.62	97.68	97.80	86.75	92.41	60.20
Dave Johnston 2	94.78	94.78	94.14	93.07	94.59	91.36	92.33	87.90	91.23	89.38	84.09	92.28	79.72	94.76	94.05	92.38	90.96	93.03	55.12	96.31	94.01

Monthly SO₂ Emissions (Adjusted to 100% Capacity Factor) Tons/Month

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04
Dave Johnston 1	412.0	400.1	404.6	420.6	373.0	410.9	371.7	402.2	382.3	368.3	338.7	272.6	268.1	276.6	271.3	311.5	315.1	330.1	294.2	285.1	262.1
Dave Johnston 2	382.0	436.9	447.5	458.4	397.4	428.2	385.7	423.2	399.5	396.3	353.9	306.5	290.9	261.6	237.7	300.6	319.6	327.3	296.8	286.2	273.4

Annual SO₂ Emissions (Adjusted to 100% Capacity Factor) Based on a rolling 24-month period) Tons/Year

UNIT NAME	Oct-02	Nov-02	Dec-02	Jan-03	Feb-03	Mar-03	Apr-03	May-03	Jun-03	Jul-03	Aug-03	Sep-03	Oct-03	Nov-03	Dec-03	Jan-04	Feb-04	Mar-04	Apr-04	May-04	Jun-04
Dave Johnston 1	This is based on a 24-month rolling average so there are no valid averages until September 2004																				
Dave Johnston 2	This is based on a 24-month rolling average so there are no valid averages until September 2004																				

Table DJ - 17

Dave Johnston Projected Actual SO₂ Emissions Evaluation

Past Actual Monthly SO₂ Emissions from CEMs - Tons/Month

Jul-04	Aug-04	Sep-04	Oct-04	Nov-04	Dec-04	Jan-05	Feb-05	Mar-05	Apr-05	May-05	Jun-05	Jul-05	Aug-05	Sep-05	Oct-05	Nov-05	Dec-05	Jan-06	Feb-06
233	238	238	218	257	290	262	242	293	230	285	194	341	280	256	281	308	318	326	333
245	247	235	202	250	252	258	231	270	245	308	294	334	312	285	267	293	299	335	314

Capacity Factor % (represent's unit's output as a percentage of what its output would have been if the unit had operated at 100% of its capacity over the time period being evaluated)

Jul-04	Aug-04	Sep-04	Oct-04	Nov-04	Dec-04	Jan-05	Feb-05	Mar-05	Apr-05	May-05	Jun-05	Jul-05	Aug-05	Sep-05	Oct-05	Nov-05	Dec-05	Jan-06	Feb-06
88.96	89.20	86.43	83.38	98.96	98.26	95.82	96.45	94.67	94.53	91.38	58.71	95.80	95.64	88.31	98.91	99.72	98.78	91.25	97.21
88.75	90.58	90.26	86.60	96.76	84.32	93.83	95.93	83.34	95.99	94.47	91.43	88.77	88.81	88.25	90.58	92.04	91.84	90.89	94.65

Monthly SO₂ Emissions (Adjusted to 100% Capacity Factor) Tons/Month

Jul-04	Aug-04	Sep-04	Oct-04	Nov-04	Dec-04	Jan-05	Feb-05	Mar-05	Apr-05	May-05	Jun-05	Jul-05	Aug-05	Sep-05	Oct-05	Nov-05	Dec-05	Jan-06	Feb-06
262.1	267.0	275.7	261.9	260.0	295.1	272.9	250.6	309.4	243.5	311.4	329.8	356.2	293.0	289.5	283.6	308.6	321.7	356.8	342.9
276.4	272.5	260.8	233.7	258.7	299.1	274.7	241.0	323.5	255.1	325.9	322.1	376.6	350.9	322.5	295.1	318.2	325.4	368.5	332.0

Annual SO₂ Emissions (Adjusted to 100% Capacity Factor) Based on a rolling 24-month period) Tons/Year

Jul-04	Aug-04	Sep-04	Oct-04	Nov-04	Dec-04	Jan-05	Feb-05	Mar-05	Apr-05	May-05	Jun-05	Jul-05	Aug-05	Sep-05	Oct-05	Nov-05	Dec-05	Jan-06	Feb-06
		3,988	3,913	3,843	3,788	3,714	3,653	3,602	3,538	3,493	3,467	3,461	3,438	3,446	3,454	3,470	3,495	3,518	3,532
		4,110	4,036	3,946	3,872	3,780	3,702	3,650	3,585	3,536	3,497	3,487	3,486	3,494	3,496	3,524	3,568	3,602	3,608

Table DJ - 17

Dave Johnston Projected Actual SO₂ Emissions Evaluation

Past Actual Monthly SO₂ Emissions from CEMs - Tons/Month

Mar-06	Apr-06	May-06	Jun-06	Jul-06	Aug-06	Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
323	326	345	326	322	332	313	318	311	321	330	279	317	327	256	336	356	341	339
352	316	339	322	323	348	313	336	330	310	317	265	19	141	335	368	376	396	395

Capacity Factor % (represent's unit's output as a percentage of what its output would have been if the unit had operated at 100% of its capacity over the time period being evaluated)

Mar-06	Apr-06	May-06	Jun-06	Jul-06	Aug-06	Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
87.67	93.94	91.70	91.89	87.78	86.59	91.22	86.57	87.59	94.23	96.10	92.71	93.71	93.96	65.11	88.87	88.25	88.84	90.02
91.33	89.58	88.84	85.43	83.68	86.10	89.11	89.58	89.29	88.25	87.60	83.49	4.84	37.02	84.59	94.50	94.61	94.61	96.30

Monthly SO₂ Emissions (Adjusted to 100% Capacity Factor) Tons/Month

Mar-06	Apr-06	May-06	Jun-06	Jul-06	Aug-06	Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
368.6	346.9	375.7	354.5	366.7	383.8	343.3	367.0	354.9	340.6	343.7	300.7	338.5	348.1	393.8	378.4	403.5	384.2	376.6
385.0	352.8	381.4	376.9	385.8	404.0	351.4	375.0	369.7	351.6	361.7	317.4	388.7	381.3	396.4	389.4	397.7	418.5	409.8

Annual SO₂ Emissions (Adjusted to 100% Capacity Factor) Based on a rolling 24-month period) Tons/Year

Mar-06	Apr-06	May-06	Jun-06	Jul-06	Aug-06	Sep-06	Oct-06	Nov-06	Dec-06	Jan-07	Feb-07	Mar-07	Apr-07	May-07	Jun-07	Jul-07	Aug-07	Sep-07
3,551	3,577	3,623	3,669	3,721	3,779	3,813	3,866	3,913	3,936	3,971	3,996	4,011	4,063	4,104	4,129	4,152	4,198	4,242
3,637	3,665	3,713	3,765	3,819	3,885	3,930	4,001	4,056	4,083	4,126	4,164	4,197	4,260	4,295	4,329	4,339	4,373	4,417

13.0 Appendix F

Best Available Control Technology/LAER Clearinghouse

TABLE F-1: Best Available Control Technology/LAER Clearinghouse

New Source Review RACT/Best Available Control Technology/LAER Clearinghouse Database
 Best Available Control Technology-Prevention of Significant Deterioration Sources for carbon monoxide
Coal Fueled Boilers

RBLC ID	Company Name and Location	Unit	Size and Configuration	Control Technology	Control Efficiency	Emission Limit			Permit and Permit No.	Date
						Standardized	Limit 1	Limit 2		
MI-0379	Detroit Edison Company Monroe Power Plant	1	Pulverized coal, 7624 mmbtu/h cell burner boiler	Good Combustion Practices	not given	not given	not given	not given	11/15/05 222-05	
MI-0380	Detroit Edison Company St. Clair Power Plant	1	Pulverized coal, 1900 mmbtu/h cell burner boiler	Good Combustion Practices	not given	not given	not given	not given	01/04/06 288-05	
		2	Pulverized coal, 1900 mmbtu/h cell burner boiler	Good Combustion Practices	not given	not given	not given	not given		
MI-0381	Detroit Edison Company Monroe Power Plant	4	Pulverized coal, 7624 mmbtu/h cell burner boiler	Good Combustion Practices	not given	not given	not given	not given	03/03/06 330-05	
TX-298	Reliant Energy Inc. WA Parish	7	Coal, 6700 mmbtu/hr Tangentially fired	Good Combustion Practices	not given	0.28 lb/mmbtu	1891 lb/hr	8281 t/yr	10/15/2003 PSD-TX-901, PSD-TX-902 & -33M1	
		6	Coal, 7400 mmbtu/hr Tangentially fired	Good Combustion Practices	not given	0.29 lb/mmbtu	2168 lb/hr	9496 t/yr		
		5	Coal, 7400 mmbtu/hr Tangentially fired	Good Combustion Practices	not given	0.29 lb/mmbtu	2168 lb/hr	9496 t/yr		
TX-0342	Reliant Energy Inc. Limestone Electric Generating Station	1	Coal, 7863 mmbtu/hr Tangentially fired	Good Combustion Practices	not given	0.28 lb/mmbtu	873 lb/hr	2202 lb/hr	05/23/01 PSD-TX-371 (M3)	
		2	Coal, 7863 mmbtu/hr Tangentially fired	Good Combustion Practices	not given	0.28 lb/mmbtu	873 lb/hr	2202 lb/hr		

14.0 Appendix G

Forms



DEPARTMENT OF ENVIRONMENTAL
QUALITY
AIR QUALITY DIVISION

PERMIT APPLICATION FORM

Date of Application: October 15, 2007

1. Name of Firm or Institution: PacifiCorp - Dave Johnston Plant

2. Mailing Address

1591	Tank Farm Road	Glenrock	Wyoming
Number	Street	City	State
Converse	82637	(307) 436-2712	
County	Zip	Telephone	

3. Plant Location

1591	Tank Farm Road	Glenrock	Wyoming
Number	Street	City	State
Converse	82637	(307) 436-2712	
County	Zip	Telephone	

4. Name of owner or company official to contact regarding air pollution matters

Gregory Hager	Managing Director	(307) 436-2001
Name	Title	Telephone

1591	Tank Farm Road	Glenrock	Wyoming	82637
Number	Street	City	State	Zip

5. General nature of business

Coal-fueled steam-electric generating plant

6. Permit application is made for: New Construction Modification
 Relocation Operation
7. Type of equipment to be constructed, modified, or relocated. (List each major piece of equipment separately.)

Dave Johnston 1

- Plant projects listed in Appendix A

Dave Johnston 2

- Plant projects listed in Appendix B

Dave Johnston 3

- Replacement of the existing cell burner configuration with low-NO_x burners
- Installation of a flue gas desulfurization system with a fabric filter baghouse to achieve an 80 percent removal rate of sulfur dioxide
- Plant projects listed in Appendix C

Dave Johnston 4

- The replacement of the existing coal burners on unit 4 with a new Alstom TFS 2000™ low-NO_x firing system and the installation of one elevation of separated overfire air.
- Installation of a flue gas desulfurization system with a fabric filter baghouse to achieve an 80 percent removal rate of sulfur dioxide
- Plant projects listed in Appendix D

8. If application is being made for operation of an existing source in a new location, list previous location and new location:

Previous Location: Not Applicable

New Location: _____

9. If application is being made for a crushing unit, is there: (mark all appropriate boxes)
Not Applicable – The permitted projects are for the installation of pollution control equipment used to reduce SO₂ and NO_x emissions from unit 3 and unit 4. No crushing equipment is involved with the identified plant projects.

10. Materials used in unit or process (include solid fuels):

Not Applicable – The permitted projects are for the installation of pollution control equipment used to reduce SO₂ and NO_x emissions from unit 3 and unit 4. No crushing equipment is involved with the identified plant projects.

Type of Material	Process Weight Average (lb/hr)	Process Weight Maximum (lb/hr)	Quantity/Year

11. Air contaminants emitted:

The identified projects have the potential to change the characteristics of the air pollutants emitted from the Dave Johnston units 3 and 4 exhaust stacks. NO_x emissions will be reduced by approximately 40 percent from current levels. There will be a reduction in sulfur dioxide emissions associated with the installation of a flue gas desulfurization system. There will be a potential net annual increase in carbon monoxide (CO) emissions associated with the installation of the low NO_x burners on units 3 and 4 of approximately 147 tons per year.

Calculations of the Emission Estimates

Summary of Baseline Actual Emissions

Dave Johnston	SO ₂ tons/yr	NO _x tons/yr	PM tons/yr	VOC tons/yr	CO tons/yr	H ₂ SO ₄ tons/yr	Lead tons/yr	Fluorides tons/yr
Stack Emissions	21,956	15,838	2,049	121	1,008	21.8	0.32	81.0
Non-stack Emissions ¹	-	-	310	-	-	-	-	-
Total Past Emissions	21,969	15,838	2,359	121	1,008	21.8	0.32	81

¹Maximum past non-stack PM emissions from 2002-2006 emissions inventories

Summary of Projected Actual Emissions

	SO ₂ tons/yr ²	NO _x tons/yr ²	PM tons/yr	VOC tons/yr	CO tons/yr	H ₂ SO ₄ tons/yr	Lead tons/yr	Fluorides tons/yr
Past Actual Annual Baseline Emissions (Not Including Non-Stack Sources)	21,953	15,553	2,049	121	1,008	21.8	0.32	81.0
Potential Past Annual (Not Including Non-Stack Sources)	22,724	16,385	2,105	125	1,042	22.6	0.33	83.9
Potential Annual Emissions (Not Including Non-Stack Sources)	-	-	1,562	139	7,500	10	0.21	53.1
Capable of Accommodating Adjustment (Potential Past – Past Actual)	-	-	56	4	34	0.8	0.01	2.9
Potential Annual Emissions minus “what the unit was capable of accommodating”	-	-	1,506	135	7,466	9.2	0.2	50.2

Evaluation of significance levels by pollutant

To determine if a Prevention of Significant Deterioration significance level has been reached the baseline actual annual emissions are subtracted from the projected actual emissions.

Permitted Projects: Unit 3 and 4 Low NO _x burners and flue gas desulfurization systems	Baseline Actual tons/year	Projected Actual emissions tons/year	Projected Actual minus Baseline Actual	PSD Review Significance Level - tons/year	Emission Increase Greater than significance level
SO ₂	21,953	-	-	40	NO
NO _x	15,553	-	-	40	NO
PM	2,049	1,562	-487	25	NO
CO	1,008	7,500	6,492	100	YES
Ozone (as VOC)	121	139	18	40	NO
Fluoride (as HF)	81.0	53.1	-27.9	3	NO
Lead	0.32	0.21	-0.11	0.6	NO
Sulfuric acid mist	21.8	10.0	-11.8	7	NO

12. Air contaminant control equipment:

Emission Point	Type	Pollutant Removed	Efficiency
Unit 3 stack	Advanced Low NO _x burners with over-fire air	NO _x	This equipment is expected to reduce annual NO _x emissions by 30-40 percent when compared to pre-project emissions
Unit 3 stack	Spray dryer flue gas desulfurization	SO ₂	This equipment is expected to reduce annual SO ₂ emissions by 80 percent when compared to pre-project emissions
Unit 4 stack	Advanced Low NO _x burners with one level of separated over-fire air	NO _x	This equipment is expected to reduce annual NO _x emissions by 30-40 percent when compared to pre-project emissions
Unit 4 stack	Spray dryer flue gas desulfurization	SO ₂	This equipment is expected to reduce annual SO ₂ emissions by 80 percent when compared to pre-project emissions

13. Type of combustion unit: (check if applicable):

A. Coal

1. *Pulverized* X:

General ___; Dry Bottom X; Wet Bottom ___; With Flyash Reinjection ___; Without Flyash Reinjection ___; Other

2. *Spreader Stoker* ___:

With Flyash Reinjection ___; Without Flyash Reinjection ___; Cyclone ___; Hand-Fired ___; Other

B. Fuel Oil

Horizontally Fired ___

Tangentially Fired

Type of combustion unit: (check if applicable):

C. Natural Gas

D. If other, please specify

The maximum unit 3 hourly heat input value will increase to 2,800 MMBtu/hour following installation of the spray dryer absorber flue gas desulfurization system.

14. Operating Schedule: 24 hours/day; 7 days/week; 52 weeks/year.

Peak production season (if any):

15. Fuel analysis: Not Applicable – The planned Dave Johnston plant projects will not change the amount or quality of fuel burned or the capacity of the generating units.

	COAL	FUEL OIL	NATURAL GAS
% Sulfur			
% Ash			
BTU Value			

16. Products of process or unit: Not Applicable – The planned Dave Johnston plant projects will not change the amount or quality of fuel burned or the capacity of the generating units.

Products	Quantity/Year

17. Emissions to the atmosphere (each point of emission should be listed separately and numbered so that it can be located on the flow sheet):

Emission Point	Stack Height (ft)	Stack Diameter (ft)	Gas Discharge SCFM	Exit Temp (°F)	Gas Velocity (ft/s)
Unit 1 stack	500	11 (exit I.D.)	538,000	300	94
Unit 2 stack	500	11 (exit I.D.)	538,000	300	94
Unit 3 stack*	500	18 (exit I.D.)	1,314,000	190	73
Unit 4 stack*	500	18 (exit I.D.)	1,352,000	190	89

* proposed new stack installation for Unit 3 and Unit 4

18. Does the input material or product from this process or unit contain finely divided materials which could become airborne?

Yes No

Is this material stored in piles or in some other way as to make possible the creation of dust problems?

Yes No

18. Continued:
List storage pile (if any):

Type of Material	Particle Size (Diameter or Screen Size)	Pile Size (Average Tons on Pile)	Pile Wetted (Yes or No)	Pile Covered (Yes or No)
Coal	1 inch minus	273,000	No	No

19. Using a flow diagram:

- (1) Illustrate input of raw materials.
- (2) Label production processes, process fuel combustion, process equipment, and air pollution control equipment.
- (3) Illustrate locations of air contaminant release so that emission points under items 11, 12 and 17 can be identified. For refineries show normal pressure relief and venting systems. Attach extra pages as needed.

20. A site map should be included indicating the layout of facility at the site. All buildings, pieces of equipment, roads, pits, rivers and other such items should be shown on the layout.
21. A location drawing should be included indicating location of the facility with respect to prominent highways, cities, towns, or other facilities (include UTM coordinates).

"I certify to the accuracy of the plans, specifications, and supplementary data submitted with this application. It is my Opinion that any new equipment installed in accordance with these submitted plans and operated in accordance with the manufacturer's recommendations will meet emission limitations specified in the Wyoming Air Quality Standards and Regulations."

Signature		Typed Name	Gregory L. Hager		
Title	Managing Director	Company	PacifiCorp		
Mailing Address	1591 Tank Farm Road	Telephone No.	(307) 436-2001		
City	Glenrock	State	Wyoming	Zip	83267
P.E. Registration (if applicable)					
State where registered					

Figure 1 - Dave Johnston Site

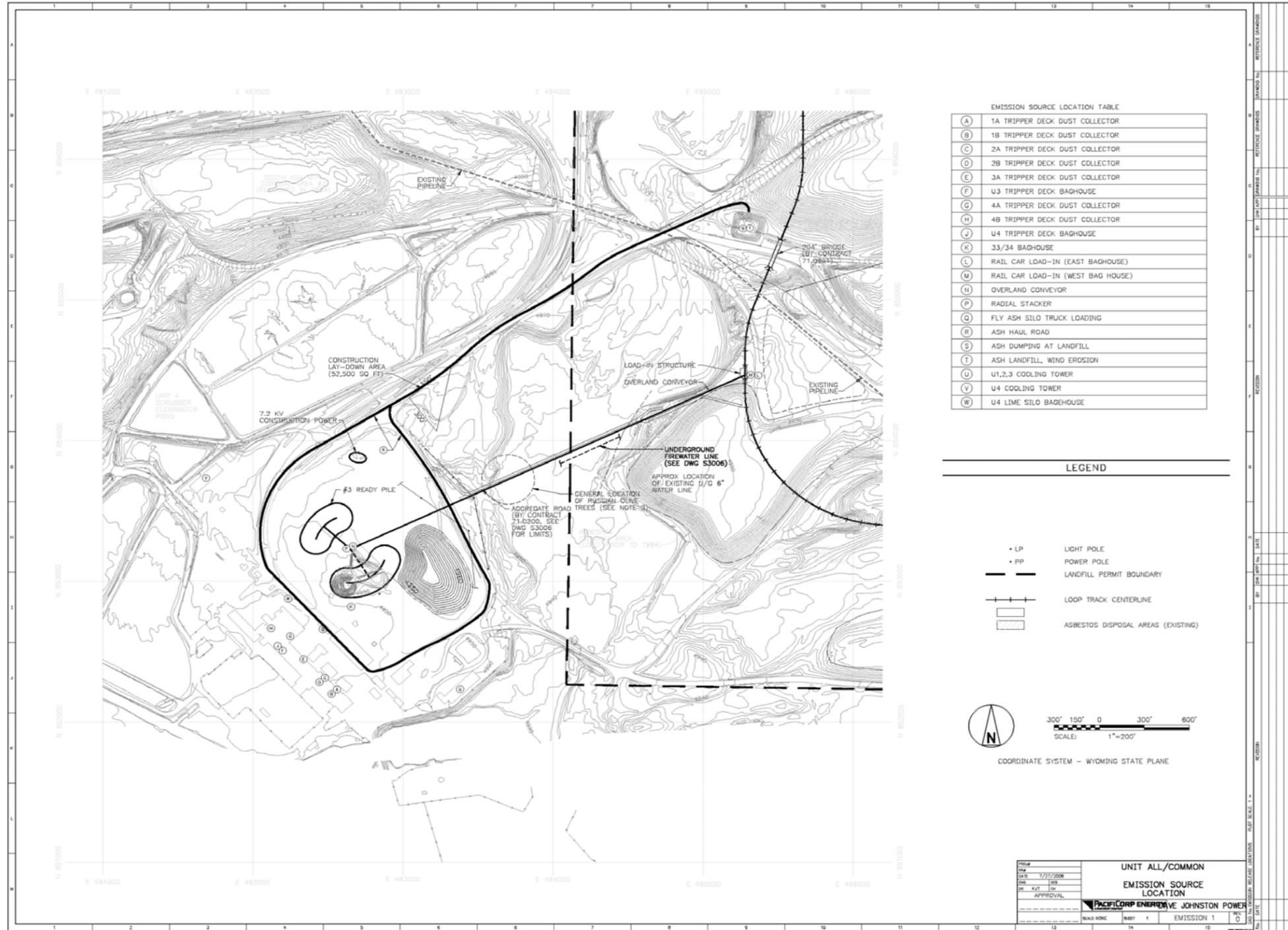


Figure 2 - Dave Johnston Aerial Site Photo



15.0 Appendix H

Modeling Protocols and Results

APPENDIX H

DISPERSION MODELING RESULTS

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1.0 INTRODUCTION AND SUMMARY

1.1 INTRODUCTION

PacifiCorp proposes several projects to modify the four existing coal-fired units at the Dave Johnston plant. As a result of the proposed modifications, only CO emissions will increase. Nitrogen oxides (NO_x), sulfur dioxide (SO₂), and particulate matter less than or equal to 10 micrometers (PM₁₀) emissions will remain the same. The increase in CO emissions will be above the Prevention of Significant Deterioration (PSD) Significant Emission Rate (SER) of 100 tons per year (tpy) for CO. Therefore, CO will be subject to PSD regulations under Wyoming Air Quality Standards and Regulations (WAQSR), Chapter 6, Section 4(b)(i)(A)(I). In addition to meeting the PSD requirements, ambient air impacts from NO_x, SO₂, PM₁₀, lead, and fluoride emissions will be compared to the Wyoming Ambient Air Quality Standards (WAAQS).

Environmental Consulting & Technology, Inc. (ECT), has been retained by PacifiCorp to perform the air quality analysis. This air quality analysis supplements the permit application for the proposed modifications. The purpose of this Appendix is to:

- Further define the modeling approach discussed in the modeling protocol.
- Identify the emissions data, meteorological data, and dispersion model used.
- Present the modeling results and discuss any potential impacts.

1.2 SUMMARY

Refined modeling, using a dense receptor grid and 4 years of onsite meteorology (1998, 2000, 2001, and 2002), was conducted to determine air quality impacts for CO, NO_x, SO₂, PM₁₀, lead, and fluoride emissions from the Dave Johnston plant. The modeling results show that the CO impacts were below the PSD significant impact levels (SIL) and NO_x, SO₂, PM₁₀, lead, and fluoride impacts were below the WAAQS. Accordingly, the proposed modifications to the Dave Johnston plant will not cause any exceedances of the WAAQS.

Section 2.0 of the report describes the applicable regulatory requirements. Section 3.0 provides a site description for the Dave Johnston facility. Section 4.0 contains the model-

ing approach and input data for modeling. Section 5.0 summarizes the results of the modeling analysis. A description of the modeling files, used to perform the modeling analysis, can be found in Attachment A. The electronic modeling files are on the enclosed CD.

This appendix is submitted to Wyoming Department of Environmental Quality (WDEQ) in fulfillment of the PSD requirements and WDEQ's request for a WAAQS analysis.

2.0 AIR QUALITY STANDARDS AND THEIR APPLICABILITY

As a result of the 1977 Clean Air Act (CAA) Amendments, the U.S. Environmental Protection Agency (EPA) has enacted primary and secondary National Ambient Air Quality Standards (NAAQS) for six air pollutants (40 Code Federal Regulations [CFR] 50). Primary NAAQS are intended to protect the public health, and secondary NAAQS are intended to protect the public welfare from any known or anticipated adverse effects associated with the presence of pollutants in the ambient air. Wyoming has adopted most of the NAAQS for the criteria pollutants, and they have produced AAQS for additional pollutants, i.e. fluorides, hydrogen sulfide, suspended sulfates, and odors. Table 2-1 presents the current WAAQS standards for NO₂, SO₂, PM₁₀, CO, ozone, lead, and fluorides.

A source impact analysis must be performed for any modification that proposes an increase in emissions above the PSD SER. EPA requires the use of atmospheric dispersion models in performing an ambient impact analysis, estimating baseline and future air quality levels, and determining compliance with WAAQS and allowable PSD increments. Designated EPA models must normally be used in performing the impact analysis. Specific applications for other than EPA-recommended models require prior approval. Guidance for the use and application of dispersion models is presented in the EPA publication, *Guideline on Air Quality Models (Revised)* (GAQM), as published in Appendix W to 40 CFR 51. Criteria pollutants may be exempt from the full source impact analysis if the net increase in impacts due to the new source or modification is below the appropriate SIL, as presented in Table 2-2. Accordingly, CO impacts are to be initially compared to the CO SIL to determine if further analysis is required.

Table 2-1. Wyoming Ambient Air Quality Standards (WAAQS)

Pollutant	Averaging Time	WAAQS ($\mu\text{g}/\text{m}^3$)	
		Primary	Secondary
PM ₁₀	Annual arithmetic mean	50	50
	24-hour maximum*	150	150
PM _{2.5}	Annual arithmetic mean	15	15
	24-hour maximum†	65	65
SO ₂	Annual arithmetic mean	60	NA
	24-hour maximum‡	260	NA
	3-hour maximum‡	NA	1,300
NO ₂	Annual arithmetic mean	100	100
CO	8-hour maximum‡	10,000	NA
	1-hour maximum‡	40,000	NA
Ozone	8-hour maximum**	157	157
Lead	Calendar quarter arithmetic mean	1.5	1.5
Fluorides	Annual arithmetic mean	NA	23,310
	30-day maximum	0.4	NA
	7-day maximum	0.5	NA
	24-hour maximum	1.8	NA
	12-hour maximum	3.0	NA

Note: NA = not applicable.

*Standard is attained when the 99th percentile 24-hour concentration is less than or equal to the standard.

†Standard is attained when the 98th percentile 24-hour concentration is less than or equal to the standard.

‡Maximum concentration not to be exceeded more than once per year.

**Standard is attained when the average of the annual 4th highest daily maximum 8-hour average concentration is less than or equal to the standard.

Sources: WAQSR, 2006.
ECT, 2006.

Table 2-2. PSD Significant Impact Levels for Criteria Pollutants

Pollutant	Averaging Period	Concentration ($\mu\text{g}/\text{m}^3$)
SO ₂	Annual	1
	24-Hour	5
	3-Hour	25
PM ₁₀	Annual	1
	24-Hour	5
NO _x	Annual	1
CO	8-Hour	500
	1-Hour	2,000
Lead	Quarterly	0.03

Sources: 40 CFR 51.165(b)(2).
 WAQSR, Section 4.
 ECT, 2006.

3.0 SITE DESCRIPTION

The Dave Johnston plant is located in Converse County, Wyoming, approximately 5 miles southeast of Glenrock and approximately 35 miles east of Casper. The project site is located along the North Platte River. The surrounding area is sparsely populated. Figures 3-1 and 3-2 show the location of the Dave Johnston Plant on a street map and a topographic map, respectively.

Major buildings and structures at the Dave Johnston Plant are shown on the site plan provided in Appendix G the permit application. The dimensions (i.e., length, width, and height) of each major facility/structure are provided in Table 3-1. All entrances to the plant site have a security gate to control site access. The site is composed of multiple sections in which each section is fenced. The fence line will be discussed in Section 4.7.

The base elevation of the site near the coal-fired units is approximately 4,950 feet above mean sea level (ft-msl). Elevations on the property vary from 4,940 to 5,040 ft-msl. The terrain immediately surrounding the site is relatively flat and varies from 4,880 to 5,250 ft-msl. Terrain to the south of the site gradually rises for approximately 8 kilometers (km) and then increases more dramatically. Elevations of approximately 6,500 ft-msl can be found at a distance of approximately 10 km from the site.

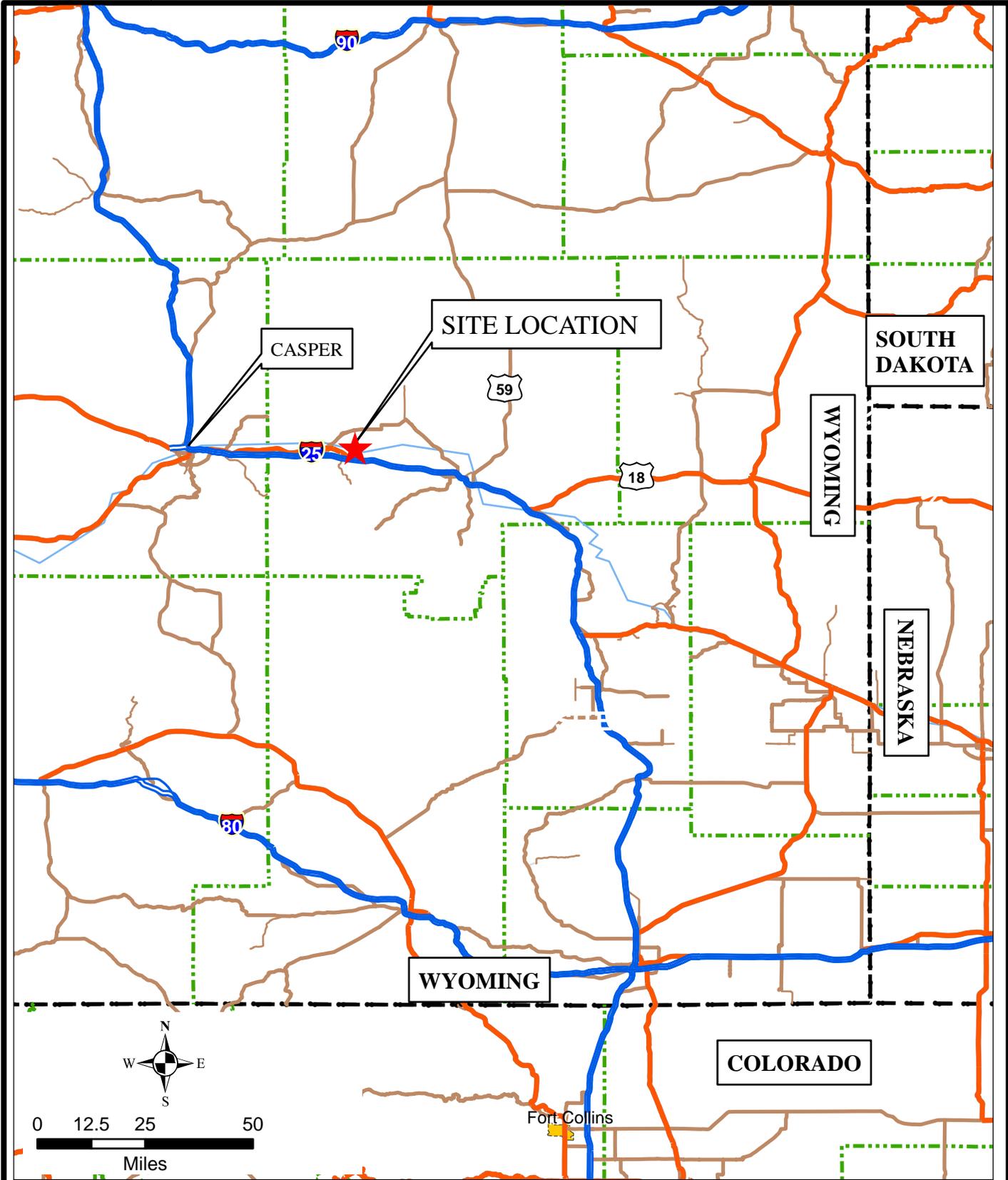


FIGURE 3-1.
SITE LOCATION
DAVE JOHNSTON PLANT
CONVERSE COUNTY, WYOMING

Sources: ESRI Street Map; ECT, 2006.

ECT
Environmental Consulting & Technology, Inc.

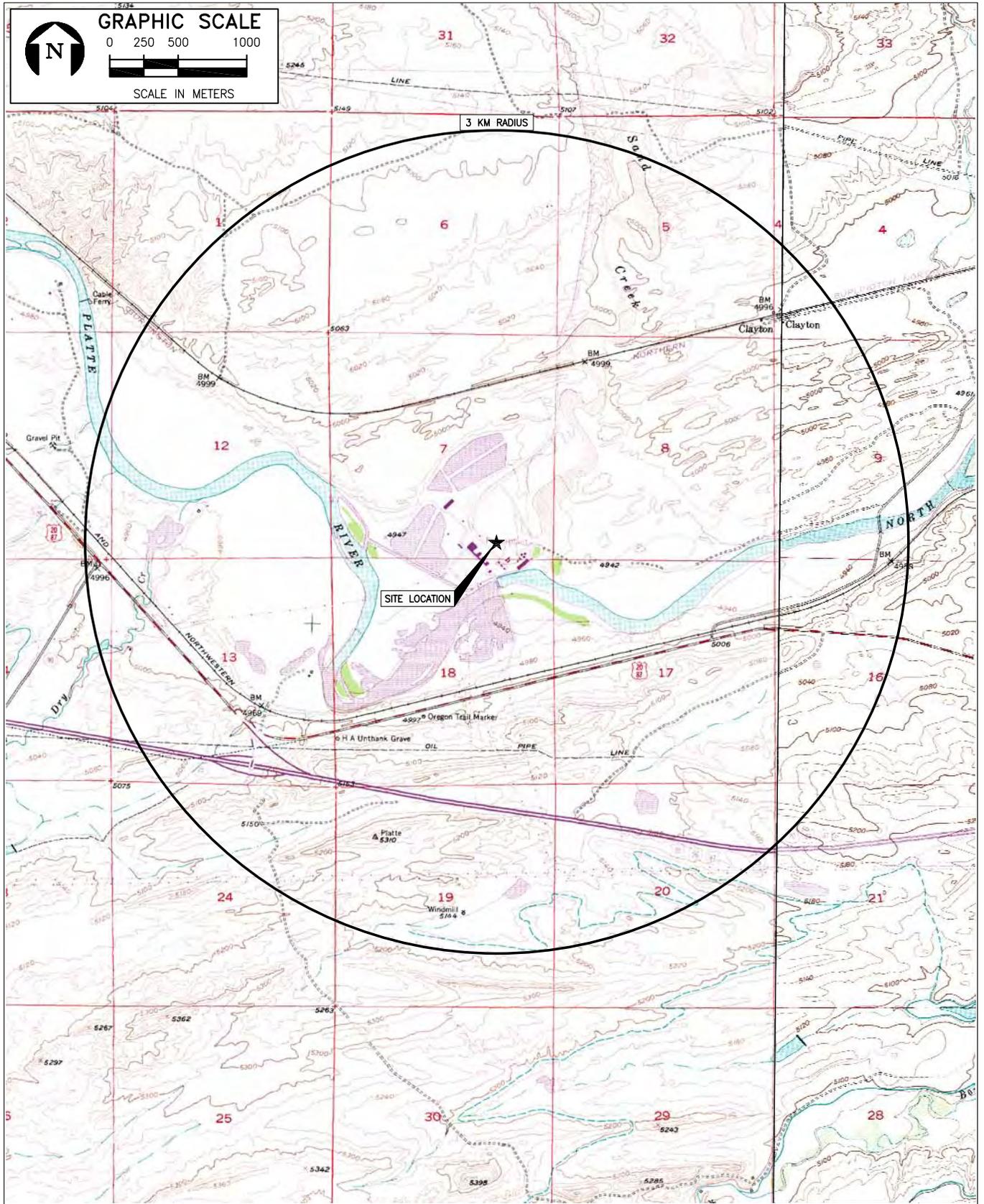


FIGURE 3-2.
LOCATION OF DAVE JOHNSTON PLANT

Sources: USGS Quad: Glenrock & Careyhurst, WY, 1974; ECT, 2006.



Table 3-1. Building/Structure Dimensions for Dave Johnston

Building/Structure	Dimensions		
	Width (meters)	Length (meters)	Height (meters)
Coal Boiler Unit 1	18.1	29.2	52.4
Coal Boiler Unit 2	19.0	29.7	52.4
New Coal Boiler Unit 3	25.5	16.8	57.8
New Coal Boiler Unit 4	20.4*		51.8
Admin. Building	20.4*		51.8
AQC Breaker Bldg.	12.4	22.9	9.1
Ash Silo-South (Tier 1)	10.0	12.6	6.1
Ash Silo-South (Tier 2)	9.8*		15.2
Ash Silo-North (Tier 1)	16.8	9.8	6.1
Ash Silo-North (Tier 2)	9.8*		15.2
South Coal Loading Hopper	15.9	6.5	24.4
North Coal Loading Hopper	6.4	11.1	24.4
Coal Yard Maintenance Bldg.	15.2	18.3	6.1
Cooling Tower for Units 1-3	79.6	21.1	18.3
Cooling Tower for Unit 4	72.6	20.5	15.2
No. 1 Crusher House	7.5	7.4	48.5
No. 2 Crusher House	8.5	9.6	48.5
No. 3 Crusher House	7.7	7.4	48.5
Floc Filter Plant	10.1	18.4	9.1
Plant Garage	51.7	24.7	15.2
Hazardous Material Storage	12.3	7.3	15.2
High Tank	9.1*		36.6
Ignition Oil Tank	7.6*		7.3
Lignasite Pump House	5.7	12.3	22.9
Lime System Building	16.5	4.6	24.4
Maintenance Shop	33.1	31.5	41.6
Maintenance Storage for Unit 4	6.9	6.9	9.1
Mill Shop	12.5	17.4	15.2
Heavy Oil Pump House	21.3	4.7	6.1
Unit 3 Old Stack	7.6*		76.4
Unit 2 Old Stack	7.6*		76.4
Unit 1 Old Stack	7.6*		76.4
Ready Pile No. 1 (Tier 1)	50.6*		4.4
Ready Pile No. 1 (Tier 2)	38*		8.8
Ready Pile No. 1 (Tier 3)	25.3*		13.3
Ready Pile No. 1 (Tier 4)	17.7*		17.7
Ready Pile No. 2 South (Tier 1)	68.6*		4.0
Ready Pile No. 2 South (Tier 2)	53.3*		7.9
Ready Pile No. 2 South (Tier 3)	38.1*		11.9
Ready Pile No. 2 South (Tier 4)	22.9*		15.9
Ready Pile No. 2B (Tier 1)	68.6*		4.0

Table 3-1. Building/Structure Dimensions for Dave Johnston (Continued, Page 2 of 2)

Building/Structure	Dimensions		
	Width (meters)	Length (meters)	Height (meters)
Ready Pile No. 2B (Tier 2)	53.3*		7.9
Ready Pile No. 2B (Tier 3)	38.1*		11.9
Ready Pile No. 2B (Tier 4)	22.9*		15.9
Ready Pile No. 3 South (Tier 1)	73.2*		4.9
Ready Pile No. 3 South (Tier 2)	54.9*		9.8
Ready Pile No. 3 South (Tier 3)	36.6*		14.6
Ready Pile No. 3 South (Tier 4)	18.3*		19.5
Ready Pile No. 3 North (Tier 1)	73.2*		4.9
Ready Pile No. 3 North (Tier 2)	54.9*		9.8
Ready Pile No. 3 North (Tier 3)	36.6*		14.6
Ready Pile No. 3 North (Tier 4)	18.3*		19.5
ESPs for Units 1 through 3	93.9	33.1	42.7
Recycle Pump House	6.0	30.3	15.2
New Unit 3 Baghouse	22.0	30.8	28.0
New Unit 4 Baghouse	22.0	30.8	28.0
New Units 3/4 Waste Ash Silo	7.9*		23.5
Coal Storage Silo for Units 1 and 2	76.4	17.0	48.8
Coal Storage Silo for Unit 3	83.8	12.4	50.3
Storage Building No. 1	33.5	15.1	30.5
Storage Building No. 2	12.8	11.4	15.2
Storage Building No. 3	12.0	4.2	9.1
Storage Building No. 4	7.7	21.7	6.1
Main Fuel Tank A	15.2*		13.4
Main Fuel Tank B	15.2*		13.4
Main Fuel Tank C	7.6*		9.1
Training Bldg	29.9	12.4	6.1
Turbine Generator Building	230.7	18.2	45.7
Unit 3 Steam Generator	23.5	10.8	38.1
Unit 4 South Silo	54.3	10.5	50.3
Unit 4 North Silos	10.1	54.2	50.3
Units 3/4 Lime Silo	9.8*		36.7
Units 3/4 Lime Prep, Ash Recycle Bldg	24.4	46.3	23.8
Units 1/2 Stack Enclosure	15.9*		152.4
Units 3/4 Stack Enclosure	14.1*		152.4
Warehouse	78.9	18.5	24.4

*Diameter.

Sources: PacifiCorp, 2007.
ECT, 2007.

4.0 MODELING APPROACH AND INPUT DATA

4.1 MODELING APPROACH

The primary objective of the air quality analysis is to compare the ambient CO impacts caused by the proposed modifications, with the PSD SIL. The remainder of the air quality analysis will include comparisons of NO_x, SO₂, PM₁₀, lead, and fluoride impacts against the WAAQS.

To achieve the primary objective, usually the CO impacts caused by the proposed modification alone are compared to the SIL. For this study, a conservative approach was taken by using the total CO emissions, including existing emissions, for the modeling analysis. If the modeled CO impacts are below the specified PSD SIL, then no further study would be required. The SIL are shown in Table 2-2. If the impacts of the proposed modifications are found to be significant, further analyses, considering all existing sources and background pollutant concentrations, are required.

To achieve the secondary objective, facility-wide emission rates were determined for NO_x, SO₂, PM₁₀, lead, and fluorides throughout the Dave Johnston plant. These emission sources were combined with significant emission sources from other facilities within 50 km of Dave Johnston. The total impact caused by the facilities was added to the respective ambient concentrations, and then compared to the WAAQS shown in Table 2-1.

The air quality modeling analysis was conducted in a manner consistent with EPA's GAQM and standard practices. This includes the use of regulatory default options, as appropriate. Specifics of the modeling approach are presented in the following paragraphs.

4.2 MODEL SELECTION AND USE

According to the modeling protocol submitted on July 24, 2006, the current version of the Industrial Source Complex-Plume Rise Model Enhancements (ISC-PRIME) model, Version 04269, was used to obtain ambient air impacts from all pollutants included in this study. Because of some unavoidable delays, submittal of this modeling analysis has been delayed, but the selection of ISC-PRIME remains valid, since an approved modeling pro-

protocol was agreed upon during the transition period of AERMOD or prior to the December 9, 2006. As stated in the GAQM, "...applications of ISC3 with approved protocols may be accepted...". For the purposes of this study ISC-PRIME is considered an acceptable *Alternative* model which has been proven previously to be reliable by EPA.

The ISC-PRIME model is a steady-state Gaussian plume model that can be used to assess potential air quality impacts from a wide variety of sources. It is capable of calculating concentrations for averaging times ranging from 1 hour to annual. Principal features of the ISC-PRIME model are summarized as follows:

- EPA has previously been approved the use of ISC-PRIME to address compliance with air quality standards in the United States.
- ISC-PRIME is capable of predicting impacts from multiple sources (including stack, area, and volume sources) that are distributed over large areas.
- Appropriate in areas of flat or elevated terrain.
- Rural or urban mode options can be selected.
- Either Cartesian or polar receptor coordinate grids can be used.
- Addresses potential for building downwash to occur.

The ISC-PRIME model calculates concentrations due to stack sources using the steady-state Gaussian plume equations for a continuous source. The plume rise equations developed for ISC-PRIME, including the momentum terms, are used to calculate plume rise. A wind profile exponent law is used to adjust the observed mean windspeed from the measurement height to the emission height, for the plume rise and concentration calculations. The Pasquill-Gifford dispersion curves are used to calculate the horizontal standard deviation (σ_y) and vertical standard deviation (σ_z) of the plume spread.

Procedures applicable to the ISC-PRIME dispersion model specified in EPA's 1999 GAQM were followed in conducting the refined dispersion modeling. In particular, the ISC-PRIME model control pathway MODELOPT keyword parameters DFAULT, CONC, and RURAL were selected. Selection of the parameter DFAULT, which specifies use of the regulatory default options, was recommended by the GAQM. The CONC and

RURAL parameters specify calculation of concentrations and use of rural dispersion, respectively.

ISC-PRIME Version 04269 was confirmed by the EPA Support Center for Regulatory Models (SCRAM) Internet site to be the latest available ISC-PRIME model code.

4.3 AREA DESCRIPTION

Area characteristics in the vicinity of proposed emission sources are important in determining model selection and use. The first consideration is whether the area is rural or urban, since dispersion rates differ between these two classifications. In general, urban areas cause greater rates of dispersion because of increased turbulent mixing and buoyancy-induced mixing. This is due to the combination of greater surface roughness caused by more buildings and structures and greater amount of heat released from concrete and similar surfaces. EPA guidance provides two procedures to determine whether the character of an area is predominantly urban or rural. One procedure is based on land use typing and the other is based on population density. The land use typing method utilizes the work of Auer (Auer, 1978) and is preferred by EPA because it is meteorologically oriented. In other words, the land use factors employed in making a rural/urban designation are also factors that have a direct effect on atmospheric dispersion. These factors include building types, extent of vegetated surface area and water surface area, types of industry and commerce, etc. Auer recommends that these land use factors be considered within 3 km of the source to be modeled to determine urban or rural classifications. The Auer land use typing method was used for the Dave Johnston air quality analysis.

The Auer technique recognizes four primary land use types: industrial (I), commercial (C), residential (R), and agricultural (A). Practically all industrial and commercial areas come under the heading of urban, while the agricultural areas are considered rural. However, those portions of generally industrial and commercial areas that are heavily vegetated can be considered rural in character. In the case of residential areas, the delineation between urban and rural is not as clear. For residential areas, Auer subdivides this land use type into four groupings based on building structures and associated vegetation. Ac-

curate classification of the residential areas into proper groupings is important to determine the most appropriate land use classification for the study area.

U.S. Geological Survey (USGS) 7.5-minute series topographic maps for the area were used to identify the land use types within a 3-km radius area of the plant site (see Figure 3-2). Based on this analysis, clearly more than 50 percent of the land use surrounding the area is rural; therefore, rural dispersion coefficients and mixing heights were used.

4.4 TERRAIN CONSIDERATION

The GAQM defines *flat terrain* as terrain equal to the elevation of the stack base, *simple terrain* as terrain lower than the height of the stack top, and *complex terrain* as terrain above the height of the plume center line (for screening modeling, *complex terrain* is terrain above the height of the stack top). Terrain above the height of the stack top but below the height of the plume center line is defined as *intermediate terrain*.

USGS quadrangle maps covering the Dave Johnston plant site and vicinity (approximately 10-km radius) were studied for terrain features. The base elevation of the site is approximately 4,950 ft-msl. The terrain immediately surrounding the facility is relatively flat. Terrain to the south of the site reaches elevations of approximately 6,500 ft-msl at a distance of approximately 10 km from the site. Units 1 through 4 have stack heights of 500 feet above ground level (ft-agl). Therefore, with respect to Units 1 through 4, terrain above 5,450 ft-msl would be considered *complex*, as defined in the GAQM describing terrain above the height of stack tops.

Terrain of 6,000 ft-msl is found at a distance of approximately 8 km to the south of the site. Due to the complex terrain found within the vicinity of the site, elevations were assigned to each receptor using elevation data obtained from USGS Digital Elevation Model (DEM) files.

4.5 METEOROLOGICAL DATA

Detailed meteorological data are needed for modeling with the ISC dispersion models. The ISC-PRIME model requires a preprocessed data file compiled from hourly surface observations and concurrent twice-daily rawinsonde soundings (i.e., mixing height data).

Four years of onsite meteorological data (1998, 2000 through 2002) collected from an onsite meteorological tower were used. Data was collected for 1999, but the data set is only 60 percent complete for wind speed. Therefore, the 1999 data could not be used for this modeling analysis. Windroses for the onsite meteorological data, representing the years 1998 through 2002, are shown in Figures 4-1 through 4-5.

The onsite surface meteorological data does not include cloud cover data. Cloud cover and ceiling height data were obtained from the Casper Natrana County International Airport (WBAN 24089), which is approximately 38 miles west-northwest of the site.

The onsite windspeed, wind direction, temperature, and relative humidity data from the Dave Johnston site is more than 97 percent complete for 1998, 2000, 2001, and 2002, with years 1998, 2001, and 2002 being more than 99.5 percent complete. Reviewing the data on a quarterly basis, the minimum quarter of completeness is 92.3 percent and occurs during the summer of 2000. Any missing meteorology data was substituted according to EPA's *objective procedure*. If two or more hours are missing, then the nearest available data was reviewed to determine an appropriate value to substitute. For example, if two hours of data are missing, then the first hour was filled with the preceding hour, and the second hour was filled by the following hour. The ceiling height data was also reviewed to obtain an appropriate value to substitute. A cloud cover code of "0" is used if the ceiling height is unlimited, and a code of "7" is used if the ceiling height is less than or equal to 7,000 ft. The method of substitution of missing meteorological data can be found in Attachment B.

The mixing height data was calculated by National Climatic Data Center (NCDC) using data from the Casper Natrana County International Airport and the Riverton Regional Airport (WBAN 24061). ECT filled in missing data using the EPA's *objective procedure*.

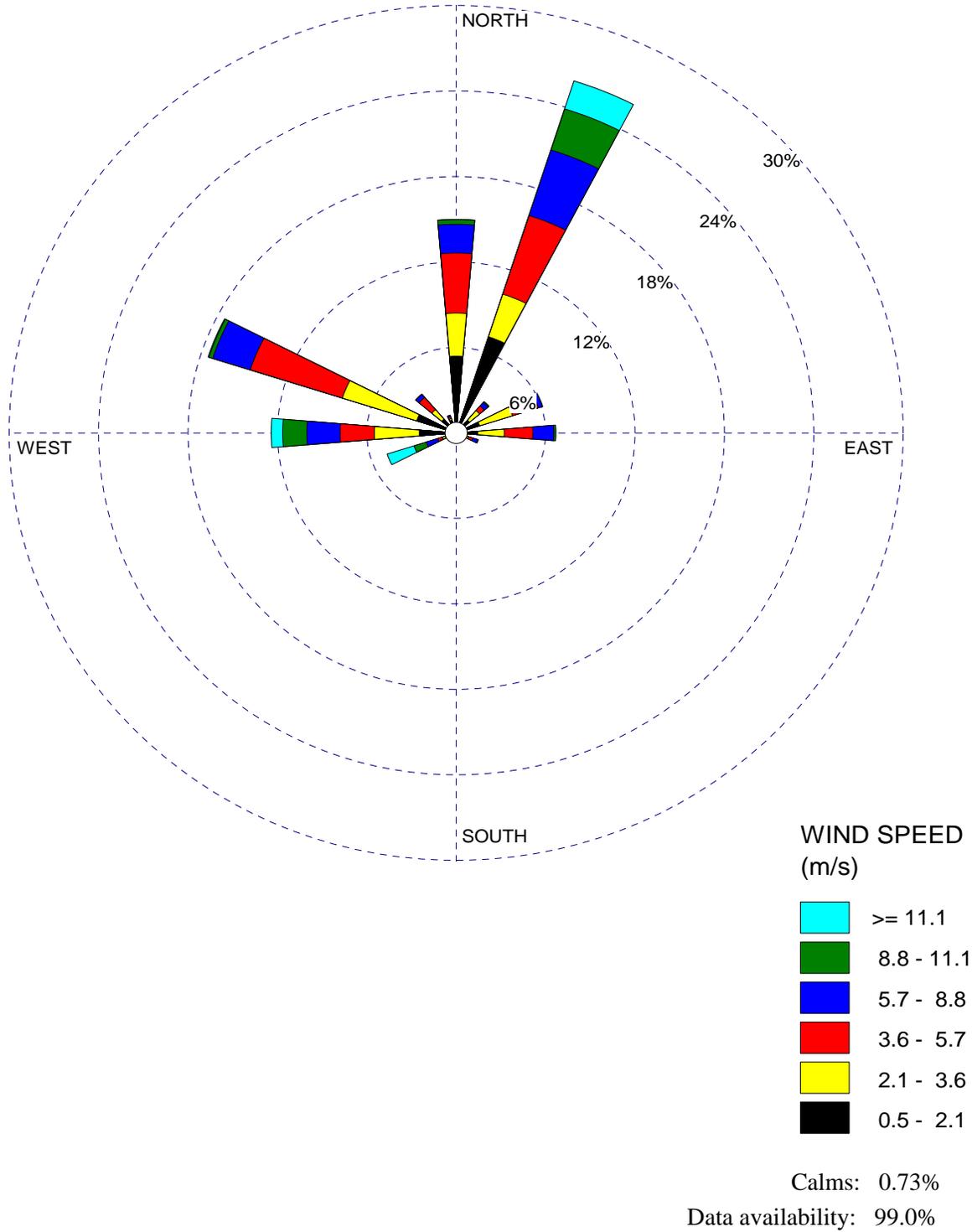


FIGURE 4-1.
ANNUAL WINDROSE FOR ONSITE MET. DATA (1998)
DAVE JOHNSON PLANT
Sources: PacifiCorp, 2006. ECT, 2006.



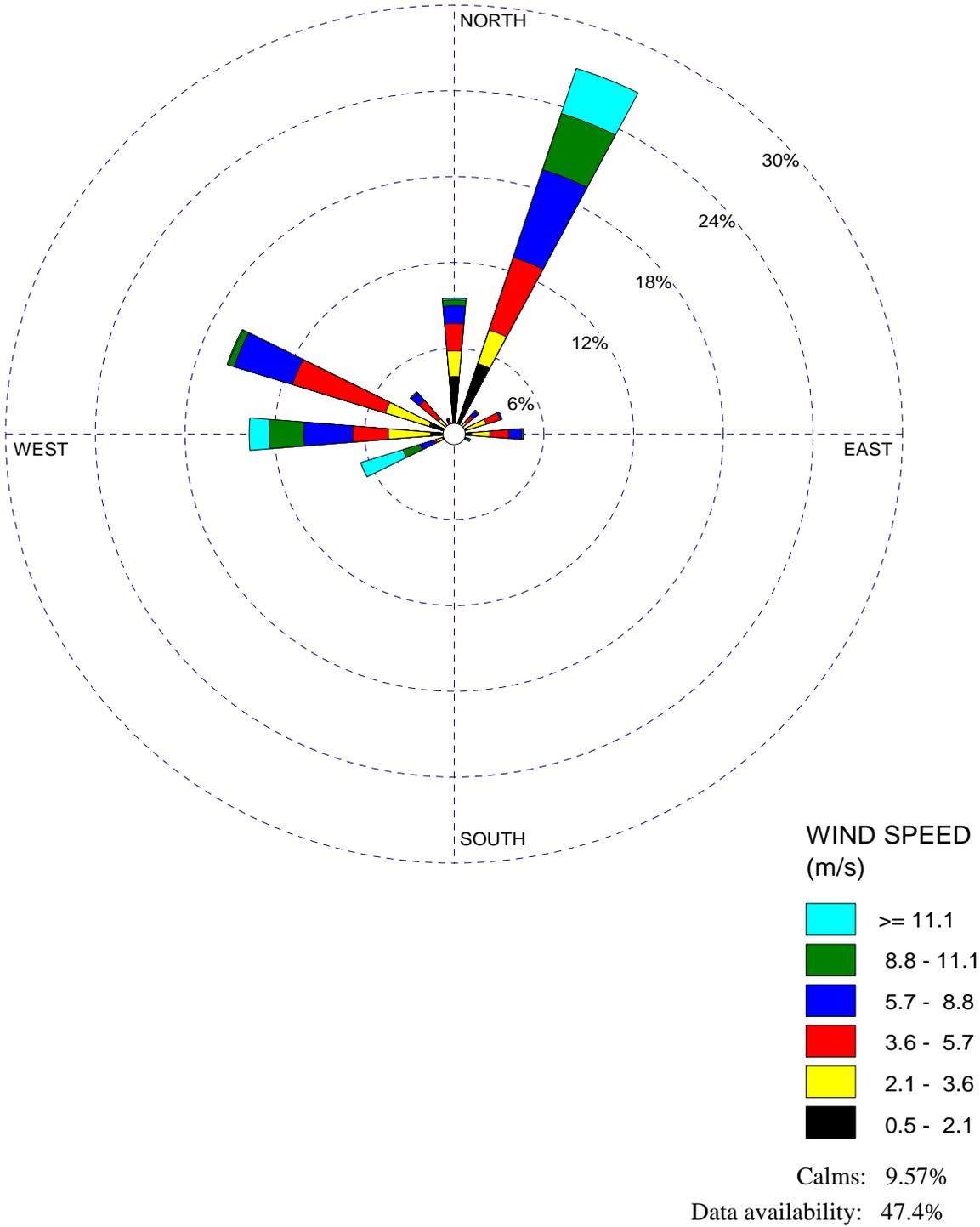


FIGURE 4-2.

ANNUAL WINDROSE FOR ONSITE MET. DATA (1999)
DAVE JOHNSON PLANT

Sources: PacifiCorp, 2006. ECT, 2006.



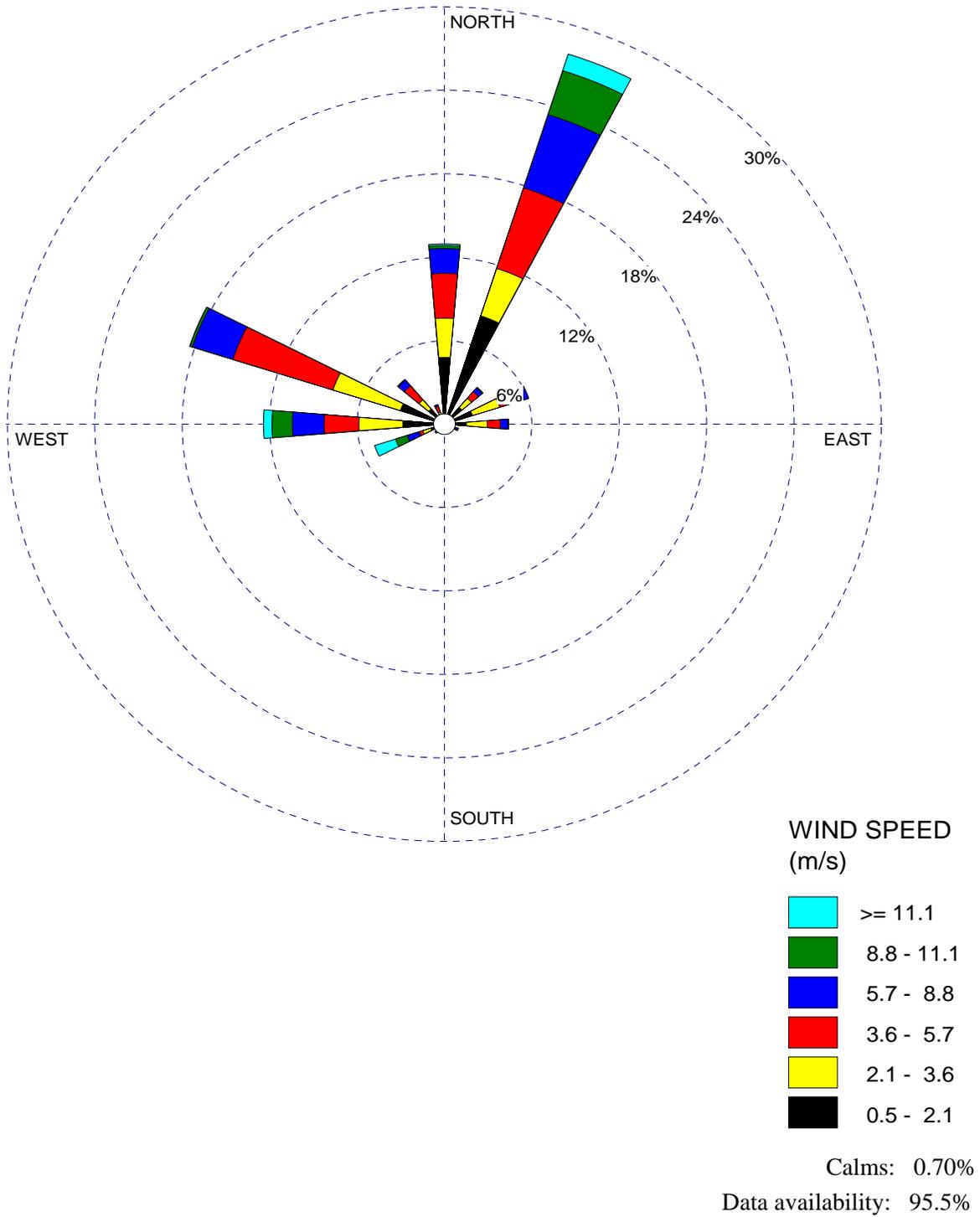


FIGURE 4-3.

ANNUAL WINDROSE FOR ONSITE MET. DATA (2000)
DAVE JOHNSON PLANT

Sources: PacifiCorp, 2006. ECT, 2006.



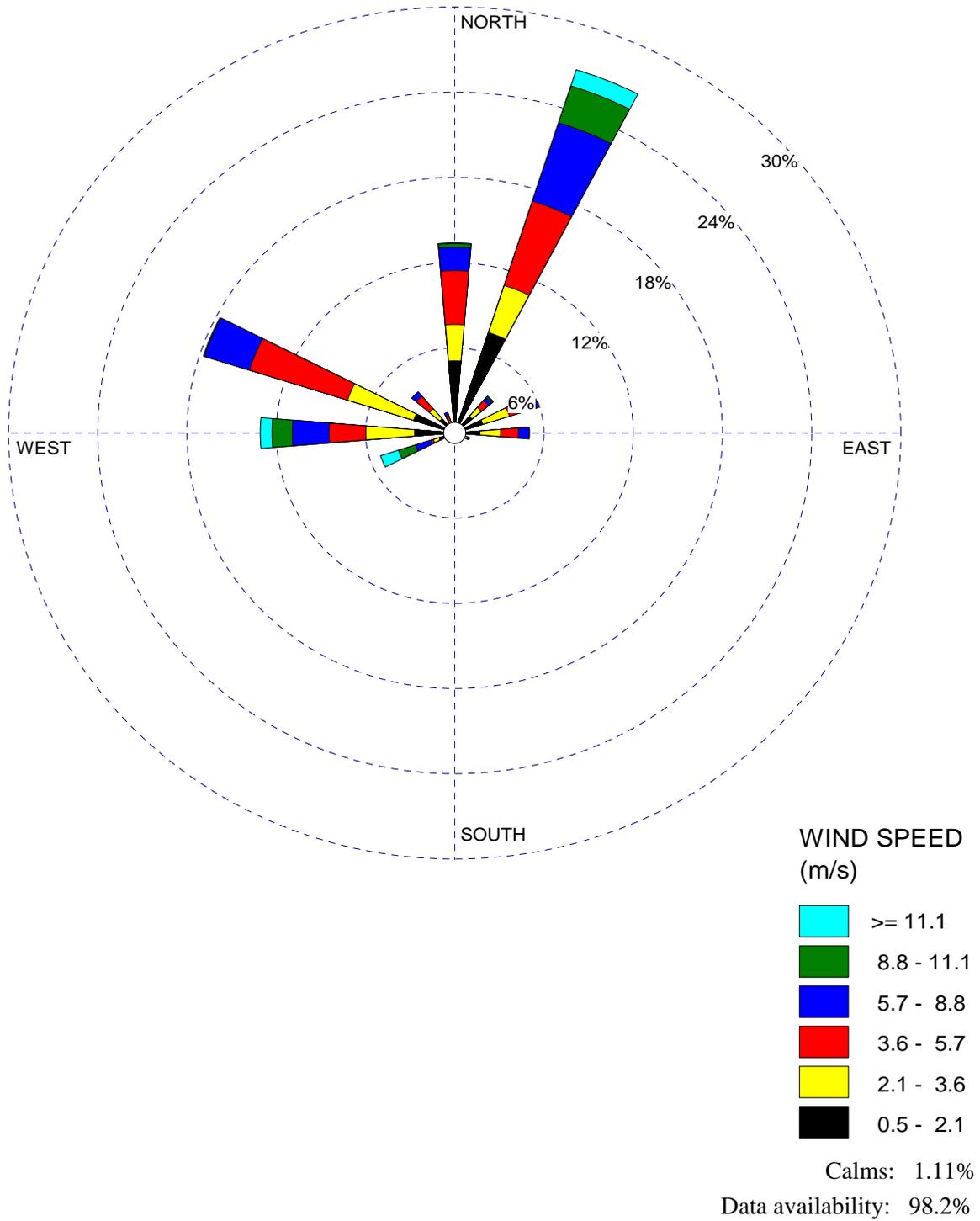


FIGURE 4-4.

ANNUAL WINDROSE FOR ONSITE MET. DATA (2001)
DAVE JOHNSON PLANT

Sources: PacifiCorp, 2006. ECT, 2006.



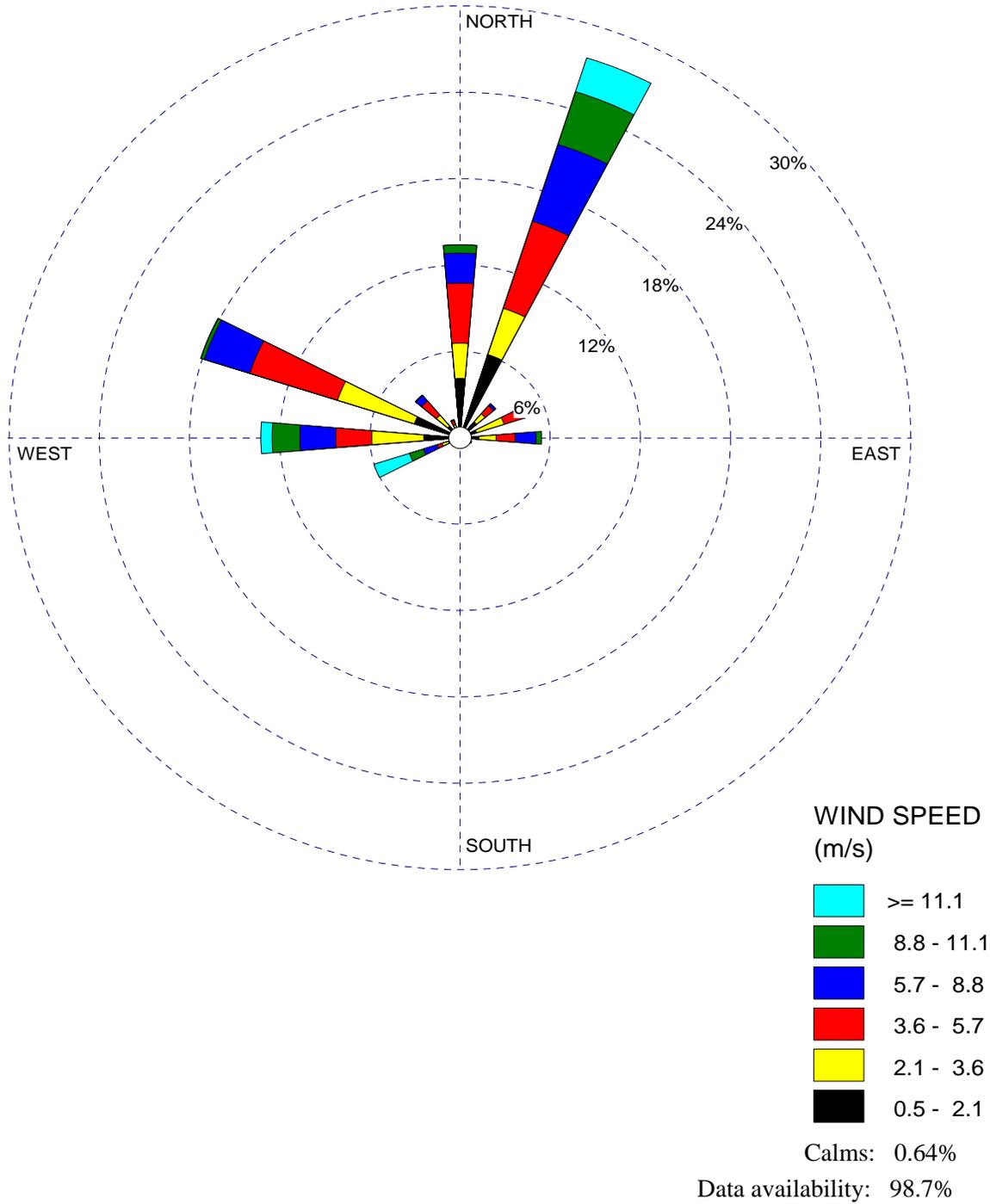


FIGURE 4-5.

ANNUAL WINDROSE FOR ONSITE MET. DATA (2002)
DAVE JOHNSON PLANT

Sources: PacifiCorp, 2006. ECT, 2006.



If one mixing height is missing, then the average of the proceeding and successive heights was substituted. For larger data gaps, interpolation between the series of mixing heights before and after the gap was used to fill the missing values.

The onsite and airport surface data were arranged in CD144 format. PCRAMMET was used to process the surface data and twice-daily mixing height observations from River-ton, Wyoming, to create the meteorological data set to be used by ISC-PRIME.

4.6 BUILDING WAKE EFFECTS

The CAA Amendments of 1990 require the degree of emission limitation required for control of any pollutant not be affected by a stack height that exceeds good engineering practice (GEP) or any other dispersion technique. On July 8, 1985, EPA promulgated fi-nal stack height regulations (40 CFR 51.100[ii]). For stacks in existence on January 12, 1979, but constructed after December 31, 1970, GEP stack height is defined as the high-est of 65 meters, or a height established by applying the formula:

$$H_g = 2.5 H$$

where: H_g = GEP stack height.

H = height of the structure or nearby structure.

Nearby is defined as a distance up to five times the lesser of the height or width dimen-sion of a structure or terrain feature, but not greater than 800 meters. While GEP stack height regulations require that stack height used in modeling for determining compliance with NAAQS and PSD increments not exceed the GEP stack height, the actual stack height may be greater. Guidelines for determining GEP stack height have been issued by EPA (1985).

Since the stacks for existing boiler Units 1 through 3 was built in 1976, the above equa-tion was used to calculate the GEP stack height. The height of the coal boiler Unit 4 is determined as a nearby structure and has a building height of 205 ft. Using the existing boiler Unit 4 height as H , the GEP stack height for the combined Units 1 through 3 stack

is determined to be 512 ft. The actual stack heights for Units 1 through 3 is 500 ft, which is below the determined GEP stack height.

For the new Unit 3 and 4 boiler stacks, an enclosure will be built around both of the stacks. The enclosure will be circular with a diameter of 18 ft and a height of 500 ft. Adding this enclosure to the BPIP analysis, the resulting GEP stack heights for Units 3 and 4 is calculated at 568 ft. The proposed 500-ft stacks for Units 3 and 4 are below the calculated GEP for these units.

While the GEP stack height rules address the maximum stack height, which can be employed in a dispersion model analysis, stacks having heights lower than GEP stack height can potentially result in higher downwind concentrations due to building downwash effects. The ISC-PRIME dispersion model contains algorithms that assess the effect of building downwash. The following steps are employed in determining the effects of building downwash:

- A determination is made as to whether a particular stack is located in the area of influence of a building (i.e., within five times the lesser of the building's height or projected width). If the stack is not within this area, it will not be subject to downwash from that building.
- If a stack is within a building's area of influence, a determination is made as to whether it will be subject to downwash based on the heights of the stack and building. If the stack height to building height ratio is equal to or greater than 2.5, the stack will not be subject to downwash from that building.
- If both conditions in Items 1 and 2 are satisfied (a stack is within the area of influence of a building and has a stack height to building height ratio of less than 2.5), the stack will be subject to building downwash. The algorithm employed by BPIP-PRIME is used to determine the effects of the nearby building.
- The ISC-PRIME downwash input data consists of an array of 36 wind direction-specific building heights and projected widths for each stack. LB is defined as the lesser of the height and projected width of the building. For di-

rectionally dependent building downwash, wake effects are assumed to occur if a stack is situated within a rectangle composed of two lines perpendicular to the wind direction, one line at 5 LB downwind of the building and the other at 2 LB upwind of the building, and by two lines parallel to the wind, each at 0.5 LB away from the side of the building.

For the air quality analysis, the complex downwash analysis described above was performed using the current version of EPA's Building Profile Input Program—PRIME (BPIPPRM—Version 04274). The BPIPPRM program was used to determine the area of influence for each building, whether a particular stack is subject to building downwash, the area of influence for directionally dependent building downwash, and finally to generate the specific building dimension data required by the ISC-PRIME model. Dimensions of the building/structures evaluated for wake effects were previously shown on Table 3-1. A three-dimensional representation of the buildings used in the downwash analysis is presented in Figure 4-6.

4.7 RECEPTOR LOCATIONS

Receptors were placed at locations considered to be *ambient air*, which is defined as “that portion of the atmosphere, external to buildings, to which the general public has access.” It is EPA policy that air quality impacts occurring at receptors on industrial property due to emission sources also located on the same industrial property do not count, with respect to determining compliance with PSD increments or AAQS.

The rectangular receptor grid included 100-meter spaced receptors out to approximately 2 km, 500-meter spaced receptors out to 5 km, 1-km spaced receptors out to 25 km, and 2-km spaced receptors out to 50 km, based on Universal Transverse Mercator (UTM) coordinate system. Receptors were also placed on the property line (or fence line) spaced every 50 meters. Additional 100-meter spaced grids were used to evaluate maximum impacts occurring outside of the near 100-meter spaced grid

Figure 4-7 shows the fence line receptors and near-field receptor grid placed on a topography map. Figure 4-8 shows the mid- and far-field receptor grids.

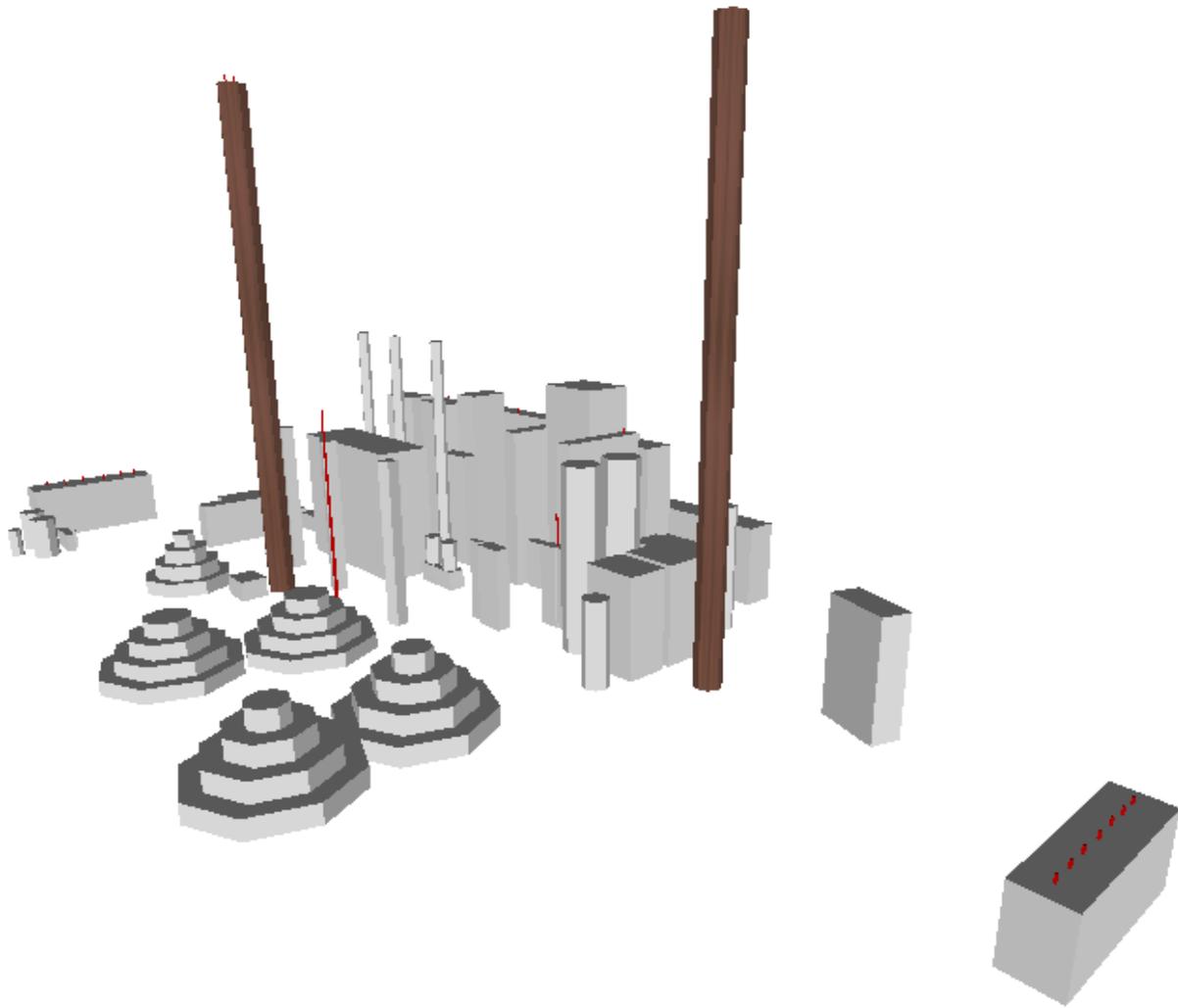


FIGURE 4-6.
BUILDING DOWNWASH PROFILE
DAVE JOHNSON PLANT
Source: ECT, 2007.



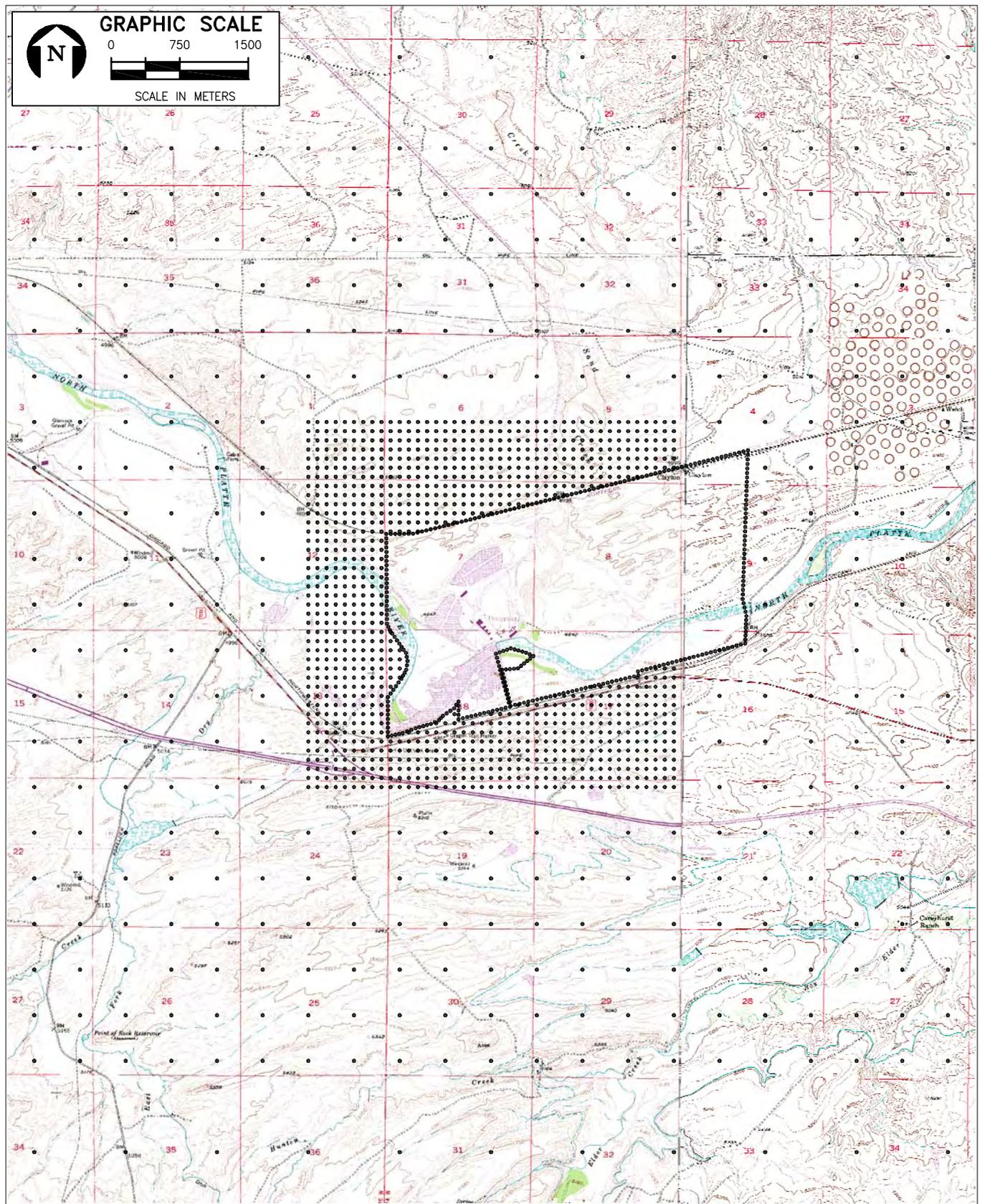


FIGURE 4-7.
LOCATION OF FENCE LINE AND NEAR-FIELD RECEPTORS

Sources: USGS Quad: Glenrock & Careyhurst, WY, 1974; ECT, 2006.

ECT
Environmental Consulting & Technology, Inc.

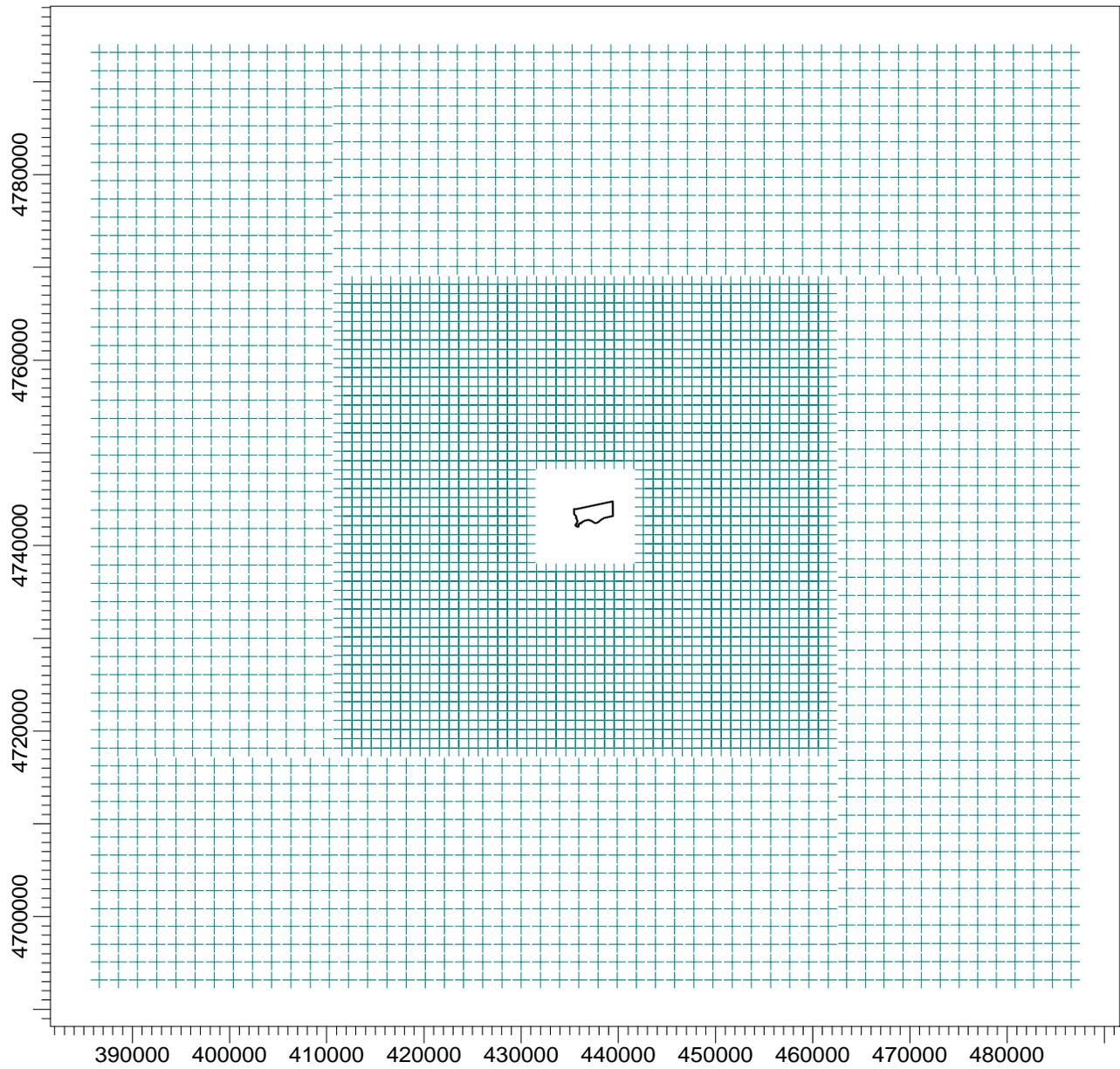


FIGURE 4-8

MID- AND FAR-FIELD RECEPTORS
1- AND 2-KM SPACING

Source: ECT, 2006.

ECT
Environmental Consulting & Technology, Inc.

It should be noted that a conservative approach was used to determine the location of the fence line. PacifiCorp's true fence line extends further than what was used for this modeling analysis, especially on the south end of the site along the North Platte River. The river was used as the property boundary when the actual southern boundary extends to the county road. This conservative approach was taken because PacifiCorp does grant public access to a small piece of land just southeast of the North Platte River dam. The submission of this fence line for the modeling analysis does not prevent PacifiCorp from submitting a less conservative fence line for future modeling analyses.

4.8 EMISSION INVENTORY

Emission rates and stack parameters for the CO, NO_x, SO₂, and PM₁₀ emission inventories are presented in Tables 4-1 through 4-4, respectively. The emission rates for Dave Johnston are derived in Appendix E of the permit application.

The stack parameters for Dave Johnston were provided by PacifiCorp. The offsite emission inventories were attained from WDEQ during a visit to the Cheyenne office. The emission inventories for some sources were further refined with assistance from WDEQ.

Table 4-1. CO Emission Inventory for the Dave Johnston PSD Significance Analysis

Source	Source Code	UTM Location		Emission Rate (g/s)	Stack Height meters	Stack Temperature K	Stack Velocity m/s	Stack Diameter meters
		Easting	Northing					
Unit 1 coal-fired boiler	DJ1	436,651	4,742,960	4.62	152.4	422	28.7	3.353
Unit 2 coal-fired boiler	DJ2	436,648	4,742,957	4.62	152.4	422	28.7	3.353
Unit 3 coal-fired boiler	DJ3	436,402	4,743,110	88.2	152.4	361	22.3	5.486
Unit 4 coal-fired boiler	DJ4	436,397	4,743,105	118.4	152.4	361	22.3	5.486

Sources: WDEQ, 2006.
ECT, 2007.

Table 4-2. NO_x Emission Inventory for the Dave Johnston WAAQS Analysis

Source	Source Code	UTM Location		Emission Rate (g/s)	Stack Height meters	Stack Temperature K	Stack Velocity m/s	Stack Diameter meters
		Eastings	Northing					
Dave Johnston Plant								
Unit 1 Coal-fired Boiler	DJ1	436,651	4,742,960	80.0	152.4	422	28.7	3.353
Unit 2 Coal-fired Boiler	DJ2	436,648	4,742,957	80.0	152.4	422	28.7	3.353
Unit 3 Coal-fired Boiler	DJ3	436,402	4,743,110	98.8	152.4	361	22.3	5.486
Unit 4 Coal-fired Boiler	DJ4	436,397	4,743,105	100.7	152.4	361	22.3	5.486
Sinclair Oil Company - Casper Refinery								
No. 4 Boiler	SRC1	398,624	4,745,609	2.02	17.7	458	6.19	1.369
No. 5 Boiler	SRC2	398,627	4,745,619	3.01	18.0	544	7.40	1.676
No. 6 Boiler	SRC3	398,629	4,745,604	0.97	41.1	527	2.49	2.134
No. 7 Boiler	SRC4	398,624	4,745,600	4.14	17.7	539	26.88	0.914
Asphalt Heater	SRC5	398,743	4,745,629	0.14	10.4	811	9.62	0.518
B-2 No. 3 Crude Heater	SRC8	398,537	4,745,598	0.60	18.3	755	13.22	0.914
B-1 No. 4 Crude Heater	SRC9	398,495	4,745,588	3.25	41.4	550	12.90	1.372
B-3 No. 4 Crude Heater	SRC7	398,528	4,745,605	1.47	41.1	575	13.80	0.914
No. 4 Vacuum Heater	SRC6	398,543	4,745,598	0.72	18.3	783	8.12	0.914
B-1 No. 5 Crude Heater	SRC11	398,312	4,745,659	2.82	18.3	811	13.40	1.524
B-1 Pretreater Heater	SRC19	398,252	4,745,662	0.61	18.4	800	7.88	1.219
B-20-1 Reformer No. 1 Heater	SRC16	398,271	4,745,663	0.79	18.3	855	17.97	0.914
B-20-2 Reformer No. 2 Heater	SRC15	398,277	4,745,662	1.36	18.5	783	38.59	0.914
B-20-2 Reformer No. 3 Heater	SRC14	398,283	4,745,662	0.62	18.3	783	20.39	0.762
B-20-3 Stabilizer Reboiler	SRC13	398,288	4,745,663	0.28	13.3	783	9.00	0.762
B-2 Splitter Reboiler	SRC17	398,265	4,745,662	0.39	18.3	816	9.13	0.914
B-201 CHD Heater	SRC18	398,246	4,745,662	0.076	18.3	728	4.80	1.219
F-202 FCC Feed Heater	SRC20	398,235	4,745,740	1.15	24.4	755	14.80	1.271
Fluid Catalyt. Cracking (FCC) Unit	SRC25	398,260	4,745,748	4.47	45.7	668	25.89	1.311
Truck Dock Flare	SRC26	398,487	4,745,471	0.30	10.7	700	8.33	2.438
Refinery Flare	SRC24	398,260	4,745,849	0.18	61.0	1273	20.19	0.945
Storage Tank Flare	SRC33	398,560	4,746,020	0.37	13.7	1033	0.06	2.438
TGTU Sulfur Recov. Unit	SRC23	398387	4745685	0.08	30.5	348	5.33	0.762
Reformer Heaters 1, 2, and 3	SRC74	398390	4745600	0.38	24.4	644	17.77	1.219

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Table 4-2. NO_x Emission Inventory for the Dave Johnston WAAQS Analysis (Continued, Page 2 of 3)

Source	Source Code	UTM Location		Emission Rate (g/s)	Stack Height meters	Stack Temperature K	Stack Velocity m/s	Stack Diameter meters
		Easting	Northing					
Kinder Morgan - Casper Extraction Plant								
Ford B6PF-6006B Fire Pump Engine	E10	398,889	4,745,343	0.009	1.7	533	14.87	0.051
Ford B6PF-6006B Fire Pump Engine	E11	398,889	4,745,343	0.009	2.5	533	14.87	0.051
1000 hp Solar T-1000 Turbine	E2	398,985	4,745,451	0.441	6.4	756	64.30	0.457
1000 hp Solar T-1000 Turbine	E3	398,983	4,745,449	0.441	6.4	756	64.30	0.457
550 hp Ingersol Rand SVG-10 Engine	E4	398,970	4,745,424	0.459	10.1	589	18.80	0.305
680 hp Ingersol Rand PSVG-10 Generator	E5	398,960	4,745,446	0.167	7.6	811	44.01	0.244
1000 hp Worthington SLCH-10	E6	398,876	4,745,390	5.556	19.8	644	33.30	0.305
2500 hp Cooper GMVH-10C Engine	E7	398,916	4,745,355	1.109	9.9	689	46.30	0.546
1000 hp Cooper GMVC-6 Engine	E8	398,877	4,745,383	4.448	19.8	650	51.10	0.396
1000 hp Cooper GMVC-6 Engine	E9	398,876	4,745,374	4.448	19.8	650	51.10	0.396
425 hp Ajax DPC-540LE	F023E	398,935	4,745,443	0.239	8.8	561	13.10	0.457
1.0 MMBtu/hr Enclosed Flare	F1	399,121	4,745,366	0.214	17.3	1273	20.00	0.305
1.0 MMBtu/hr Elevated Flare	F2	399,126	4,745,415	0.026	30.0	1273	20.00	0.203
0.75 MMBtu/hr Glycol Reboiler	H1	399,005	4,745,447	0.021	6.6	533	3.30	0.244
Lean Oil Reboiler (1 of 2 Stacks)	H21	399,000	4,745,449	0.114	19.4	533	13.17	1.219
Lean Oil Reboiler (2 of 2 Stacks)	H22	399,000	4,745,445	0.114	19.4	533	13.17	1.219
0.5 MMBtu/hr Glycol Preheater	H3	399,004	4,745,451	0.014	3.5	411	1.60	0.254
1.5 MMBtu/hr Water Tank Heater	H4	398,877	4,745,352	0.043	7.6	533	9.50	0.203
Kinder Morgan - Douglas Gas Plant								
White Superior 8G-825	DE1	470,876	4,737,734	0.366	4.6	726	38.10	0.253
White Superior 8G-825	DE2	470,886	4,737,734	0.366	4.6	723	38.10	0.253
White Superior 8G-825	DE3	470,989	4,737,734	0.366	4.6	709	38.10	0.253
White Superior 8G-825	DE4	470,905	4,737,734	0.366	4.6	714	38.10	0.253
Clark HRA-8	DE5	470,910	4,737,768	4.209	15.2	508	53.68	0.305
White Superior 8G-825	DE6	470,916	4,737,734	0.367	4.6	728	38.10	0.253

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Table 4-2. NO_x Emission Inventory for the Dave Johnston WAAQS Analysis (Continued, Page 3 of 3)

Source	Source Code	UTM Location		Emission Rate (g/s)	Stack Height meters	Stack Temperature K	Stack Velocity m/s	Stack Diameter meters
		Easting	Northing					
Clark HRA-8	DE7	470,916	4,737,768	4.209	15.2	505	53.68	0.305
Clark RA-6	DE8	470,827	4,737,661	3.533	10.7	655	54.44	0.253
Clark RA-6	DE9	470,836	4,737,661	3.533	10.7	655	54.44	0.253
Clark HRA-6	DE10	470,843	4,737,661	3.158	9.8	555	59.13	0.253
Clark HRA-6	DE11	470,851	4,737,661	3.158	10.7	551	59.13	0.253
Clark HRA-6	DE12	470,859	4,737,661	3.158	10.7	555	59.13	0.253
Clark HRA-6	DE13	470,865	4,737,661	3.158	10.4	555	46.12	0.287
Clark HRA-6	DE14	470,874	4,737,661	3.158	10.4	555	59.13	0.253
Clark RA-6	DE15	470,887	4,737,661	3.53	10.7	655	54.44	0.253
White Superior 8G-825	DE16	470,922	4,737,661	0.366	4.6	720	38.10	0.253
Clark HRA-8	DE17	470,922	4,737,768	4.209	15.2	505	53.68	0.305
Clark RA-6	DE18	470,907	4,737,661	3.533	10.7	655	54.44	0.253
Clark HRA-6	DE19	470,915	4,737,661	3.158	10.4	559	46.12	0.287
Clark HRA-6	DE20	470,924	4,737,661	3.158	10.4	556	46.12	0.204
White Superior 8G-825	DE21	470,924	4,737,734	0.366	4.6	728	38.10	0.253
Chrysler 413 Firepump	DE22	470,807	4,737,683	0.179	3.4	533	94.95	0.064
John Deere 375DLQ	DE23	471,000	4,737,608	0.397	1.5	533	77.48	0.064
Hot Oil Heater	DH1	470,973	4,737,674	0.519	15.9	555	3.74	0.991
Hot Oil Heater	DH3	470,973	4,737,664	0.26	15.9	555	1.86	0.991

Sources: WDEQ, 2006.

ECT, 2007.

Table 4-3. SO₂ Emission Inventory for the Dave Johnston WAAQS Analysis

Source	Source Code	UTM Location		Emission Rate (g/s)	Stack Height meters	Stack Temperature K	Stack Velocity m/s	Stack Diameter meters
		Eastings	Northing					
Dave Johnston Plant								
Unit 1 Coal-fired Boiler	DJ1	436,651	4,742,960	196.8	152.4	422	28.7	3.353
Unit 2 Coal-fired Boiler	DJ2	436,648	4,742,957	196.8	152.4	422	28.7	3.353
Unit 3 Coal-fired Boiler	DJ3	436,402	4,743,110	52.9	152.4	361	22.3	5.486
Unit 4 Coal-fired Boiler	DJ4	436,397	4,743,105	88.8	152.4	361	22.3	5.486
Sinclair Oil Company - Casper Refinery								
No. 4 Boiler	SRC1	398,624	4,745,609	7.3	17.7	458	6.19	1.369
No. 5 Boiler	SRC2	398,627	4,745,619	10.9	18.0	544	7.40	1.676
No. 6 Boiler	SRC3	398,629	4,745,604	0.090	41.1	527	2.49	2.134
No. 7 Boiler	SRC4	398,624	4,745,600	18.1	17.7	539	26.88	0.914
Asphalt Heater	SRC5	398,743	4,745,629	0.01	10.4	811	9.62	0.518
B-2 No. 3 Crude Heater	SRC8	398,537	4,745,598	0.06	18.3	755	13.22	0.914
B-1 No. 4 Crude Heater	SRC9	398,495	4,745,588	10.8	41.4	550	12.90	1.372
B-3 No. 4 Crude Heater	SRC7	398,528	4,745,605	4.9	41.1	575	13.80	0.914
No. 4 Vacuum Heater	SRC6	398,543	4,745,598	0.07	18.3	783	8.12	0.914
B-1 No. 5 Crude Heater	SRC11	398,312	4,745,659	9.4	18.3	811	13.40	1.524
B-1 Pretreater Heater	SRC19	398,252	4,745,662	0.060	18.4	800	7.88	1.219
B-20-1 Reformer No. 1 Heater	SRC16	398,271	4,745,663	0.080	18.3	855	17.97	0.914
B-20-2 Reformer No. 2 Heater	SRC15	398,277	4,745,662	0.15	18.5	783	38.59	0.914
B-20-2 Reformer No. 3 Heater	SRC14	398,283	4,745,662	0.060	18.3	783	20.39	0.762
B-20-3 Stabilizer Reboiler	SRC13	398,288	4,745,663	0.030	13.3	783	9.00	0.762
B-2 Splitter Reboiler	SRC17	398,265	4,745,662	0.040	18.3	816	9.13	0.914
B-201 CHD Heater	SRC18	398,246	4,745,662	0.050	18.3	728	4.80	1.219
F-202 FCC Feed Heater	SRC20	398,235	4,745,740	0.13	24.4	755	14.80	1.271
Fluid Catalyt. Cracking (FCC) Unit	SRC25	398,260	4,745,748	31.1	45.7	668	25.89	1.311
Truck Dock Flare	SRC26	398,487	4,745,471	0.010	10.7	700	8.33	2.438
Refinery Flare	SRC24	398,260	4,745,849	0.93	61.0	1273	20.19	0.945
Storage Tank Flare	SRC33	398,560	4,746,020	0.40	13.7	1033	0.06	2.438
TGTU Sulfur Recov. Unit	SRC23	398,387	4,745,685	0.58	30.5	348	5.33	0.762
Reformer Heaters 1, 2, and 3	SRC74	398,390	4,745,600	0.24	24.4	644	17.77	1.219

Sources: WDEQ, 2006.
ECT, 2007.

Table 4-4. PM₁₀ Emission Inventory for the Dave Johnston WAAQS Analysis

Source	Source Code	UTM Location		Emission Rate (g/s)	Stack Height meters	Stack Temperature K	Stack Velocity m/s	Stack Diameter meters
		Easting	Northing					
Dave Johnston Plant								
Unit 1 Coal-fired Boiler	DJ1	436,651	4,742,960	40.0	152.4	422	28.7	3.353
Unit 2 Coal-fired Boiler	DJ2	436,648	4,742,957	40.0	152.4	422	28.7	3.353
Unit 3 Coal-fired Boiler	DJ3	436,402	4,743,110	5.3	152.4	361	22.3	5.486
Unit 4 Coal-fired Boiler	DJ4	436,397	4,743,105	8.9	152.4	361	22.3	5.486
1A Tripper Deck Dust Collector	TRIP1A	436,573	4,742,829	0.00743	50.3	433	20.73	0.305
1B Tripper Deck Dust Collector	TRIP1B	436,561	4,742,818	0.00743	50.3	330	19.81	0.305
2A Tripper Deck Dust Collector	TRIP2A	436,549	4,742,855	0.00557	50.3	294	14.29	0.305
2B Tripper Decker Dust Collector	TRIP2B	436,537	4,742,844	0.00255	48.8	294	3.47	0.610
3A Tripper Decker Dust Collector	TRIP3A	436,505	4,742,893	0.0724	51.8	294	8.35	0.610
U4 Tripper Baghouse	TRIP4	436,452	4,742,923	0.354	51.8	294	23.56	0.914
U3 Tripper Deck Baghouse	TRIP3	436,462	4,742,912	0.291	48.8	294	19.32	0.914
4B Tripper Decker Dust Collector	TRIP4B	436,436	4,742,964	0.0835	51.8	294	13.81	0.610
4A Tripper Decker Dust Collector	TRIP4A	436,478	4,742,942	0.111	51.8	294	11.13	0.610
Unit 4 Lime Silo Baghouse	LIME_U4	436,474	4,743,025	0.0223	32.6	283	17.37	0.305
33/34 Baghouse	33_34BAG	436,601	4,743,007	0.0334	61.0	411	26.52	4.267
Radial Stacker	RADIAL	436,592	4,743,133	0.0211	3.0	283	8.35	0.610
Overland Conveyor	OVER	436,606	4,743,138	0.00776	3.0	283	8.35	0.610
Rail Car Load-In (West Baghouse)	RAIL_WES	437,414	4,743,508	0.279	3.0	283	97.29	0.610
Rail Car Load-In (East Baghouse)	RAIL_EAS	437,428	4,743,506	0.221	3.0	283	97.29	0.610
Unit 4 Cooling Tower - Cell 1	COOL4_C1	436,288	4,743,267	0.659	16.8	300	7.86	7.620
Unit 4 Cooling Tower - Cell 2	COOL4_C2	436,294	4,743,273	0.659	16.8	300	7.86	7.620
Unit 4 Cooling Tower - Cell 3	COOL4_C3	436,300	4,743,278	0.659	16.8	300	7.86	7.620
Unit 4 Cooling Tower - Cell 4	COOL4_C4	436,307	4,743,285	0.659	16.8	300	7.86	7.620
Unit 4 Cooling Tower - Cell 5	COOL4_C5	436,315	4,743,292	0.659	16.8	300	7.86	7.620
Unit 4 Cooling Tower - Cell 6	COOL4_C6	436,322	4,743,299	0.659	16.8	300	7.86	7.620
Unit 4 Cooling Tower - Cell 7	COOL4_C7	436,329	4,743,305	0.659	16.8	300	7.86	7.620
Cooling Tower for Units 1,2, and 3 - Cell 1	COOL1_C1	436,804	4,742,811	0.179	19.8	300	7.86	10.668
Cooling Tower for Units 1,2, and 3 - Cell 2	COOL1_C2	436,811	4,742,818	0.179	19.8	300	7.86	10.668
Cooling Tower for Units 1,2, and 3 - Cell 3	COOL1_C3	436,820	4,742,826	0.179	19.8	300	7.86	10.668

Table 4-4. PM₁₀ Emission Inventory for the Dave Johnston WAAQS Analysis (Continued, Page 2 of 3)

Source	Source Code	UTM Location		Emission Rate (g/s)	Stack Height meters	Stack Temperature K	Stack Velocity m/s	Stack Diameter meters
		Easting	Northing					
Cooling Tower for Units 1,2, and 3 - Cell 4	COOL1_C4	436,830	4,742,836	0.179	19.8	300	7.86	10.668
Cooling Tower for Units 1,2, and 3 - Cell 5	COOL1_C5	436,839	4,742,845	0.179	19.8	300	7.86	10.668
Cooling Tower for Units 1,2, and 3 - Cell 6	COOL1_C6	436,848	4,742,852	0.179	19.8	300	7.83	10.668
Ash Dumping at Landfill (Area Source)	ASH_DUMP	437,393	4,743,815	0.0038	3.0	20	20.00	0.000
Fugitives from Ash Landfill (Area Source)	ASH_LAND	437,678	4,743,635	0.8935	6.1	518	106.68	-14.590
Fly Ash Truck Loading	FLY_ASH	436,532	4,742,969	0.00384	7.6	33	12.19	47.380
Coal Pile No. 3 - Push Out (Area Source)	C_PILE3P	436,416	4,743,208	0.321	6.1	90	170.00	42.590
Ready Coal Pile No. 1 (Area Source)	C_PILE1	436,692	4,742,936	0.045	3.0	45	45.00	-24.610
Long-term Coal Storage Pile (Area Source)	C_PILELT	436,542	4,743,353	0.408	6.1	240	145.00	57.870
Ready Coal Pile No. 3 (Area Source)	C_PILE3	436,532	4,743,100	0.179	9.8	135	66.60	-46.320
Ready Coal Pile No. 2 (Area Source)	C_PILE2	436,581	4,743,019	0.162	7.9	140	65.00	-26.600
Coal Pile No. 1 Push Out (Area Source)	C_PILE1P	436,744	4,742,944	0.187	6.1	60	140.00	-32.260
Dead Storage Coal Pile (Area Source)	C_PILEDS	436,685	4,743,161	0.307	6.1	222	118.00	58.800
Ash Haul Road (Start of Line Source)	ASH_HAUL	436,537	4,742,976	0.0573				
Ash Haul Road (Finish of Line Source)	ASH_HAUL	437,409	4,743,862	-				
Sinclair Oil Company - Casper Refinery								
No. 4 Boiler	SRC1	398,624	4,745,609	1.39	17.7	458	6.19	1.369
No. 5 Boiler	SRC2	398,627	4,745,619	1.94	18.0	544	7.40	1.676
No. 6 Boiler	SRC3	398,629	4,745,604	0.018	41.1	527	2.49	2.134
No. 7 Boiler	SRC4	398,624	4,745,600	2.95	17.7	539	26.88	0.914
Asphalt Heater	SRC5	398,743	4,745,629	0.003	10.4	811	9.62	0.518
B-2 No. 3 Crude Heater	SRC8	398,537	4,745,598	0.011	18.3	755	13.22	0.914
B-1 No. 4 Crude Heater	SRC9	398,495	4,745,588	1.92	41.4	550	12.90	1.372
B-3 No. 4 Crude Heater	SRC7	398,528	4,745,605	1.00	41.1	575	13.80	0.914
No. 4 Vacuum Heater	SRC6	398,543	4,745,598	0.013	18.3	783	8.12	0.914
B-1 No. 5 Crude Heater	SRC11	398,312	4,745,659	1.705	18.3	811	13.40	1.524
B-1 Pretreater Heater	SRC19	398,252	4,745,662	0.011	18.4	800	7.88	1.219
B-20-1 Reformer No. 1 Heater	SRC16	398,271	4,745,663	0.014	18.3	855	17.97	0.914
B-20-2 Reformer No. 2 Heater	SRC15	398,277	4,745,662	0.028	18.5	783	38.59	0.914

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Table 4-4. PM₁₀ Emission Inventory for the Dave Johnston WAAQS Analysis (Continued, Page 3 of 3)

Source	Source Code	UTM Location		Emission Rate (g/s)	Stack Height meters	Stack Temperature K	Stack Velocity m/s	Stack Diameter meters
		Easting	Northing					
B-20-2 Reformer No. 3 Heater	SRC14	398,283	4,745,662	0.011	18.3	783	20.39	0.762
B-20-3 Stabilizer Reboiler	SRC13	398,288	4,745,663	0.005	13.3	783	9.00	0.762
B-2 Splitter Reboiler	SRC17	398,265	4,745,662	0.008	18.3	816	9.13	0.914
B-201 CHD Heater	SRC18	398,246	4,745,662	0.016	18.3	728	4.80	1.219
F-202 FCC Feed Heater	SRC20	398,235	4,745,740	0.024	24.4	755	14.80	1.271
Fluid Catalyt. Cracking (FCC) Unit	SRC25	398,260	4,745,748	0.955	45.7	668	25.89	1.311
Truck Dock Flare	SRC26	398,487	4,745,471	0.001	10.7	700	8.33	2.438
Refinery Flare	SRC24	398,260	4,745,849	0.006	61.0	1273	20.19	0.945
Storage Tank Flare	SRC33	398,560	4,746,020	0.001	13.7	1033	0.06	2.438
TGTU Sulfur Recov. Unit	SRC23	398,387	4,745,685	0.004	30.5	348	5.33	0.762
Reformer Heaters 1, 2, and 3	SRC74	398,390	4,745,600	0.08	24.4	644	17.77	1.219

Sources: WDEQ, 2006.
ECT, 2007.

5.0 MODEL RESULTS

5.1 PSD SIGNIFICANCE LEVELS

The refined modeling runs were conducted for CO to assess the impacts from the Dave Johnston (DJ) modifications. ISC-PRIME model results for each year of meteorology evaluated (1998, and 2000-2002) are summarized in Table 5-1 (8-hour CO impacts) and Table 5-2 (1-hour CO impacts). Highest impacts in these tables are highlighted in bold-face type. Impacts for the year 2000 were run a second time using a 100-meter space grid surrounding the maximum impact. As shown in Table 5-1, the predicted maximum impacts are below the PSD significant impact levels for both 8- and 1-hour averaging periods. Therefore, no further analysis for CO is required. The concentration isopleths and maximum impacts for the 8- and 1-hour averaging periods are shown in Figures 5-1 and 5-2, respectively.

5.2 WAAQS ANALYSIS

An assessment of the project impacts, together with other sources within 50 km, was performed for comparison to the applicable WAAQS. The final emissions inventories for NO_x, SO₂, and PM₁₀ are presented in Section 4.8. Allowable emissions were used in the modeling.

Table 5-3 provides the results of the NO_x WAAQS analysis. With background levels added in, all maximum predicted annual NO₂ impacts are well below the WAAQS. The overall maximum impact was determined using a 100-m spaced grid. The concentration isopleths, and maximum impact location are shown in Figure 5-3. As shown in Figure 5-3, the majority of the maximum impact is caused by Kinder Morgan's Douglas Gas Plant.

Tables 5-4, 5-5, and 5-6 summarize the results of the SO₂ WAAQS analyses. With background levels added in, all maximum predicted annual, 24-hour, and 3-hour SO₂ impacts are below the respective standards. For 24-hour and 3-hour averaging periods, highest, second highest impacts were used. The overall maximum impacts were determined using a 100-meter spaced grid. The concentration isopleths and maximum impact locations for

the annual, 24-hour, and 3-hour averaging periods are shown in Figures 5-4 through 5-6, respectively.

Tables 5-7 and 5-8 summarize the results of the PM₁₀ WAAQS analyses. With background levels added in, all maximum predicted annual and 24-hour PM₁₀ impacts are below the respective standards. For 24-hour averaging periods, highest, second highest impacts and background concentrations were used. The maximum overall impacts were determined using a 100-meter spaced grid. The concentration isopleths and maximum impacts location for the annual and 24-hour averaging periods are shown in Figures 5-7 and 5-8, respectively.

Table 5-9 provides the results of the lead WAAQS analysis. With background levels added in, all maximum predicted annual lead impacts are well below the WAAQS. The overall maximum impact was determined using a 100-meter spaced grid. The concentration isopleth and maximum impact location are shown in Figure 5-9.

Table 5-10 provides the results of the fluoride WAAQS analysis. Background levels could not be determined, therefore the maximum impacts from Dave Johnston were compared to the 12-hour, 24-hour, 30-day, and annual average WAAQS. The overall maximum impact was determined using a 100-meter spaced grid. The concentration isopleth and maximum impact locations for the 30-day, 24-hour, and 12-hour averaging periods are shown in Figures 5-10 through 5-12, respectively.

Table 5-1. ISC-PRIME Model Results—Maximum 8-Hour Average CO Impacts for Dave Johnston PSD Significance Comparison

Maximum 8-Hour Impacts	1998	2000	2001	2002
ISC-PRIME Impact ($\mu\text{g}/\text{m}^3$)	91.0	121.9	105.4	96.8
PSD Significant Impact ($\mu\text{g}/\text{m}^3$)	500	500	500	500
Exceed PSD Significant Impact (Yes/No)	No	No	No	No
Percent of PSD Significant Impact (%)	18.2	24.4	21.1	19.4
PSD <i>de minimis</i> Ambient Impact Threshold ($\mu\text{g}/\text{m}^3$)	575.0	575.0	575.0	575.0
Exceed PSD <i>de minimis</i> Ambient Impact (Yes/No)	No	No	No	No
Percent of PSD <i>de minimis</i> Ambient Impact (%)	15.8	21.2	18.3	16.8
Receptor UTM Easting (meters)	434,595	442,770	433,595	435,595
Receptor UTM Northing (meters)	4,736,155	4,733,981	4,735,155	4,736,155
Distance From Grid Origin (meters)	7,105	10,984	8,366	6,905
Direction From Grid Origin (Vector $^{\circ}$)	196	145	200	188
Date of Maximum Impact	06/21/98	07/15/00	10/28/01	07/05/02
Julian Date of Maximum Impact	172	197	301	186
Ending Hour of Maximum Impact	0800	0800	2400	0800

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.

Table 5-2. ISC-PRIME Model Results—Maximum 1-Hour Average CO Impacts for the Dave Johnston PSD Significance Comparison

Maximum 1-Hour Impacts	1998	2000	2001	2002
ISC-PRIME Impact ($\mu\text{g}/\text{m}^3$)	511.0	647.7	499.5	534.8
PSD Significant Impact ($\mu\text{g}/\text{m}^3$)	2,000	2,000	2,000	2,000
Exceed PSD Significant Impact (Yes/No)	No	No	No	No
Percent of PSD Significant Impact (%)	25.6	32.4	25.0	26.7
Receptor UTM Easting (meters)	436,595	435,494	435,595	435,595
Receptor UTM Northing (meters)	4,735,155	4,736,640	4,736,155	4,737,155
Distance From Grid Origin (meters)	7,846	6,439	6,905	5,915
Direction From Grid Origin (Vector $^{\circ}$)	179	189	188	189
Date of Maximum Impact	07/28/98	10/05/00	09/04/01	02/11/02
Julian Date of Maximum Impact	209	279	247	42
Ending Hour of Maximum Impact	0100	0100	2300	2300

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.

Table 5-3. ISC-PRIME Model Results—Annual Average NO₂ Impacts for Dave Johnston WAAQS Analysis

Maximum Annual Impacts	1998	2000	2001	2002
ISC-PRIME NO _x Impact (µg/m ³)	67.6	72.9	70.9	67.8
Tier 1 Impact (µg/m ³)*	67.6	72.9	70.9	67.8
Tier 2 Impact (µg/m ³)†	50.7	54.7	53.2	50.9
Background (µg/m ³)	9.40	9.40	9.40	9.40
Total WAAQS Impact (µg/m ³)	60.1	64.1	62.6	60.3
Maximum NO ₂ Impact for DJ (µg/m ³)	5.46	5.63	5.69	5.55
WAAQS (µg/m ³)	100	100	100	100
Exceed WAAQS (Yes/No)	No	No	No	No
Percent of WAAQS (%)	60.1	64.1	62.6	60.3
WAAQS Impact Receptor UTM Easting (meters)	473,036	473,036	473,036	473,036
WAAQS Receptor UTM Northing (meters)	4,737,279	4,737,279	4,737,279	4,737,279
Distance From Plant Bench Mark (meters)	36,981	36,981	36,981	36,981
Direction From Plant Bench Mark (Vector °)	99	99	99	99

Note: Highest impact year highlighted in **boldface** type.

*Unadjusted ISC-PRIME impact (assumed complete conversion of NO_x to NO₂; i.e., NO₂/NO_x ratio of 1.0).

†Tier 1 impact times USEPA national default NO₂/NO_x ratio of 0.75.

Source: ECT, 2007.

Table 5-4. ISC-PRIME Model Results—Annual Average SO₂ Impacts for the Dave Johnston WAAQS Analysis

Maximum Annual Impacts	1998	2000	2001	2002
ISC-PRIME Impact (µg/m ³)	22.2	37.5	23.5	23.1
Background (µg/m ³)	10.5	10.5	10.5	10.5
Total WAAQS Impact (µg/m ³)	32.7	48.0	34.0	33.6
Maximum Impact for DJ (µg/m ³)	12.7	13.0	12.7	13.0
WAAQS (µg/m ³)	60	60	60	60
Exceed WAAQS (Yes/No)	No	No	No	No
Percent of WAAQS (%)	54.5	80.0	56.6	56.0
Percent of Impact from Dave Johnston (%)	65.0	28.3	58.8	60.7
WAAQS Receptor UTM Easting (meters)	403,903	399,938	403,903	403,903
WAAQS Receptor UTM Northing (meters)	4,743,813	4,744,901	4,743,813	4,743,813
Distance From Plant Bench Mark (meters)	32,607	36,611	32,607	32,607
Direction From Plant Bench Mark (Vector °)	271	273	271	271

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.

Table 5-5. ISC-PRIME Model Results—Highest, Second Highest 24-Hour Average SO₂ Impacts for the Dave Johnston WAAQS Analysis

HSH 24-Hour Average Impacts	1998	2000	2001	2002
ISC-PRIME HSH Impact (µg/m ³)	138.2	179.2	140.0	109.4
Background (µg/m ³)	68.1	68.1	68.1	68.1
Total WAAQS Impact (µg/m ³)	206.3	247.3	208.1	177.5
WAAQS (µg/m ³)	260	260	260	260
Exceed WAAQS (Yes/No)	No	No	No	No
Percent of WAAQS (%)	79.3	95.1	80.0	68.3
Percent of Impact from Dave Johnston (%)	99.8	55.0	100.0	93.4
WAAQS Receptor UTM Easting (meters)	436,388	399,938	436,770	403,903
WAAQS Receptor UTM Northing (meters)	4,742,632	4,744,901	4,742,661	4,743,813
Distance From Plant Bench Mark (meters)	385	36,611	433	32,607
Direction From Plant Bench Mark (Vector °)	197	273	141	271
Date of Maximum HSH Impact	04/19/98	03/30/00	04/11/01	02/07/02
Julian Date of Maximum HSH Impact	109	90	101	38

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.

Table 5-6. ISC-PRIME Model Results—Highest, Second Highest 3-Hour Average SO₂ Impacts for the Dave Johnston WAAQS Analysis

HSH 3-Hour Average Impacts	1998	2000	2001	2002
ISC-PRIME HSH Impact (µg/m ³)	627.3	789.5	725.4	535.6
Background (µg/m ³)	125.8	125.8	125.8	125.8
Total WAAQS Impact (µg/m ³)	753.1	915.3	851.2	661.4
Maximum HSH Impact for DJ (µg/m ³)	584.1	735.2	552.2	584.2
WAAQS (µg/m ³)	1,300	1,300	1,300	1,300
Exceed WAAQS (Yes/No)	No	No	No	No
Percent of WAAQS (%)	57.9	70.4	65.5	50.9
WAAQS Receptor UTM Easting (meters)	437,017	428,625	436,647	436,688
WAAQS Receptor UTM Northing (meters)	4,742,609	4,737,093	4,742,618	4,742,632
Distance From Plant Bench Mark (meters)	648	9,844	409	413
Direction From Plant Bench Mark (Vector °)	127	233	159	153
Date of Maximum HSH Impact	06/18/98	12/01/00	04/11/01	08/14/02
Julian Date of Maximum HSH Impact	169	336	101	226
Ending Hour of Maximum Impact	1800	2400	0600	2400

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.

Table 5-7. ISC-PRIME Model Results—Annual Average PM₁₀ Impacts for the Dave Johnston WAAQS Analysis

Maximum Annual Impacts	1998	2000	2001	2002
ISC-PRIME Impact (µg/m ³)	9.8	10.8	10.4	10.1
Background (µg/m ³)	17.0	17.0	17.0	17.0
Total WAAQS Impact (µg/m ³)	26.8	27.8	27.4	27.1
Maximum Impact for DJ (µg/m ³)	11.9	13.3	13.1	11.8
WAAQS (µg/m ³)	50	50	50	50
Exceed WAAQS (Yes/No)	No	No	No	No
Percent of WAAQS (%)	53.5	55.6	54.8	54.2
WAAQS Receptor UTM Easting (meters)	439,355	439,355	439,355	439,354
WAAQS Receptor UTM Northing (meters)	4,743,414	4,743,414	4,743,414	4,743,365
Distance From Plant Bench Mark (meters)	2,885	2,885	2,885	2,877
Direction From Plant Bench Mark (Vector °)	82	82	82	83

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.

Table 5-8. ISC-PRIME Model Results—Highest, Second Highest 24-Hour Average PM₁₀ Impacts for the Dave Johnston WAAQS Analysis

HSH 24-Hour Average Impacts	1998	2000	2001	2002
ISC-PRIME HSH Impact (µg/m ³)	64.0	56.7	65.6	50.5
Background (µg/m ³)	47.0	47.0	47.0	47.0
Total WAAQS Impact (µg/m ³)	111.0	103.7	112.6	97.5
Maximum HSH Impact for DJ (µg/m ³)	61.4	58.1	51.1	45.9
WAAQS (µg/m ³)	150	150	150	150
Exceed WAAQS (Yes/No)	No	No	No	No
Percent of WAAQS (%)	74.0	69.1	75.1	65.0
WAAQS Receptor UTM Easting (meters)	436,688	436,811	439,397	439,354
WAAQS Receptor UTM Northing (meters)	4,742,632	4,742,675	4,744,598	4,743,365
Distance From Plant Bench Mark (meters)	413	450	3,309	2,877
Direction From Plant Bench Mark (Vector °)	153	136	61	83
Date of Maximum HSH Impact	06/14/98	07/15/00	11/14/01	10/17/02
Julian Date of Maximum HSH Impact	165	197	318	290

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.

Table 5-9. ISC-PRIME Model Results—Quarterly Average Lead Impacts for the Dave Johnston WAAQS Analysis

Maximum Quarterly Impacts	1998	2000	2001	2002
ISC-PRIME Monthly Impact for DJ ($\mu\text{g}/\text{m}^3$)*	0.00022	0.00027	0.00023	0.00022
Background ($\mu\text{g}/\text{m}^3$)	0.10	0.10	0.10	0.10
Total WAAQS Impact ($\mu\text{g}/\text{m}^3$)	0.10	0.10	0.10	0.10
WAAQS ($\mu\text{g}/\text{m}^3$)	1.5	1.5	1.5	1.5
Exceed WAAQS (Yes/No)	No	No	No	No
Percent of WAAQS (%)	6.7	6.7	6.7	6.7
WAAQS Receptor UTM Easting (meters)	439,595	441,194	427,595	440,095
WAAQS Receptor UTM Northing (meters)	4,741,155	4,740,778	4,738,155	4,741,155
Distance From Plant Bench Mark (meters)	3,603	5,193	10,138	4,041
Direction From Plant Bench Mark (Vector °)	121	115	241	117

*30-day average impact was conservatively used for quarterly average impact.

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.

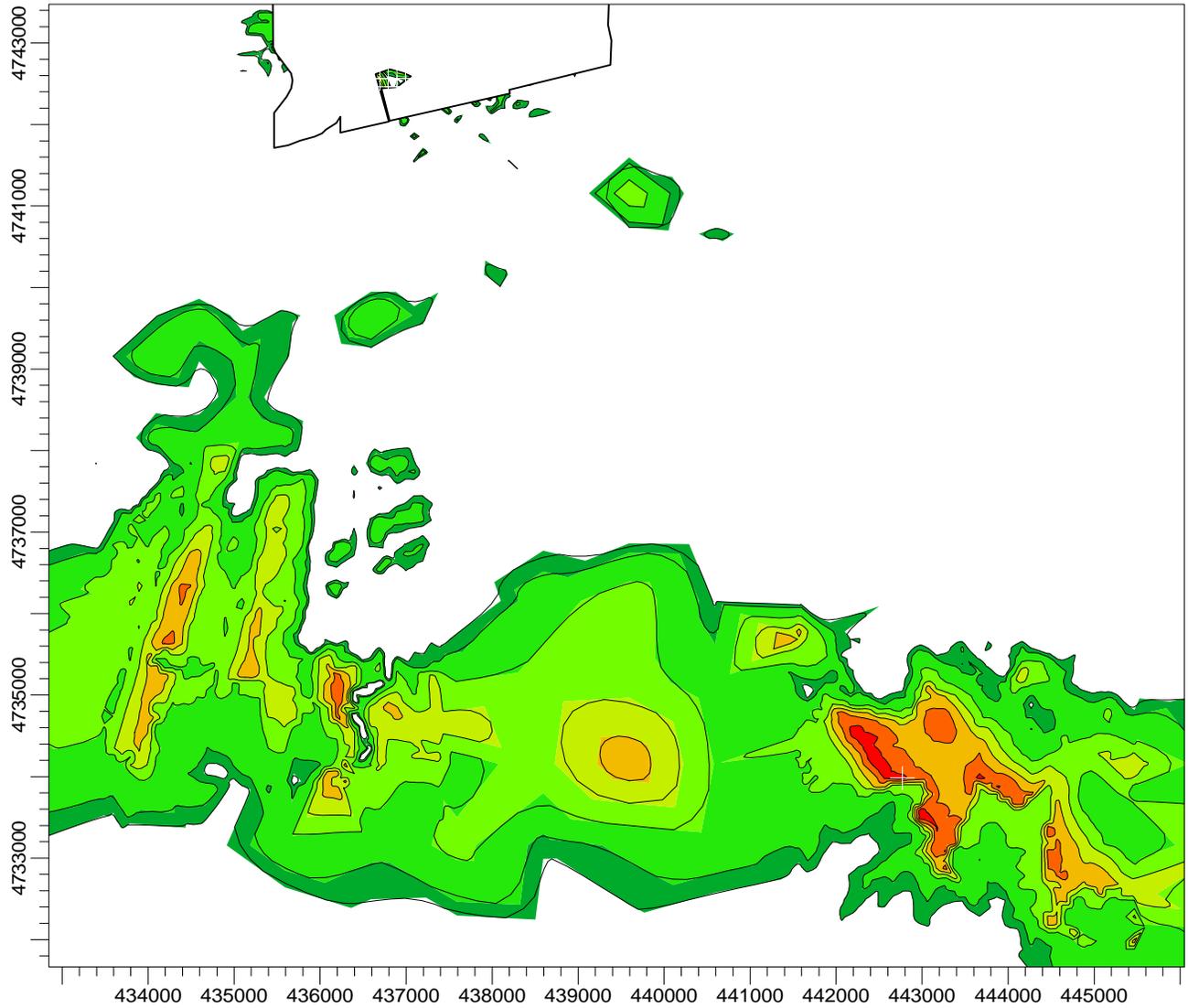
Table 5-10. ISC-PRIME Model Results—Fluoride Impacts for the Dave Johnston WAAQS Analysis

Maximum Impacts	1998	2000	2001	2002
ISC-PRIME 12-hour Impact from DJ ($\mu\text{g}/\text{m}^3$)	0.93	0.78	1.50	0.68
12-hour WAAQS ($\mu\text{g}/\text{m}^3$)	3.0	3.0	3.0	3.0
ISC-PRIME 24-hour Impact from DJ ($\mu\text{g}/\text{m}^3$)	0.70	0.49	1.01	0.37
24-hour WAAQS ($\mu\text{g}/\text{m}^3$)	1.8	1.8	1.8	1.8
ISC-PRIME 7-day Impact from DJ ($\mu\text{g}/\text{m}^3$)*	0.13	0.16	0.14	0.13
7-day WAAQS ($\mu\text{g}/\text{m}^3$)	0.5	0.5	0.5	0.5
ISC-PRIME 30-day Impact from DJ ($\mu\text{g}/\text{m}^3$)	0.061	0.075	0.067	0.065
30-day WAAQS ($\mu\text{g}/\text{m}^3$)	0.4	0.4	0.4	0.4
ISC-PRIME Annual Impact from DJ ($\mu\text{g}/\text{m}^3$)	0.042	0.039	0.040	0.041
Annual WAAQS ($\mu\text{g}/\text{m}^3$)	23,310	23,310	23,310	23,310
Exceed WAAQS (Yes/No)	No	No	No	No

*30-day impact used to estimate 7-day impact using $C_{\text{new}} = C_{\text{old}} \times (T_{\text{old}}/T_{\text{new}})^{0.5}$.

Note: Highest impact year highlighted in **boldface** type.

Source: ECT, 2007.



ug/m³



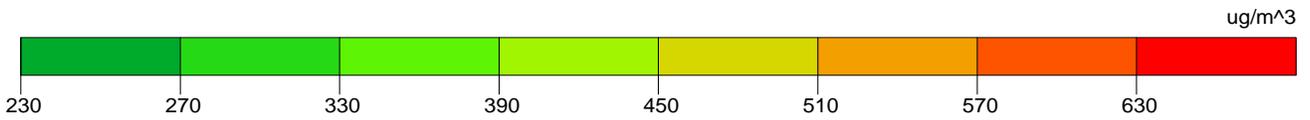
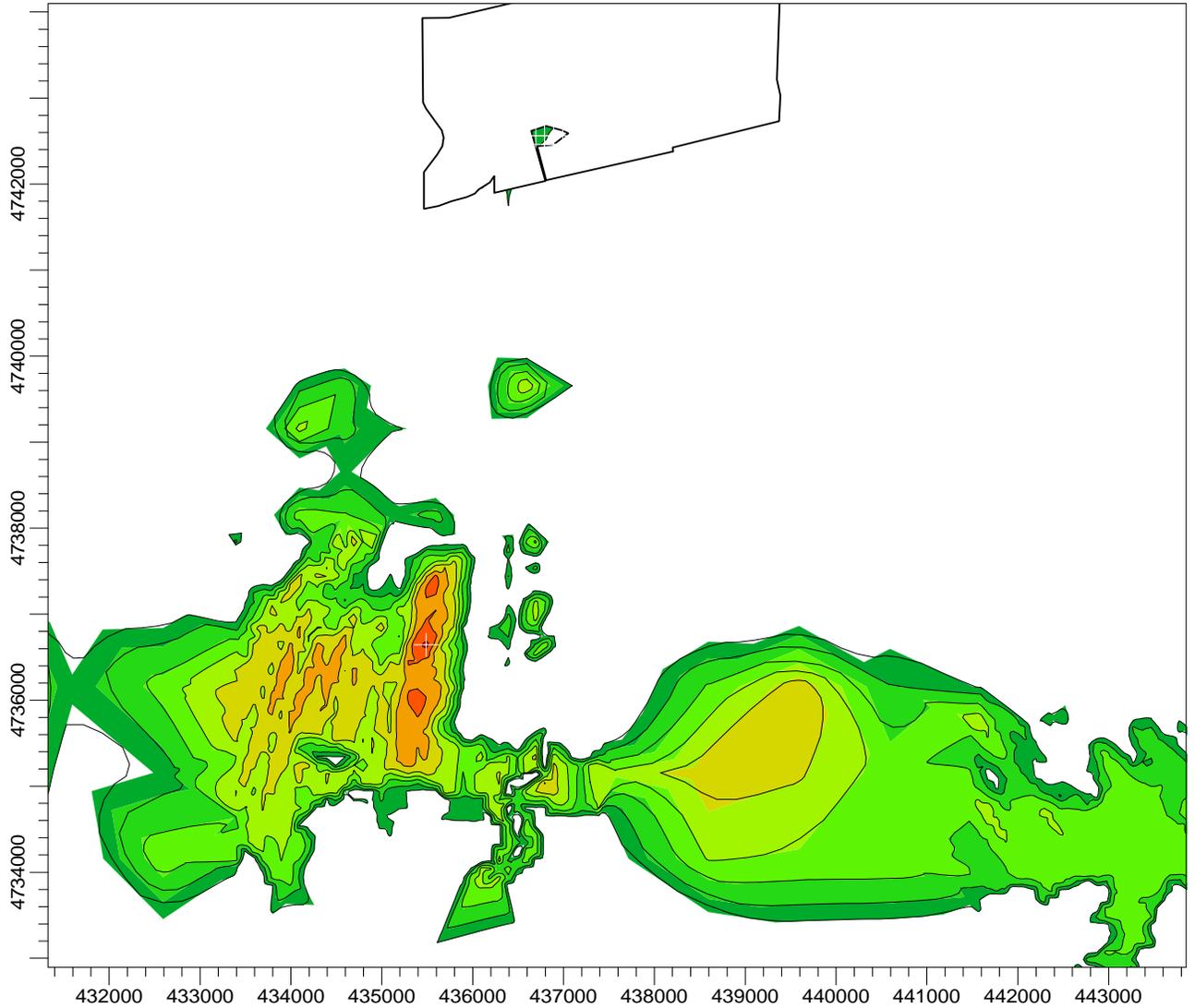
+ Highest 8-hr Average Concentration = 121.9 $\mu\text{g}/\text{m}^3$

FIGURE 5-1.

2000 CO IMPACTS—DJ PSD SIGNIFICANCE ANALYSIS
CONCENTRATION ISOPLETH - 8-HR AVERAGE

Source: ECT, 2007.

ECT
Environmental Consulting & Technology, Inc.



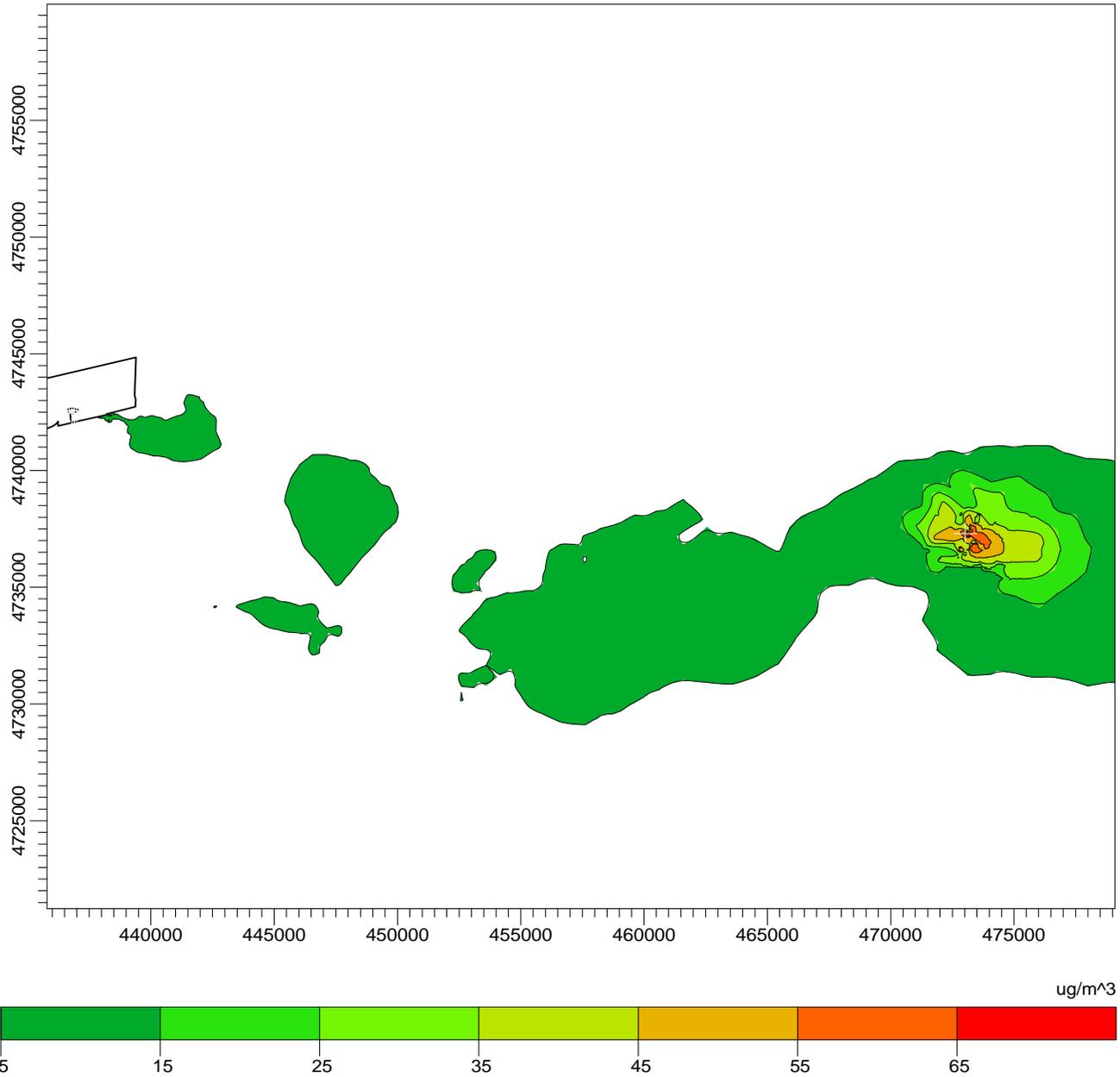
+ Highest 1-hr Average Concentration = 647.7 $\mu\text{g}/\text{m}^3$

FIGURE 5-2.

2000 CO IMPACTS—DJ PSD SIGNIFICANCE ANALYSIS
 CONCENTRATION ISOPLETH - 1-HR AVERAGE

Source: ECT, 2007.

ECT
 Environmental Consulting & Technology, Inc.



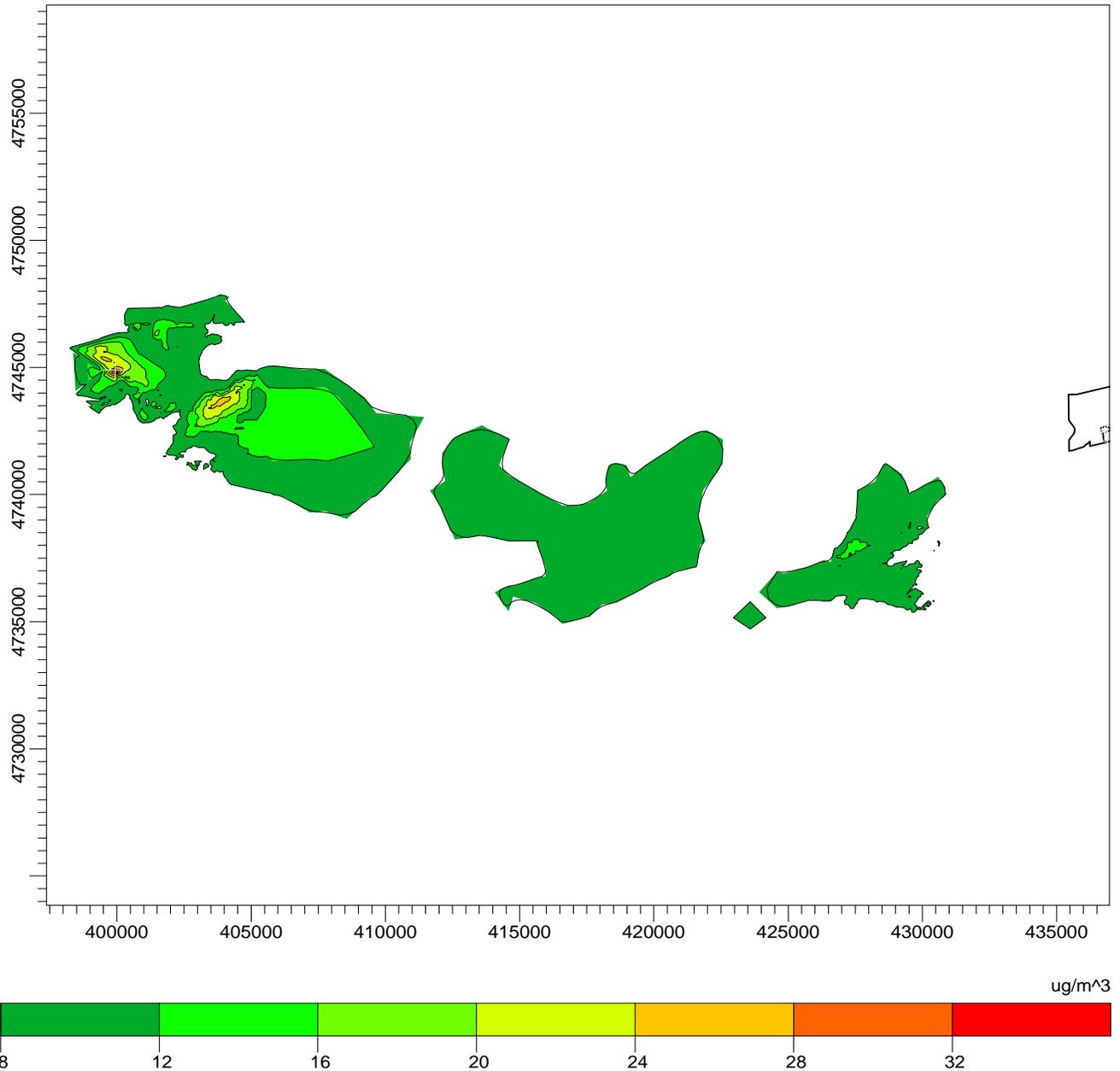
+ Highest Annual Average NO_x Concentration = 72.9 μg/m³

FIGURE 5-3.

2000 NO_x IMPACTS—DJ WAAQS ANALYSIS
 CONCENTRATION ISOPLETH - ANNUAL AVERAGE

Source: ECT, 2006.





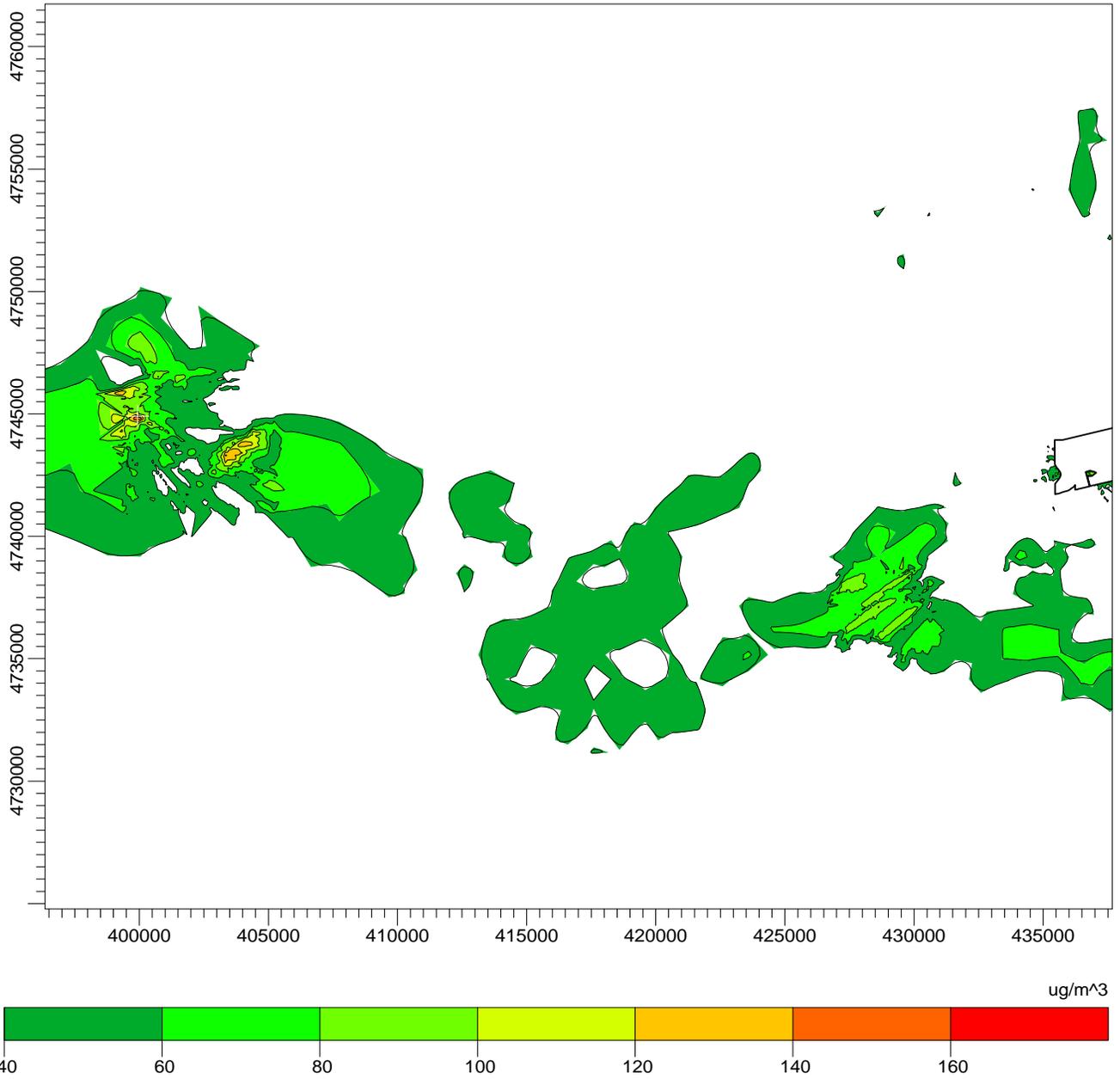
+ Highest Annual Average Concentration = 37.5 $\mu\text{g}/\text{m}^3$

FIGURE 5-4.

2000 SO₂ IMPACTS—DJ WAAQS ANALYSIS
CONCENTRATION ISOPLETH - ANNUAL AVERAGE

Source: ECT, 2006.



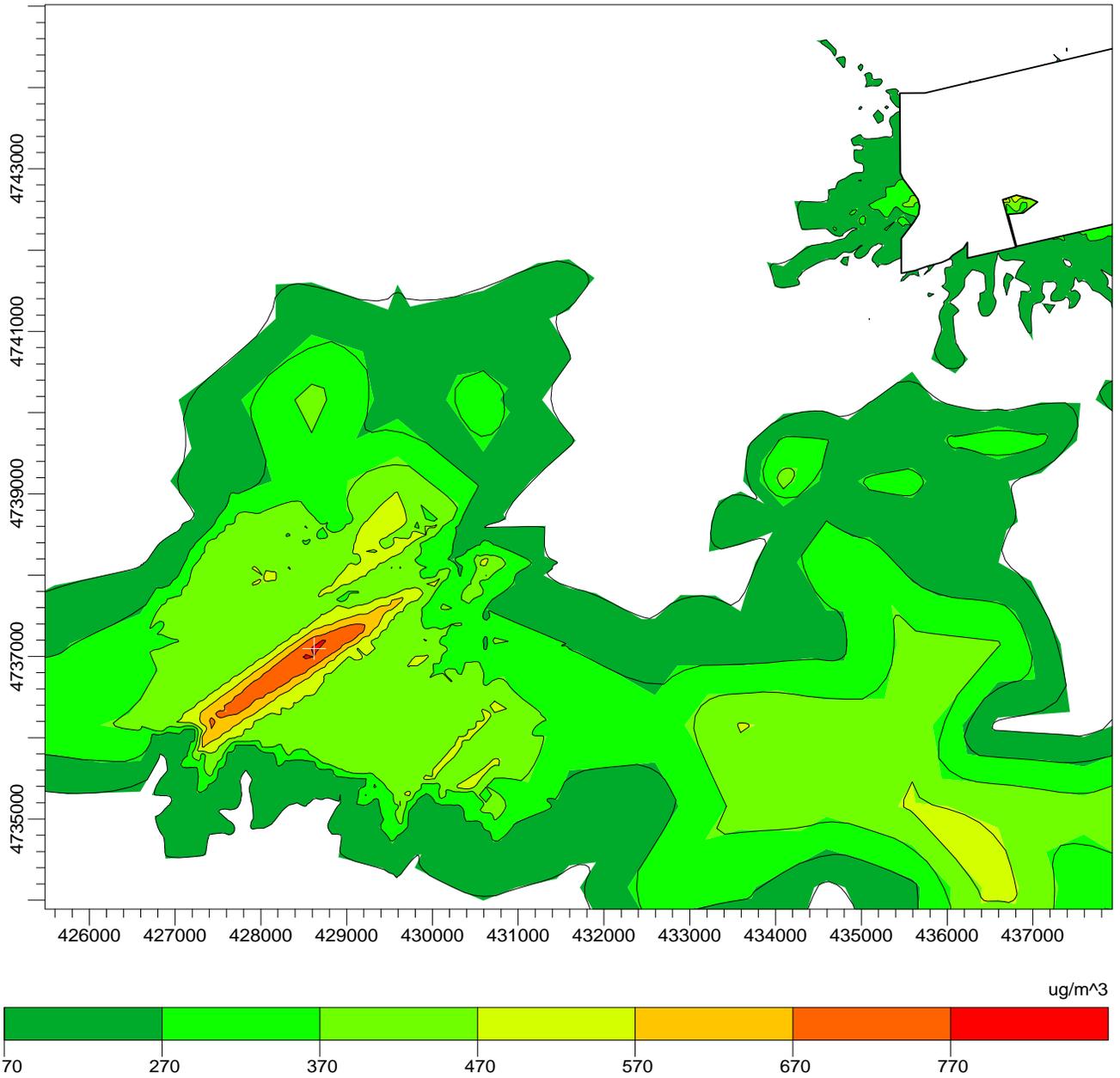


+ HSH 24-Hr Average Concentration = 179.2 $\mu\text{g}/\text{m}^3$

FIGURE 5-5.

2000 SO₂ IMPACTS—DJ WAAQS ANALYSIS
 CONCENTRATION ISOPLETH - 24-HR AVERAGE HSH
 Source: ECT, 2006.



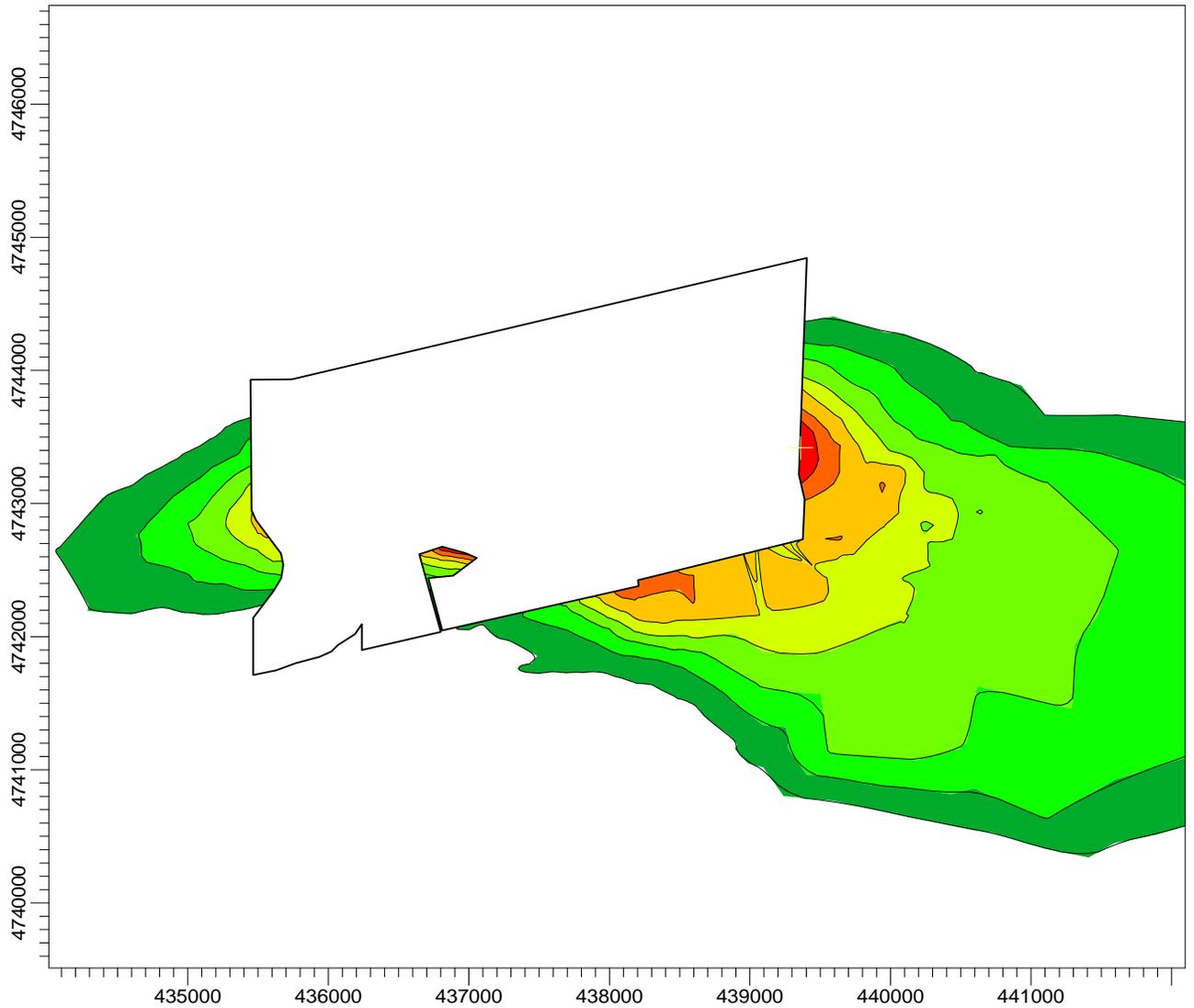


+ HSH 3-Hr Average Concentration = 789.5 $\mu\text{g}/\text{m}^3$

FIGURE 5-6.

2000 SO₂ IMPACTS—DJ WAAQS ANALYSIS
CONCENTRATION ISOPLETH - 3-HR AVERAGE HSH
Source: ECT, 2006.





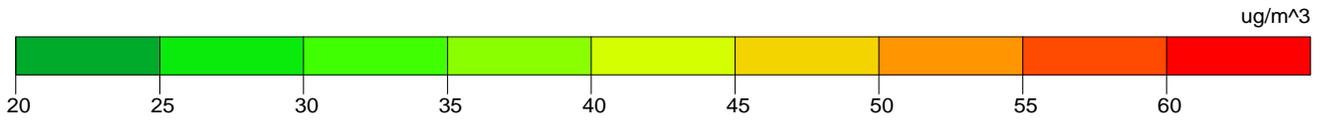
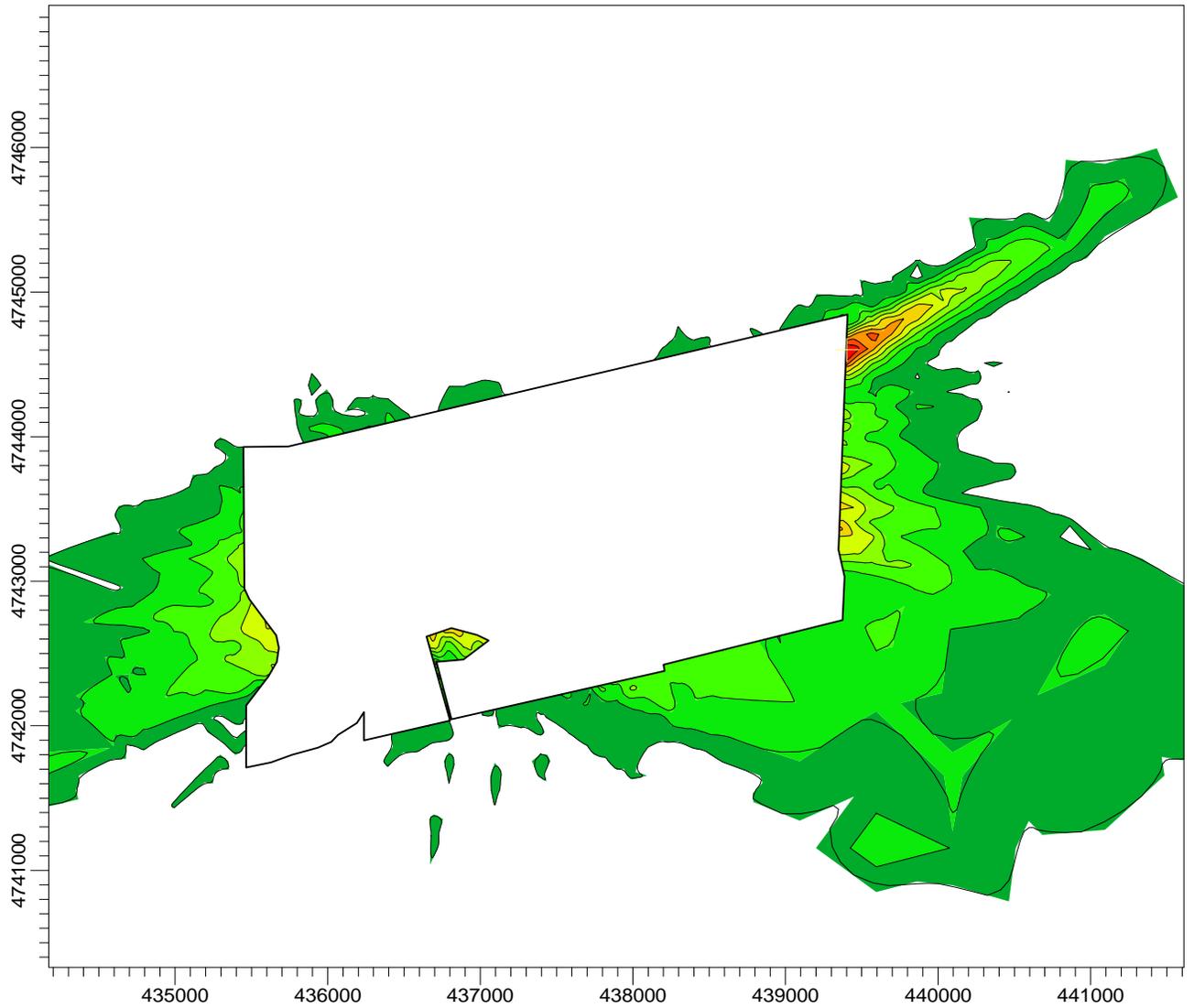
+ Highest Annual Average Concentration = 10.8 $\mu\text{g}/\text{m}^3$

FIGURE 5-7.

2000 PM₁₀ IMPACTS— DJ WAAQS ANALYSIS
CONCENTRATION ISOPLETH - ANNUAL AVERAGE

Source: ECT, 2006.



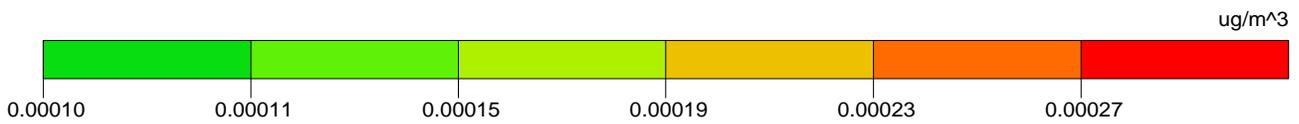
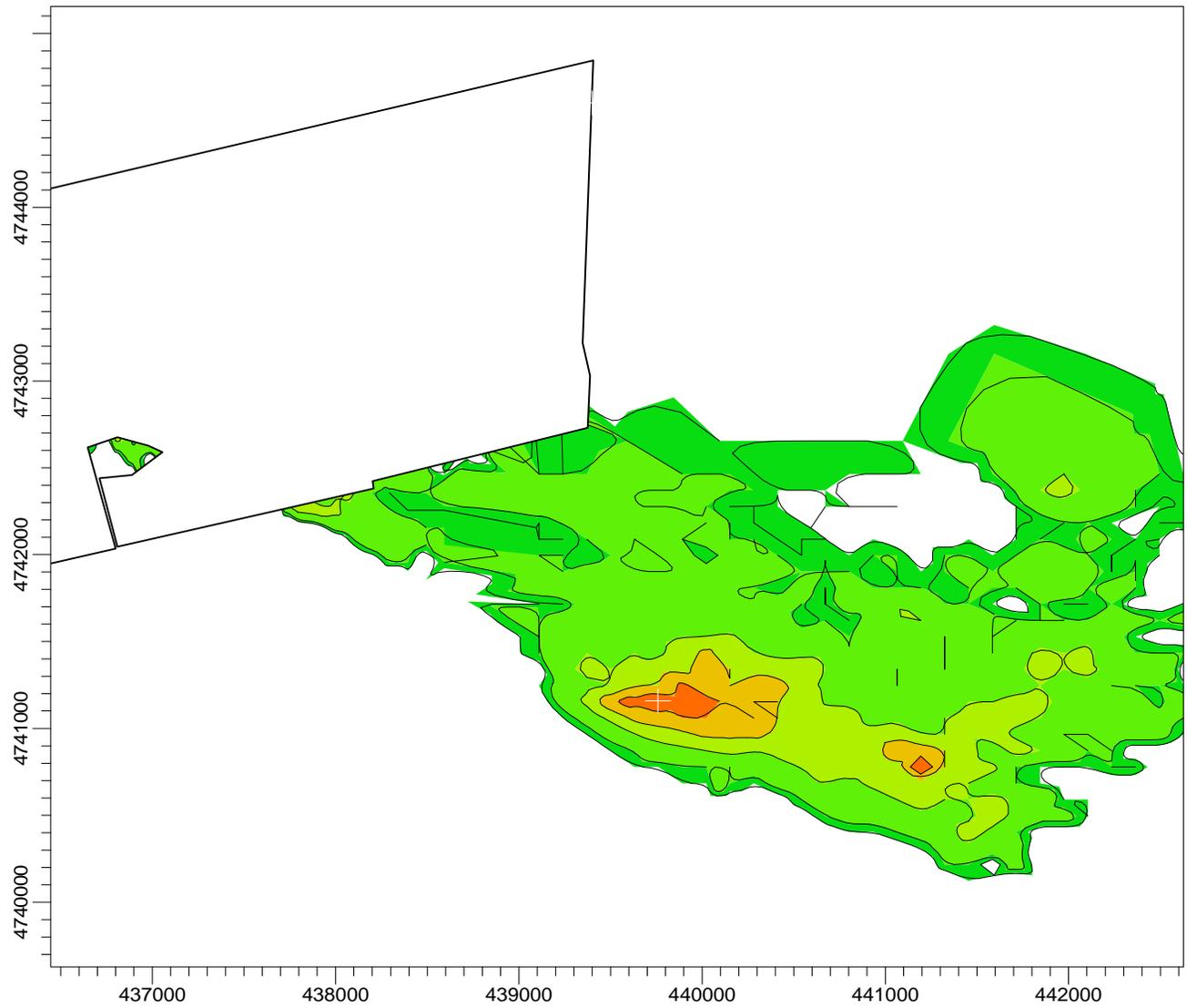


+ HSH 24-Hr Average Concentration = 65.6 $\mu\text{g}/\text{m}^3$

FIGURE 5-8.

2001 PM₁₀ IMPACTS—DJ WAAQS ANALYSIS
 CONCENTRATION ISOPLETH - 24-HOUR AVERAGE HSH
 Source: ECT, 2006.





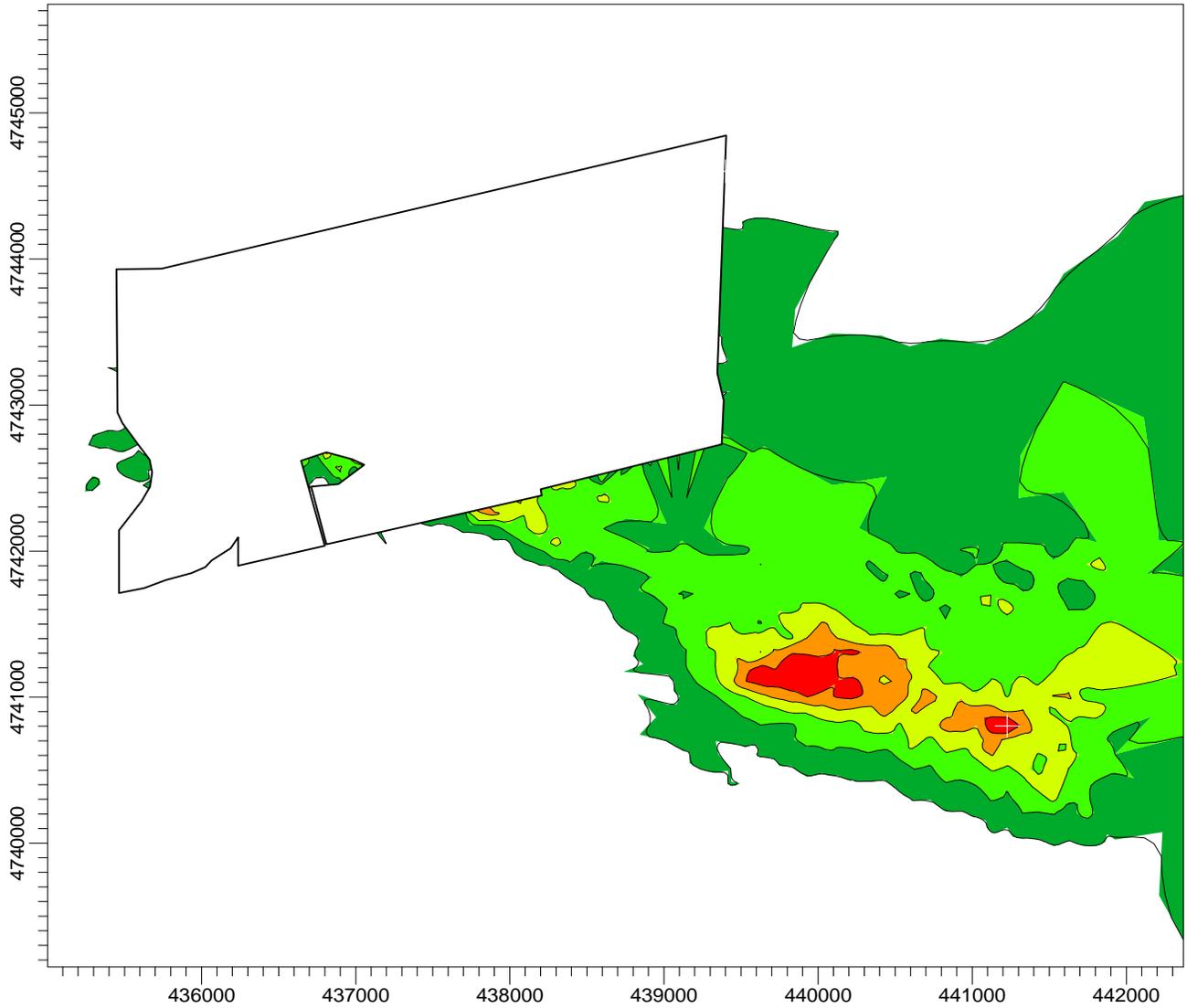
+ Highest Monthly Average Concentration = 0.00027 $\mu\text{g}/\text{m}^3$

FIGURE 5-9.

2000 LEAD IMPACTS—DJ WAAQS ANALYSIS
 CONCENTRATION ISOPLETH - MONTHLY AVERAGE

Source: ECT, 2006.





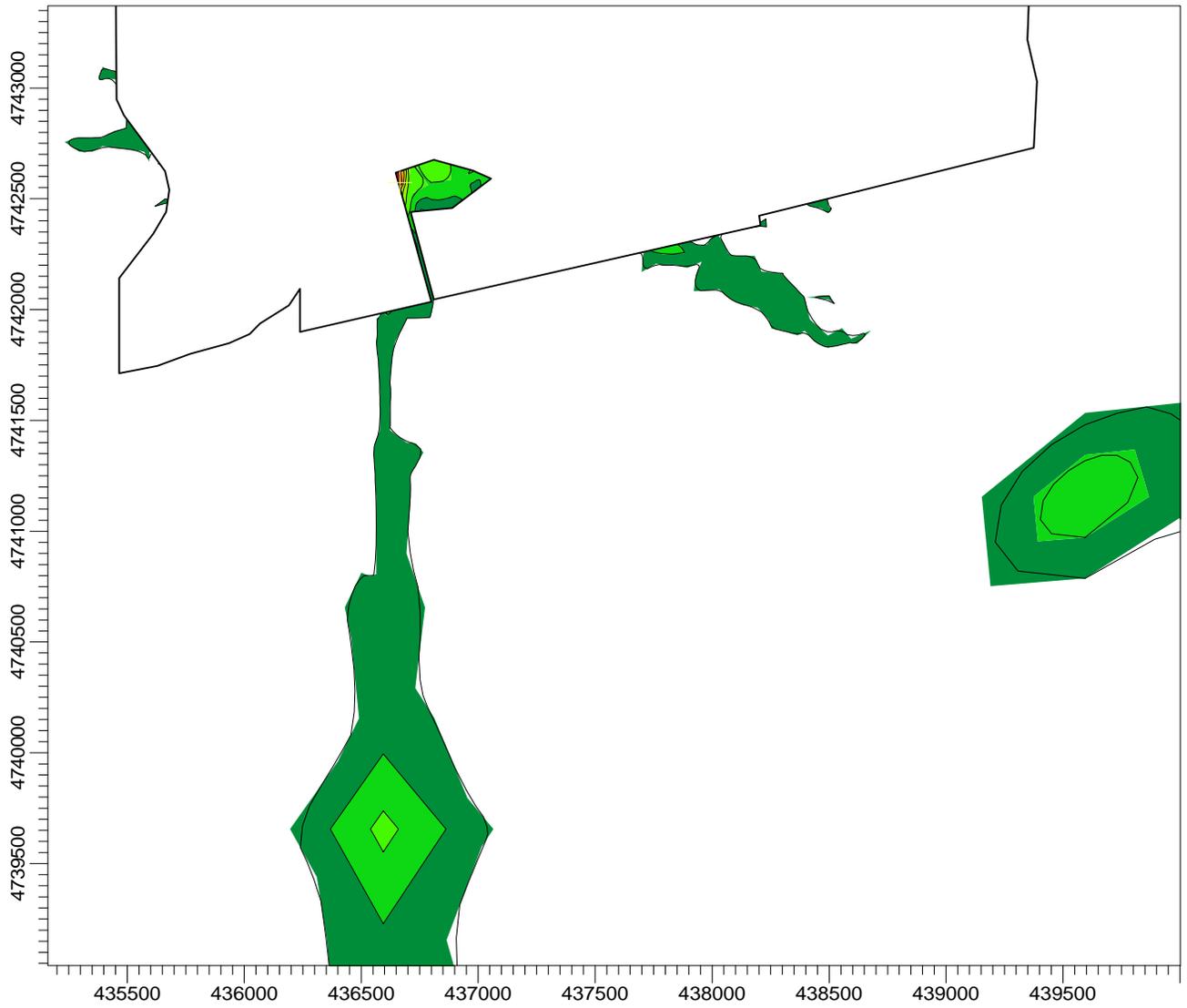
+ Highest 30-day Average Concentration = 0.075 $\mu\text{g}/\text{m}^3$

FIGURE 5-10.

2000 FLOURIDE IMPACTS—DJ WAAQS ANALYSIS
CONCENTRATION ISOPLETH - 30-DAY AVERAGE

Source: ECT, 2006.

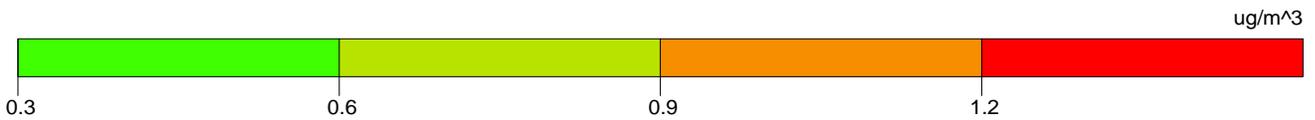
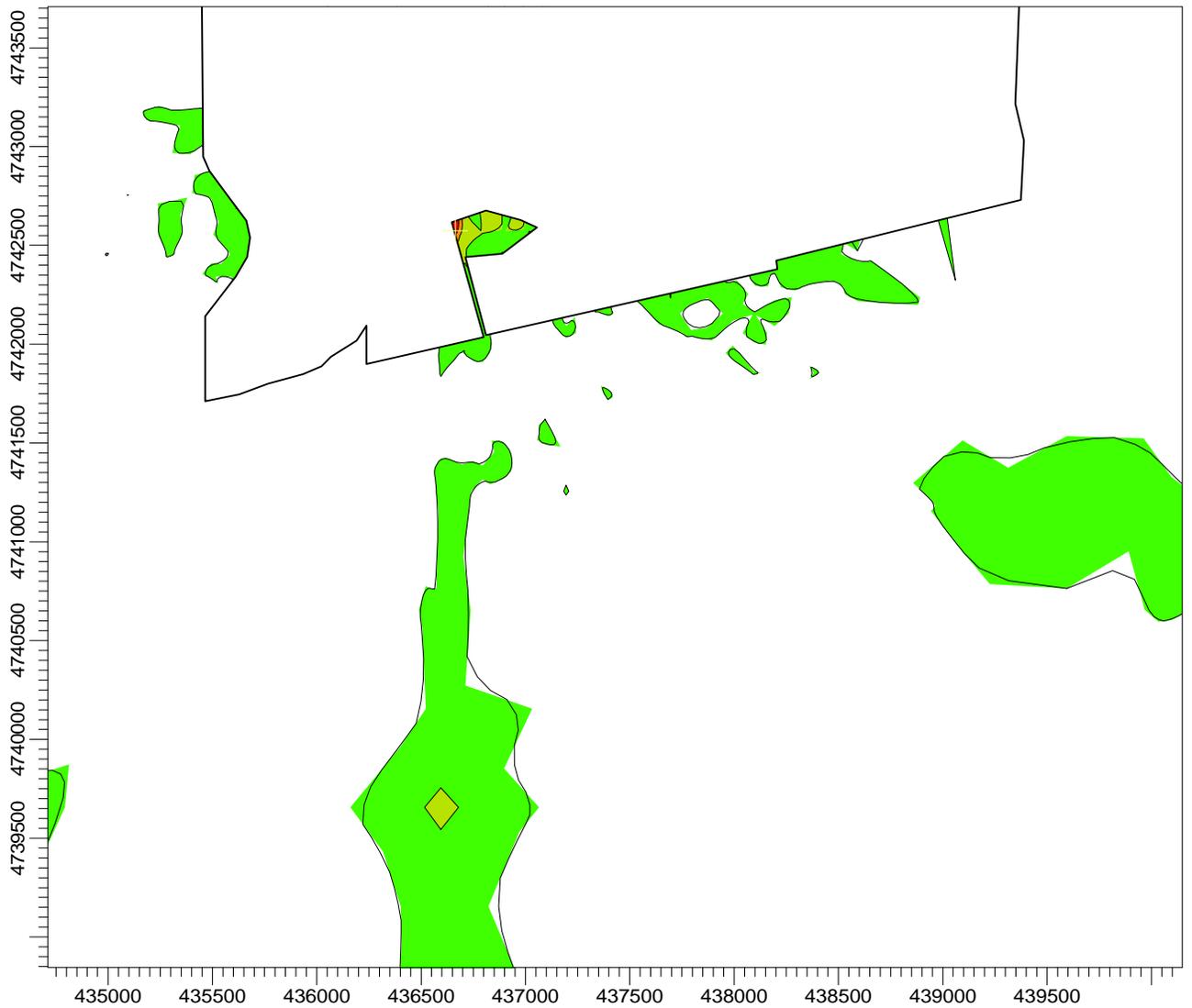




+ Highest 24-hr Average Concentration = 1.01 $\mu\text{g}/\text{m}^3$

FIGURE 5-11.
2001 FLOURIDE IMPACTS—DJ WAAQS ANALYSIS
CONCENTRATION ISOPLETH - 24-HR AVERAGE
Source: ECT, 2006.





+ Highest 12-hr Average Concentration = 1.50 $\mu\text{g}/\text{m}^3$

FIGURE 5-12.

2000 FLOURIDE IMPACTS—DJ WAAQS ANALYSIS
CONCENTRATION ISOPLETH - 12-HR AVERAGE

Source: ECT, 2006.



6.0 CONCLUSION

The proposed modifications will cause an increase in CO emission at the Dave Johnston Plant. As a result of this emission increase, the ambient air impacts for CO were determined. The modeling results show that the maximum impact will be below the PSD SIL. Therefore, it can be concluded that the proposed modifications will not cause or contribute to significant deterioration of the ambient air quality.

A WAAQS analysis was performed for NO₂, SO₂, CO, lead, and fluorides, including all significant facilities within 50 km of the Dave Johnston Plant. The modeling analysis showed that all ambient air impacts are currently below the WAAQS. Therefore, the proposed modifications will not cause any exceedances of the WAAQS.

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ATTACHMENT A
MODELING FILES

ELECTRONIC FILES FOR DISPERSION MODELING
DAVE JOHNSTON WAAQS ANALYSIS

Air quality analysis electronic files are provided within the following subdirectories on the enclosed CD:

1. Original Meteorological Data Files From 1998 through 2002 (7 Files): **\RAW_MET**

CAS98-02.DAT	Surface data from NCDC for Casper Natrona Airport
MIX98-02.TXT	Mixing height data from NCDC for Casper\Riverton
ONSITE _{xx} .DAT	Onsite surface data from Dave Johnston; xx = 98 – 02

2. Processed Meteorological Data Files From 1998, 2000 - 2002 (4 Files): **\PROC_MET**

DJ_ _{xx} .MET	Processed met. data; xx = 98, 00 – 02
------------------------	---------------------------------------

3. BPIP Files (3 Files): **\BPIP**

DJ_PM.SUP	BPIP-PRIME summary output file for all sources
DJ_PM.BPI	BPIP-PRIME input file for all sources
DJ_PM.PRO	BPIP-PRIME output file for all sources

4. DJ Maximum CO Impacts (10 Files): **\PSD**

_{xx} COPSD.PIN	ISC-PRIME input files; xx = 98, 00 – 02
_{xx} COPSD.POU	ISC-PRIME output files; xx = 98, 00 – 02
00COPSDM.PIN	ISC-PRIME input files; max. impact, year 2000
00COPSDM.POU	ISC-PRIME output files; max. impact, year 2000

5. WAAQS Analysis (40 Files): **\WAAQS**

_{xx} NOXNQ.PIN	ISC-PRIME input files for NO _x ; xx = 98, 00 – 02
_{xx} NOXNQ.POU	ISC-PRIME output files for NO _x ; xx = 98, 00 – 02
_{xx} SO2NQ.PIN	ISC-PRIME input files for SO ₂ ; xx = 98, 00 – 02
_{xx} SO2NQ.POU	ISC-PRIME output files for SO ₂ ; xx = 98, 00 – 02
_{xx} PMNQ.PIN	ISC-PRIME input files for PM ₁₀ ; xx = 98, 00 – 02
_{xx} PMNQ.POU	ISC-PRIME output files for PM ₁₀ ; xx = 98, 00 – 02
_{xx} PBNQ.PIN	ISC-PRIME input files for lead; xx = 98, 00 – 02
_{xx} PBNQ.POU	ISC-PRIME output files for lead; xx = 98, 00 – 02
_{xx} HFNQ.PIN	ISC-PRIME input files for HF; xx = 98, 00 – 02
_{xx} HFNQ.POU	ISC-PRIME output files for HF; xx = 98, 00 – 02

xxyyNQM.PIN

ISC-PRIME max. impact input files; xx = 00 and 01
yy = SO2, PM, PB, and HF

xxyyNQM.POU

ISC-PRIME max. impact output files; xx = 98 and 01
yy = SO2, PM, PB, and HF

6. Plot Files from the PSD and WAAQS Analyses (60 Files): **\PLOT**

xxxxxxxx.PLT

Plot files showing first and second highest impacts for
all pollutants.

ATTACHMENT B
FILLED METEOROLOGICAL DATA

Table B-1. Filled Cloud Cover and Ceiling Height Data
from Casper Natrona Airport

<u>Year</u>	<u>Month</u>	<u>Day</u>	<u>Hour</u>	<u>Substituted Parameter</u>
1998	1	1	4	CEILING HT
1998	1	1	4	SKY COVER
1998	1	1	7	CEILING HT
1998	1	1	7	SKY COVER
1998	1	1	21	CEILING HT
1998	1	1	21	SKY COVER
1998	1	3	18	CEILING HT
1998	1	3	18	SKY COVER
1998	1	4	2	CEILING HT
1998	1	4	2	SKY COVER
1998	1	4	6	CEILING HT
1998	1	4	6	SKY COVER
1998	1	4	21	CEILING HT
1998	1	4	21	SKY COVER
1998	1	5	1	CEILING HT
1998	1	5	1	SKY COVER
1998	1	6	3	CEILING HT
1998	1	6	3	SKY COVER
1998	1	6	15	CEILING HT
1998	1	6	15	SKY COVER
1998	1	7	23	CEILING HT
1998	1	7	23	SKY COVER
1998	1	8	12	CEILING HT
1998	1	8	12	SKY COVER
1998	1	8	23	CEILING HT
1998	1	8	23	SKY COVER
1998	1	8	24	SKY COVER
1998	1	10	4	CEILING HT
1998	1	10	4	SKY COVER
1998	1	10	18	SKY COVER
1998	1	10	22	CEILING HT
1998	1	10	22	SKY COVER
1998	1	11	11	CEILING HT
1998	1	11	11	SKY COVER
1998	1	11	14	CEILING HT
1998	1	11	14	SKY COVER
1998	1	12	11	CEILING HT
1998	1	12	11	SKY COVER
1998	1	12	20	CEILING HT
1998	1	12	20	SKY COVER
1998	1	12	24	SKY COVER
1998	1	13	6	CEILING HT
1998	1	13	6	SKY COVER
1998	1	13	10	CEILING HT
1998	1	13	10	SKY COVER
1998	1	13	18	CEILING HT
1998	1	13	18	SKY COVER
1998	1	14	14	CEILING HT
1998	1	14	14	SKY COVER
1998	1	15	14	CEILING HT
1998	1	15	14	SKY COVER
1998	1	16	5	CEILING HT
1998	1	16	5	SKY COVER

1998	1	16	18	CEILING HT
1998	1	16	18	SKY COVER
1998	1	16	20	CEILING HT
1998	1	16	20	SKY COVER
1998	1	17	12	SKY COVER
1998	1	17	15	CEILING HT
1998	1	17	15	SKY COVER
1998	1	17	18	CEILING HT
1998	1	17	18	SKY COVER
1998	1	17	22	CEILING HT
1998	1	17	22	SKY COVER
1998	1	19	7	CEILING HT
1998	1	19	7	SKY COVER
1998	1	19	12	CEILING HT
1998	1	19	12	SKY COVER
1998	1	19	14	CEILING HT
1998	1	19	14	SKY COVER
1998	1	19	23	CEILING HT
1998	1	19	23	SKY COVER
1998	1	20	12	SKY COVER
1998	1	20	18	CEILING HT
1998	1	20	18	SKY COVER
1998	1	21	10	CEILING HT
1998	1	21	10	SKY COVER
1998	1	21	18	CEILING HT
1998	1	21	18	SKY COVER
1998	1	22	6	SKY COVER
1998	1	22	24	CEILING HT
1998	1	22	24	SKY COVER
1998	1	23	6	SKY COVER
1998	1	23	22	CEILING HT
1998	1	23	22	SKY COVER
1998	1	24	1	CEILING HT
1998	1	24	1	SKY COVER
1998	1	25	7	CEILING HT
1998	1	25	7	SKY COVER
1998	1	25	12	SKY COVER
1998	1	25	17	CEILING HT
1998	1	25	17	SKY COVER
1998	1	25	18	SKY COVER
1998	1	26	20	CEILING HT
1998	1	26	20	SKY COVER
1998	1	27	10	CEILING HT
1998	1	27	10	SKY COVER
1998	1	27	16	CEILING HT
1998	1	27	16	SKY COVER
1998	1	27	23	CEILING HT
1998	1	27	23	SKY COVER
1998	1	27	24	SKY COVER
1998	1	29	4	CEILING HT
1998	1	29	4	SKY COVER
1998	1	30	2	CEILING HT
1998	1	30	2	SKY COVER
1998	1	30	12	CEILING HT
1998	1	30	12	SKY COVER
1998	1	30	18	CEILING HT
1998	1	30	18	SKY COVER
1998	1	30	24	CEILING HT
1998	1	30	24	SKY COVER

1998	1	31	5	CEILING HT
1998	1	31	5	SKY COVER
1998	1	31	9	CEILING HT
1998	1	31	9	SKY COVER
1998	1	31	11	CEILING HT
1998	1	31	11	SKY COVER
1998	1	31	21	CEILING HT
1998	1	31	21	SKY COVER
1998	2	2	18	SKY COVER
1998	2	3	1	CEILING HT
1998	2	3	1	SKY COVER
1998	2	3	14	CEILING HT
1998	2	3	14	SKY COVER
1998	2	5	18	SKY COVER
1998	2	8	24	SKY COVER
1998	2	12	21	CEILING HT
1998	2	12	21	SKY COVER
1998	2	13	5	CEILING HT
1998	2	13	5	SKY COVER
1998	2	13	24	SKY COVER
1998	2	17	17	CEILING HT
1998	2	17	17	SKY COVER
1998	2	18	24	SKY COVER
1998	2	23	6	SKY COVER
1998	2	25	18	SKY COVER
1998	2	25	24	CEILING HT
1998	2	25	24	SKY COVER
1998	2	26	12	SKY COVER
1998	3	1	24	SKY COVER
1998	3	3	24	SKY COVER
1998	3	5	2	CEILING HT
1998	3	5	2	SKY COVER
1998	3	5	6	SKY COVER
1998	3	5	18	SKY COVER
1998	3	6	18	SKY COVER
1998	3	7	4	CEILING HT
1998	3	7	4	SKY COVER
1998	3	8	9	CEILING HT
1998	3	8	9	SKY COVER
1998	3	17	23	CEILING HT
1998	3	17	23	SKY COVER
1998	3	19	12	SKY COVER
1998	3	20	22	CEILING HT
1998	3	20	22	SKY COVER
1998	3	25	24	SKY COVER
1998	3	26	6	SKY COVER
1998	3	27	24	SKY COVER
1998	3	29	3	CEILING HT
1998	3	29	3	SKY COVER
1998	3	29	5	CEILING HT
1998	3	29	5	SKY COVER
1998	3	29	18	SKY COVER
1998	3	29	24	SKY COVER
1998	3	30	3	CEILING HT
1998	3	30	3	SKY COVER
1998	3	30	10	CEILING HT
1998	3	30	10	SKY COVER
1998	3	30	12	CEILING HT
1998	3	30	12	SKY COVER

1998	4	1	14	CEILING HT
1998	4	1	14	SKY COVER
1998	4	5	18	SKY COVER
1998	4	5	23	CEILING HT
1998	4	5	23	SKY COVER
1998	4	6	24	SKY COVER
1998	4	7	24	SKY COVER
1998	4	8	24	SKY COVER
1998	4	10	21	CEILING HT
1998	4	10	21	SKY COVER
1998	4	12	5	CEILING HT
1998	4	12	5	SKY COVER
1998	4	12	6	SKY COVER
1998	4	12	18	SKY COVER
1998	4	12	24	SKY COVER
1998	4	13	24	SKY COVER
1998	4	14	1	CEILING HT
1998	4	14	12	SKY COVER
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1998	4	17	6	SKY COVER
1998	4	18	6	SKY COVER
1998	4	18	18	SKY COVER
1998	4	19	6	SKY COVER
1998	4	19	16	CEILING HT
1998	4	19	16	SKY COVER
1998	4	20	18	SKY COVER
1998	4	21	15	CEILING HT
1998	4	21	15	SKY COVER
1998	4	23	19	CEILING HT
1998	4	23	19	SKY COVER
1998	4	23	21	CEILING HT
1998	4	23	21	SKY COVER
1998	4	25	10	CEILING HT
1998	4	25	10	SKY COVER
1998	4	27	24	SKY COVER
1998	4	30	22	CEILING HT
1998	4	30	22	SKY COVER
1998	5	1	16	CEILING HT
1998	5	1	16	SKY COVER
1998	5	2	1	CEILING HT
1998	5	2	1	SKY COVER
1998	5	4	21	CEILING HT
1998	5	4	21	SKY COVER
1998	5	5	6	SKY COVER
1998	5	5	19	CEILING HT
1998	5	5	19	SKY COVER
1998	5	6	12	SKY COVER
1998	5	7	12	SKY COVER
1998	5	8	18	SKY COVER
1998	5	10	17	CEILING HT
1998	5	10	17	SKY COVER
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1998	5	11	7	SKY COVER
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1998	5	11	23	SKY COVER
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1998	5	12	1	SKY COVER
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1998	5	19	22	SKY COVER
1998	5	19	24	SKY COVER
1998	5	21	4	CEILING HT
1998	5	21	4	SKY COVER
1998	5	22	19	CEILING HT
1998	5	22	19	SKY COVER
1998	5	23	17	CEILING HT
1998	5	23	17	SKY COVER
1998	5	23	22	CEILING HT
1998	5	23	22	SKY COVER
1998	5	23	24	CEILING HT
1998	5	24	5	CEILING HT
1998	5	24	5	SKY COVER
1998	5	24	18	SKY COVER
1998	5	24	24	SKY COVER
1998	5	25	19	CEILING HT
1998	5	25	19	SKY COVER
1998	5	26	21	CEILING HT
1998	5	26	21	SKY COVER
1998	5	27	4	CEILING HT
1998	5	27	4	SKY COVER
1998	5	27	12	CEILING HT
1998	5	27	12	SKY COVER
1998	5	27	17	CEILING HT
1998	5	27	17	SKY COVER
1998	5	28	2	CEILING HT
1998	5	28	2	SKY COVER
1998	5	28	15	CEILING HT
1998	5	28	15	SKY COVER
1998	5	28	23	CEILING HT
1998	5	28	23	SKY COVER
1998	5	30	7	CEILING HT
1998	5	30	7	SKY COVER
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1998	5	30	16	SKY COVER
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1998	6	1	12	SKY COVER
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1998	6	4	24	SKY COVER
1998	6	5	6	SKY COVER
1998	6	5	18	SKY COVER
1998	6	7	18	SKY COVER
1998	6	9	18	SKY COVER
1998	6	10	16	CEILING HT
1998	6	10	16	SKY COVER
1998	6	11	12	SKY COVER
1998	6	12	13	CEILING HT
1998	6	12	13	SKY COVER
1998	6	13	9	CEILING HT
1998	6	13	9	SKY COVER
1998	6	14	6	SKY COVER
1998	6	14	18	SKY COVER
1998	6	14	24	SKY COVER
1998	6	15	18	SKY COVER
1998	6	15	24	SKY COVER
1998	6	20	1	CEILING HT
1998	6	20	1	SKY COVER
1998	6	23	5	CEILING HT

1998	6	23	5	SKY COVER
1998	6	23	10	CEILING HT
1998	6	23	10	SKY COVER
1998	6	23	16	CEILING HT
1998	6	23	16	SKY COVER
1998	6	24	21	CEILING HT
1998	6	24	21	SKY COVER
1998	6	26	15	CEILING HT
1998	6	26	15	SKY COVER
1998	6	28	7	CEILING HT
1998	6	28	7	SKY COVER
1998	6	28	17	CEILING HT
1998	6	28	17	SKY COVER
1998	6	28	20	CEILING HT
1998	6	28	20	SKY COVER
1998	6	29	4	CEILING HT
1998	6	29	4	SKY COVER
1998	6	30	22	CEILING HT
1998	6	30	22	SKY COVER
1998	7	3	6	CEILING HT
1998	7	4	4	CEILING HT
1998	7	4	4	SKY COVER
1998	7	6	12	SKY COVER
1998	7	6	23	CEILING HT
1998	7	6	23	SKY COVER
1998	7	8	5	CEILING HT
1998	7	8	5	SKY COVER
1998	7	12	20	CEILING HT
1998	7	12	20	SKY COVER
1998	7	13	7	CEILING HT
1998	7	13	7	SKY COVER
1998	7	13	17	CEILING HT
1998	7	13	17	SKY COVER
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1998	7	13	22	SKY COVER
1998	7	14	21	CEILING HT
1998	7	14	21	SKY COVER
1998	7	15	23	CEILING HT
1998	7	15	23	SKY COVER
1998	7	16	19	CEILING HT
1998	7	16	19	SKY COVER
1998	7	17	2	CEILING HT
1998	7	17	2	SKY COVER
1998	7	18	23	CEILING HT
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1998	7	19	4	SKY COVER
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1998	7	19	11	SKY COVER
1998	7	22	17	CEILING HT
1998	7	22	17	SKY COVER
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1998	7	23	23	SKY COVER
1998	7	24	24	SKY COVER
1998	7	25	18	SKY COVER
1998	7	28	12	SKY COVER
1998	7	28	23	CEILING HT

1998	7	28	23	SKY COVER
1998	7	30	20	CEILING HT
1998	7	30	20	SKY COVER
1998	8	1	20	CEILING HT
1998	8	1	20	SKY COVER
1998	8	1	23	CEILING HT
1998	8	1	23	SKY COVER
1998	8	2	2	CEILING HT
1998	8	2	2	SKY COVER
1998	8	2	5	CEILING HT
1998	8	2	5	SKY COVER
1998	8	3	6	SKY COVER
1998	8	3	18	SKY COVER
1998	8	4	12	CEILING HT
1998	8	4	12	SKY COVER
1998	8	7	2	CEILING HT
1998	8	7	2	SKY COVER
1998	8	12	15	CEILING HT
1998	8	12	15	SKY COVER
1998	8	13	20	CEILING HT
1998	8	13	20	SKY COVER
1998	8	14	17	CEILING HT
1998	8	14	17	SKY COVER
1998	8	14	19	CEILING HT
1998	8	14	19	SKY COVER
1998	8	14	23	CEILING HT
1998	8	14	23	SKY COVER
1998	8	15	21	CEILING HT
1998	8	15	21	SKY COVER
1998	8	16	18	CEILING HT
1998	8	16	18	SKY COVER
1998	8	18	1	CEILING HT
1998	8	18	1	SKY COVER
1998	8	18	14	CEILING HT
1998	8	18	14	SKY COVER
1998	8	19	14	CEILING HT
1998	8	19	14	SKY COVER
1998	8	21	1	CEILING HT
1998	8	21	1	SKY COVER
1998	8	21	20	CEILING HT
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1998	8	22	18	SKY COVER
1998	8	22	23	CEILING HT
1998	8	22	23	SKY COVER
1998	8	26	16	CEILING HT
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1998	8	26	20	CEILING HT
1998	8	26	20	SKY COVER
1998	8	26	24	SKY COVER
1998	8	27	18	SKY COVER
1998	8	28	21	CEILING HT
1998	8	28	21	SKY COVER
1998	8	29	23	CEILING HT
1998	8	29	23	SKY COVER
1998	8	30	23	CEILING HT
1998	8	30	23	SKY COVER
1998	8	31	13	CEILING HT
1998	8	31	13	SKY COVER

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1998	9	12	12	SKY COVER
1998	9	13	6	SKY COVER
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1998	10	14	19	SKY COVER
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1998	10	30	6	SKY COVER
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1998	10	30	9	SKY COVER

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1998	11	1	17	SKY COVER
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1998	11	2	10	SKY COVER
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1998	11	17	21	CEILING HT
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1998	11	18	18	SKY COVER
1998	11	19	12	SKY COVER
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1998	11	22	24	SKY COVER
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1998	12	25	1	SKY COVER
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1998	12	25	7	SKY COVER
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2000	1	4	20	CEILING HT
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2000	1	7	10	SKY COVER
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2000	1	10	19	SKY COVER
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2000	1	13	24	SKY COVER
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2000	1	14	6	SKY COVER
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2000	1	14	24	SKY COVER
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2000	1	15	6	SKY COVER
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2000	1	16	12	SKY COVER
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2000	1	16	17	SKY COVER
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2000	1	17	6	SKY COVER
2000	1	17	18	CEILING HT
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2000	1	17	24	SKY COVER
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2000	1	18	6	SKY COVER
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2000	1	18	12	SKY COVER
2000	1	18	18	CEILING HT
2000	1	18	18	SKY COVER
2000	1	18	24	CEILING HT
2000	1	18	24	SKY COVER
2000	1	19	6	CEILING HT
2000	1	19	6	SKY COVER
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2000	1	19	14	SKY COVER
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2000	1	23	18	CEILING HT
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2000	1	27	24	SKY COVER
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2000	1	28	12	SKY COVER
2000	1	29	9	CEILING HT
2000	1	29	9	SKY COVER
2000	1	30	10	CEILING HT
2000	1	30	10	SKY COVER
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2000	2	4	6	CEILING HT
2000	2	4	12	CEILING HT
2000	2	9	21	CEILING HT
2000	2	9	21	SKY COVER
2000	2	9	22	SKY COVER
2000	2	9	24	CEILING HT
2000	2	9	24	SKY COVER

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2000	2	11	12	CEILING HT
2000	2	12	12	CEILING HT
2000	2	12	18	CEILING HT
2000	2	12	24	CEILING HT
2000	2	12	24	SKY COVER
2000	2	13	5	CEILING HT
2000	2	13	5	SKY COVER
2000	2	13	12	CEILING HT
2000	2	14	11	CEILING HT
2000	2	14	11	SKY COVER
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2000	2	17	6	CEILING HT
2000	2	17	12	CEILING HT
2000	2	17	14	CEILING HT
2000	2	17	14	SKY COVER
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2000	2	18	6	CEILING HT
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2000	2	21	11	SKY COVER
2000	2	21	13	CEILING HT
2000	2	21	13	SKY COVER
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2000	2	23	20	SKY COVER
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2000	2	25	18	CEILING HT
2000	2	26	6	CEILING HT
2000	2	26	16	CEILING HT
2000	2	26	16	SKY COVER
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2000	2	28	23	SKY COVER
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2000	2	29	6	SKY COVER
2000	2	29	11	CEILING HT
2000	2	29	11	SKY COVER
2000	2	29	18	CEILING HT
2000	2	29	18	SKY COVER
2000	2	29	24	CEILING HT
2000	2	29	24	SKY COVER
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2000	3	1	6	SKY COVER
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2000	3	1	24	CEILING HT
2000	3	6	3	CEILING HT
2000	3	6	3	SKY COVER
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2000	3	6	23	CEILING HT
2000	3	6	23	SKY COVER
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2000	3	8	6	CEILING HT
2000	3	8	18	CEILING HT
2000	3	8	24	CEILING HT

2000	3	9	6	CEILING HT
2000	3	9	12	CEILING HT
2000	3	9	18	CEILING HT
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2000	3	10	12	CEILING HT
2000	3	10	24	CEILING HT
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2000	3	14	24	CEILING HT
2000	3	15	6	CEILING HT
2000	3	15	12	CEILING HT
2000	3	15	19	CEILING HT
2000	3	15	19	SKY COVER
2000	3	17	12	CEILING HT
2000	3	18	6	CEILING HT
2000	3	18	7	SKY COVER
2000	3	18	12	CEILING HT
2000	3	18	23	CEILING HT
2000	3	18	23	SKY COVER
2000	3	19	24	CEILING HT
2000	3	20	6	CEILING HT
2000	3	20	6	SKY COVER
2000	3	20	10	SKY COVER
2000	3	20	12	CEILING HT
2000	3	20	13	SKY COVER
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2000	3	21	12	CEILING HT
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2000	3	24	12	CEILING HT
2000	3	24	18	CEILING HT
2000	3	26	12	CEILING HT
2000	3	26	18	CEILING HT
2000	3	27	19	CEILING HT
2000	3	27	19	SKY COVER
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2000	3	28	21	SKY COVER
2000	3	29	6	CEILING HT
2000	3	29	12	CEILING HT
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2000	3	29	20	SKY COVER
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2000	3	30	14	CEILING HT
2000	3	30	14	SKY COVER
2000	3	30	18	CEILING HT
2000	3	30	24	CEILING HT
2000	3	31	18	CEILING HT
2000	4	1	6	CEILING HT
2000	4	1	8	CEILING HT
2000	4	1	8	SKY COVER
2000	4	1	22	CEILING HT
2000	4	1	22	SKY COVER
2000	4	2	6	CEILING HT

2000	4	2	12	CEILING HT
2000	4	2	18	CEILING HT
2000	4	2	24	SKY COVER
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2000	4	10	12	CEILING HT
2000	4	10	13	SKY COVER
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2000	4	12	21	CEILING HT
2000	4	12	21	SKY COVER
2000	4	14	6	CEILING HT
2000	4	14	12	CEILING HT
2000	4	14	12	SKY COVER
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2000	4	15	6	CEILING HT
2000	4	15	12	CEILING HT
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2000	4	15	24	SKY COVER
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2000	4	18	24	CEILING HT
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2000	4	19	5	SKY COVER
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2000	4	19	18	CEILING HT
2000	4	19	24	CEILING HT
2000	4	20	6	CEILING HT
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2000	4	20	24	SKY COVER
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2000	4	22	10	CEILING HT
2000	4	22	10	SKY COVER
2000	4	22	12	CEILING HT
2000	4	22	12	SKY COVER
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2000	4	23	11	CEILING HT
2000	4	23	11	SKY COVER
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2000	4	24	12	SKY COVER
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2000	4	25	19	SKY COVER
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2000	4	26	10	SKY COVER
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2000	4	29	7	SKY COVER
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2000	4	29	18	CEILING HT
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2000	5	3	16	SKY COVER
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2000	5	3	24	SKY COVER
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2000	5	17	3	SKY COVER
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2000	5	21	14	CEILING HT
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2000	5	28	5	SKY COVER
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2000	5	28	22	SKY COVER
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2000	5	31	2	SKY COVER
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2000	6	3	17	SKY COVER
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2000	6	5	18	SKY COVER
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2000	6	6	1	SKY COVER
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2000	6	12	7	SKY COVER
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2000	6	20	2	SKY COVER
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2000	6	23	1	CEILING HT

2000	6	23	1	SKY COVER
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2000	6	27	24	CEILING HT
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2000	7	8	2	SKY COVER
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2000	7	16	12	CEILING HT
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2000	7	18	1	SKY COVER
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2000	7	22	17	SKY COVER
2000	7	23	11	SKY COVER
2000	7	24	2	CEILING HT
2000	7	24	2	SKY COVER
2000	7	25	20	SKY COVER
2000	7	27	21	CEILING HT
2000	7	27	21	SKY COVER
2000	7	28	15	SKY COVER
2000	7	28	23	CEILING HT
2000	7	28	23	SKY COVER
2000	8	8	4	CEILING HT
2000	8	8	4	SKY COVER
2000	8	8	15	CEILING HT
2000	8	8	15	SKY COVER
2000	8	10	8	CEILING HT
2000	8	10	8	SKY COVER
2000	8	10	13	CEILING HT
2000	8	10	13	SKY COVER
2000	8	10	18	CEILING HT
2000	8	10	18	SKY COVER
2000	8	10	21	SKY COVER
2000	8	10	22	SKY COVER
2000	8	11	3	CEILING HT
2000	8	11	3	SKY COVER
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2000	8	11	9	SKY COVER
2000	8	12	1	CEILING HT
2000	8	12	1	SKY COVER
2000	8	12	15	CEILING HT
2000	8	12	15	SKY COVER

2000	8	13	1	CEILING HT
2000	8	13	1	SKY COVER
2000	8	13	16	CEILING HT
2000	8	13	16	SKY COVER
2000	8	14	11	CEILING HT
2000	8	14	11	SKY COVER
2000	8	15	2	CEILING HT
2000	8	15	2	SKY COVER
2000	8	15	23	CEILING HT
2000	8	15	23	SKY COVER
2000	8	16	9	CEILING HT
2000	8	16	9	SKY COVER
2000	8	16	23	CEILING HT
2000	8	16	23	SKY COVER
2000	8	17	11	CEILING HT
2000	8	17	11	SKY COVER
2000	8	18	11	CEILING HT
2000	8	18	11	SKY COVER
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2000	8	31	6	CEILING HT
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2000	8	31	11	SKY COVER
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2000	9	8	16	CEILING HT
2000	9	8	16	SKY COVER
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2000	9	15	15	SKY COVER
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2000	9	23	6	CEILING HT
2000	9	23	6	SKY COVER
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2000	9	24	12	CEILING HT
2000	9	26	22	CEILING HT
2000	9	26	22	SKY COVER
2000	9	28	24	CEILING HT
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2000	10	8	22	CEILING HT
2000	10	8	22	SKY COVER
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2000	10	13	3	SKY COVER
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2000	10	15	19	SKY COVER
2000	10	17	17	CEILING HT
2000	10	17	17	SKY COVER
2000	10	19	3	SKY COVER
2000	10	19	17	SKY COVER
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2000	10	22	24	CEILING HT
2000	10	23	6	CEILING HT
2000	10	23	12	CEILING HT
2000	10	24	18	CEILING HT
2000	10	25	12	CEILING HT
2000	10	25	18	CEILING HT
2000	10	26	4	SKY COVER
2000	10	26	6	CEILING HT
2000	10	26	12	CEILING HT
2000	10	31	6	CEILING HT
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2000	11	7	15	CEILING HT
2000	11	7	15	SKY COVER
2000	11	7	18	CEILING HT
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2000	11	7	21	SKY COVER
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2000	11	8	3	SKY COVER
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2000	11	9	6	SKY COVER
2000	11	9	12	CEILING HT
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2000	11	9	24	CEILING HT

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2000	11	10	12	CEILING HT
2000	11	10	18	CEILING HT
2000	11	10	24	CEILING HT
2000	11	11	6	CEILING HT
2000	11	11	10	CEILING HT
2000	11	11	10	SKY COVER
2000	11	12	11	SKY COVER
2000	11	13	16	CEILING HT
2000	11	13	16	SKY COVER
2000	11	15	7	CEILING HT
2000	11	15	7	SKY COVER
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2000	11	16	12	CEILING HT
2000	11	17	12	CEILING HT
2000	11	17	18	CEILING HT
2000	11	17	18	SKY COVER
2000	11	18	18	CEILING HT
2000	11	18	19	SKY COVER
2000	11	19	6	CEILING HT
2000	11	19	24	CEILING HT
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2000	11	24	1	SKY COVER
2000	11	25	6	CEILING HT
2000	11	25	14	CEILING HT
2000	11	25	14	SKY COVER
2000	11	26	18	CEILING HT
2000	11	26	18	SKY COVER
2000	11	28	6	CEILING HT
2000	11	28	12	CEILING HT
2000	11	28	18	CEILING HT
2000	11	30	16	CEILING HT
2000	11	30	16	SKY COVER
2000	11	30	18	CEILING HT
2000	11	30	24	CEILING HT
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2000	12	4	12	CEILING HT
2000	12	5	6	CEILING HT
2000	12	5	18	CEILING HT
2000	12	5	18	SKY COVER
2000	12	5	20	SKY COVER
2000	12	5	24	CEILING HT
2000	12	6	22	CEILING HT
2000	12	6	22	SKY COVER
2000	12	7	18	CEILING HT
2000	12	7	24	CEILING HT
2000	12	8	6	CEILING HT
2000	12	8	12	CEILING HT
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2000	12	11	6	CEILING HT
2000	12	11	12	CEILING HT
2000	12	12	6	SKY COVER
2000	12	15	24	CEILING HT
2000	12	16	6	CEILING HT

2000	12	16	12	CEILING HT
2000	12	16	24	CEILING HT
2000	12	18	12	CEILING HT
2000	12	20	6	CEILING HT
2000	12	20	12	CEILING HT
2000	12	22	6	CEILING HT
2000	12	22	12	CEILING HT
2000	12	22	24	CEILING HT
2000	12	23	18	CEILING HT
2000	12	24	18	CEILING HT
2000	12	25	6	CEILING HT
2000	12	25	12	CEILING HT
2000	12	25	18	CEILING HT
2000	12	25	21	CEILING HT
2000	12	25	21	SKY COVER
2000	12	28	12	CEILING HT
2000	12	28	18	CEILING HT
2000	12	29	6	CEILING HT
2000	12	29	24	CEILING HT
2000	12	30	6	CEILING HT
2000	12	30	12	CEILING HT
2000	12	30	18	CEILING HT
2000	12	30	24	CEILING HT
2000	12	31	4	CEILING HT
2000	12	31	4	SKY COVER
2000	12	31	6	CEILING HT
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2001	1	1	24	CEILING HT
2001	1	5	5	CEILING HT
2001	1	5	5	SKY COVER
2001	1	6	22	CEILING HT
2001	1	6	22	SKY COVER
2001	1	7	2	SKY COVER
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2001	1	13	18	CEILING HT
2001	1	13	24	CEILING HT
2001	1	14	6	CEILING HT
2001	1	14	18	CEILING HT
2001	1	15	12	CEILING HT
2001	1	15	18	CEILING HT
2001	1	15	21	SKY COVER
2001	1	16	6	CEILING HT
2001	1	16	12	CEILING HT
2001	1	16	18	CEILING HT
2001	1	17	24	CEILING HT
2001	1	18	6	CEILING HT
2001	1	18	12	CEILING HT
2001	1	18	18	CEILING HT
2001	1	19	6	CEILING HT
2001	1	20	9	CEILING HT
2001	1	20	9	SKY COVER
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2001	1	20	24	CEILING HT
2001	1	23	18	CEILING HT
2001	1	25	24	CEILING HT
2001	1	26	6	CEILING HT
2001	1	26	12	CEILING HT

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2001	1	28	12	CEILING HT
2001	1	28	18	CEILING HT
2001	1	28	24	CEILING HT
2001	1	29	6	CEILING HT
2001	1	29	11	CEILING HT
2001	1	29	11	SKY COVER
2001	1	29	23	CEILING HT
2001	1	29	23	SKY COVER
2001	1	31	12	CEILING HT
2001	2	1	6	CEILING HT
2001	2	1	12	CEILING HT
2001	2	1	16	CEILING HT
2001	2	1	16	SKY COVER
2001	2	1	18	CEILING HT
2001	2	2	24	CEILING HT
2001	2	3	6	CEILING HT
2001	2	5	18	CEILING HT
2001	2	5	24	CEILING HT
2001	2	6	6	CEILING HT
2001	2	6	24	CEILING HT
2001	2	7	6	CEILING HT
2001	2	7	12	CEILING HT
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2001	2	13	18	CEILING HT
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2001	2	14	6	CEILING HT
2001	2	14	12	CEILING HT
2001	2	16	6	CEILING HT
2001	2	16	12	CEILING HT
2001	2	17	5	CEILING HT
2001	2	17	5	SKY COVER
2001	2	20	18	CEILING HT
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2001	2	23	12	CEILING HT
2001	2	23	18	CEILING HT
2001	2	23	24	CEILING HT
2001	2	24	6	CEILING HT
2001	2	24	12	CEILING HT
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2001	2	25	6	CEILING HT
2001	2	26	12	CEILING HT
2001	2	26	18	CEILING HT
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2001	2	27	12	CEILING HT
2001	2	27	18	CEILING HT
2001	2	27	24	CEILING HT
2001	3	6	6	CEILING HT
2001	3	6	12	CEILING HT
2001	3	6	22	CEILING HT
2001	3	6	22	SKY COVER
2001	3	8	17	CEILING HT
2001	3	8	17	SKY COVER

2001	3	10	6	CEILING HT
2001	3	10	12	CEILING HT
2001	3	10	18	CEILING HT
2001	3	10	24	CEILING HT
2001	3	11	12	CEILING HT
2001	3	11	18	CEILING HT
2001	3	11	24	CEILING HT
2001	3	12	6	CEILING HT
2001	3	12	12	CEILING HT
2001	3	12	18	CEILING HT
2001	3	12	19	SKY COVER
2001	3	12	21	SKY COVER
2001	3	14	7	CEILING HT
2001	3	14	7	SKY COVER
2001	3	14	18	CEILING HT
2001	3	15	6	CEILING HT
2001	3	15	12	CEILING HT
2001	3	18	12	CEILING HT
2001	3	20	12	CEILING HT
2001	3	20	24	CEILING HT
2001	3	21	24	CEILING HT
2001	3	24	4	CEILING HT
2001	3	24	4	SKY COVER
2001	3	24	6	CEILING HT
2001	3	24	12	CEILING HT
2001	3	24	18	CEILING HT
2001	3	24	24	CEILING HT
2001	3	25	6	CEILING HT
2001	3	25	12	CEILING HT
2001	3	25	18	CEILING HT
2001	3	25	24	CEILING HT
2001	3	26	6	CEILING HT
2001	3	26	12	CEILING HT
2001	3	26	18	CEILING HT
2001	3	26	24	CEILING HT
2001	3	27	6	CEILING HT
2001	3	27	12	CEILING HT
2001	3	27	18	CEILING HT
2001	3	28	24	CEILING HT
2001	3	29	6	CEILING HT
2001	3	29	12	CEILING HT
2001	3	29	18	CEILING HT
2001	3	29	19	SKY COVER
2001	3	30	18	CEILING HT
2001	3	30	24	CEILING HT
2001	3	31	6	CEILING HT
2001	3	31	12	CEILING HT
2001	3	31	17	CEILING HT
2001	3	31	17	SKY COVER
2001	4	1	12	CEILING HT
2001	4	1	24	CEILING HT
2001	4	2	18	CEILING HT
2001	4	2	24	CEILING HT
2001	4	3	12	CEILING HT
2001	4	3	18	CEILING HT
2001	4	3	24	CEILING HT
2001	4	4	6	CEILING HT
2001	4	4	12	CEILING HT
2001	4	4	18	CEILING HT

2001	4	5	6	CEILING HT
2001	4	5	12	CEILING HT
2001	4	5	24	CEILING HT
2001	4	6	6	CEILING HT
2001	4	7	1	CEILING HT
2001	4	7	1	SKY COVER
2001	4	7	12	CEILING HT
2001	4	7	18	CEILING HT
2001	4	8	10	SKY COVER
2001	4	9	7	CEILING HT
2001	4	9	7	SKY COVER
2001	4	10	12	CEILING HT
2001	4	10	18	CEILING HT
2001	4	10	24	CEILING HT
2001	4	11	12	CEILING HT
2001	4	11	24	CEILING HT
2001	4	12	6	CEILING HT
2001	4	14	24	CEILING HT
2001	4	20	12	CEILING HT
2001	4	21	6	CEILING HT
2001	4	21	24	CEILING HT
2001	4	22	17	CEILING HT
2001	4	22	17	SKY COVER
2001	4	22	24	CEILING HT
2001	4	27	19	CEILING HT
2001	4	27	19	SKY COVER
2001	4	29	20	SKY COVER
2001	5	2	6	CEILING HT
2001	5	2	12	CEILING HT
2001	5	2	18	CEILING HT
2001	5	2	24	CEILING HT
2001	5	3	6	CEILING HT
2001	5	3	12	CEILING HT
2001	5	3	18	CEILING HT
2001	5	3	24	CEILING HT
2001	5	4	5	CEILING HT
2001	5	4	5	SKY COVER
2001	5	4	12	CEILING HT
2001	5	4	24	CEILING HT
2001	5	5	12	CEILING HT
2001	5	6	6	CEILING HT
2001	5	6	12	CEILING HT
2001	5	6	19	SKY COVER
2001	5	11	15	CEILING HT
2001	5	11	15	SKY COVER
2001	5	13	22	CEILING HT
2001	5	13	22	SKY COVER
2001	5	14	17	CEILING HT
2001	5	14	17	SKY COVER
2001	5	15	19	CEILING HT
2001	5	15	19	SKY COVER
2001	5	16	12	CEILING HT
2001	5	17	23	CEILING HT
2001	5	17	23	SKY COVER
2001	5	19	6	CEILING HT
2001	5	20	15	CEILING HT
2001	5	20	15	SKY COVER
2001	5	20	17	SKY COVER
2001	5	20	18	CEILING HT

2001	5	21	12	CEILING HT
2001	5	22	12	CEILING HT
2001	5	23	11	CEILING HT
2001	5	23	11	SKY COVER
2001	5	27	6	CEILING HT
2001	5	27	24	CEILING HT
2001	5	30	6	CEILING HT
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2001	6	2	3	SKY COVER
2001	6	3	6	CEILING HT
2001	6	3	12	CEILING HT
2001	6	4	6	CEILING HT
2001	6	4	18	CEILING HT
2001	6	4	24	CEILING HT
2001	6	7	19	CEILING HT
2001	6	7	19	SKY COVER
2001	6	8	15	CEILING HT
2001	6	8	15	SKY COVER
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2001	6	9	1	SKY COVER
2001	6	9	4	CEILING HT
2001	6	9	4	SKY COVER
2001	6	11	5	CEILING HT
2001	6	11	5	SKY COVER
2001	6	11	17	SKY COVER
2001	6	11	18	CEILING HT
2001	6	11	19	SKY COVER
2001	6	11	20	SKY COVER
2001	6	11	21	SKY COVER
2001	6	11	22	CEILING HT
2001	6	12	1	SKY COVER
2001	6	12	2	SKY COVER
2001	6	12	24	CEILING HT
2001	6	14	6	CEILING HT
2001	6	14	7	SKY COVER
2001	6	14	12	CEILING HT
2001	6	14	18	CEILING HT
2001	6	15	12	CEILING HT
2001	6	18	5	CEILING HT
2001	6	18	5	SKY COVER
2001	6	19	12	CEILING HT
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2001	6	21	19	CEILING HT
2001	6	21	19	SKY COVER
2001	6	22	3	CEILING HT
2001	6	22	3	SKY COVER
2001	6	23	1	CEILING HT
2001	6	23	1	SKY COVER
2001	6	23	22	CEILING HT
2001	6	23	22	SKY COVER
2001	6	26	5	CEILING HT
2001	6	26	5	SKY COVER
2001	6	27	3	CEILING HT
2001	6	27	3	SKY COVER
2001	6	27	6	CEILING HT
2001	6	27	11	CEILING HT
2001	6	27	11	SKY COVER
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2001	7	2	21	SKY COVER
2001	7	5	22	CEILING HT
2001	7	5	22	SKY COVER
2001	7	6	17	CEILING HT
2001	7	6	17	SKY COVER
2001	7	7	15	CEILING HT
2001	7	7	15	SKY COVER
2001	7	8	23	CEILING HT
2001	7	8	23	SKY COVER
2001	7	10	5	CEILING HT
2001	7	10	5	SKY COVER
2001	7	12	20	SKY COVER
2001	7	13	21	CEILING HT
2001	7	13	21	SKY COVER
2001	7	14	1	CEILING HT
2001	7	14	1	SKY COVER
2001	7	18	19	CEILING HT
2001	7	18	19	SKY COVER
2001	7	19	19	CEILING HT
2001	7	19	19	SKY COVER
2001	7	23	12	CEILING HT
2001	7	24	12	CEILING HT
2001	7	26	10	CEILING HT
2001	7	26	10	SKY COVER
2001	7	26	12	CEILING HT
2001	7	26	24	CEILING HT
2001	7	31	6	CEILING HT
2001	8	2	15	CEILING HT
2001	8	2	15	SKY COVER
2001	8	2	19	CEILING HT
2001	8	2	19	SKY COVER
2001	8	3	7	CEILING HT
2001	8	3	7	SKY COVER
2001	8	3	13	CEILING HT
2001	8	3	13	SKY COVER
2001	8	3	19	CEILING HT
2001	8	3	19	SKY COVER
2001	8	4	1	CEILING HT
2001	8	4	1	SKY COVER
2001	8	4	7	CEILING HT
2001	8	4	7	SKY COVER
2001	8	4	13	CEILING HT
2001	8	4	13	SKY COVER
2001	8	4	19	CEILING HT
2001	8	4	19	SKY COVER
2001	8	5	13	CEILING HT
2001	8	5	13	SKY COVER
2001	8	5	19	CEILING HT
2001	8	5	19	SKY COVER
2001	8	6	7	CEILING HT
2001	8	6	7	SKY COVER
2001	8	6	13	CEILING HT
2001	8	6	13	SKY COVER
2001	8	6	19	CEILING HT
2001	8	6	19	SKY COVER
2001	8	7	1	CEILING HT
2001	8	7	1	SKY COVER
2001	8	7	7	CEILING HT
2001	8	7	7	SKY COVER

2001	8	7	13	CEILING HT
2001	8	7	13	SKY COVER
2001	8	8	1	CEILING HT
2001	8	8	1	SKY COVER
2001	8	8	7	SKY COVER
2001	8	8	19	CEILING HT
2001	8	8	19	SKY COVER
2001	8	9	7	SKY COVER
2001	8	9	13	SKY COVER
2001	8	9	19	CEILING HT
2001	8	9	19	SKY COVER
2001	8	10	1	CEILING HT
2001	8	10	1	SKY COVER
2001	8	10	7	SKY COVER
2001	8	10	13	CEILING HT
2001	8	10	13	SKY COVER
2001	8	10	19	CEILING HT
2001	8	10	19	SKY COVER
2001	8	11	1	CEILING HT
2001	8	11	1	SKY COVER
2001	8	11	7	CEILING HT
2001	8	11	7	SKY COVER
2001	8	11	13	CEILING HT
2001	8	11	13	SKY COVER
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2001	12	4	1	SKY COVER
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2001	12	4	7	SKY COVER
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2001	12	4	13	SKY COVER
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2001	12	5	19	CEILING HT

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2001	12	6	1	SKY COVER
2001	12	6	7	CEILING HT
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2001	12	6	13	SKY COVER
2001	12	6	19	CEILING HT
2001	12	6	19	SKY COVER
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2001	12	13	1	SKY COVER
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2001	12	13	7	SKY COVER
2001	12	13	13	CEILING HT
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2001	12	13	19	SKY COVER
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2001	12	14	1	SKY COVER
2001	12	14	7	CEILING HT
2001	12	14	7	SKY COVER
2001	12	14	13	CEILING HT
2001	12	14	13	SKY COVER

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2001	12	14	19	SKY COVER
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2001	12	15	7	SKY COVER
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2001	12	17	7	SKY COVER
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2001	12	19	1	SKY COVER
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2001	12	19	7	SKY COVER
2001	12	19	13	CEILING HT
2001	12	19	13	SKY COVER
2001	12	19	19	CEILING HT
2001	12	19	19	SKY COVER
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2001	12	20	1	SKY COVER
2001	12	20	7	CEILING HT
2001	12	20	7	SKY COVER
2001	12	20	13	CEILING HT
2001	12	20	13	SKY COVER
2001	12	20	19	CEILING HT
2001	12	20	19	SKY COVER
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2001	12	21	1	SKY COVER
2001	12	21	7	CEILING HT
2001	12	21	7	SKY COVER
2001	12	21	13	CEILING HT
2001	12	21	13	SKY COVER
2001	12	21	15	CEILING HT
2001	12	21	15	SKY COVER
2001	12	21	19	CEILING HT
2001	12	21	19	SKY COVER

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2001	12	22	1	SKY COVER
2001	12	22	7	SKY COVER
2001	12	22	13	SKY COVER
2001	12	22	19	SKY COVER
2001	12	23	1	CEILING HT
2001	12	23	1	SKY COVER
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2001	12	23	19	CEILING HT
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2001	12	24	1	SKY COVER
2001	12	24	7	CEILING HT
2001	12	24	7	SKY COVER
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2001	12	24	13	SKY COVER
2001	12	24	19	CEILING HT
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2001	12	25	1	SKY COVER
2001	12	25	7	CEILING HT
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2001	12	27	1	CEILING HT
2001	12	27	1	SKY COVER
2001	12	27	7	CEILING HT
2001	12	27	7	SKY COVER
2001	12	27	13	CEILING HT
2001	12	27	13	SKY COVER
2001	12	27	19	CEILING HT
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2001	12	28	1	SKY COVER
2001	12	28	7	CEILING HT
2001	12	28	7	SKY COVER
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2001	12	28	13	SKY COVER
2001	12	28	19	CEILING HT
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2001	12	29	7	SKY COVER
2001	12	29	13	SKY COVER
2001	12	29	19	SKY COVER
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2001	12	30	19	CEILING HT
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2002	1	2	1	SKY COVER
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2002	1	3	13	SKY COVER
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2002	1	4	1	SKY COVER
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2002	1	4	7	SKY COVER
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2002	1	6	13	SKY COVER
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2002	1	7	1	SKY COVER
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2002	1	7	7	SKY COVER
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2002	1	7	13	SKY COVER
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2002	1	7	19	SKY COVER
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2002	1	8	1	SKY COVER

2002	1	8	7	CEILING HT
2002	1	8	7	SKY COVER
2002	1	8	13	CEILING HT
2002	1	8	13	SKY COVER
2002	1	8	19	CEILING HT
2002	1	8	19	SKY COVER
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2002	1	13	13	CEILING HT
2002	1	13	13	SKY COVER
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2002	1	16	13	SKY COVER

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2002	1	19	19	SKY COVER
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2002	1	22	7	SKY COVER
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2002	1	22	19	CEILING HT
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2002	1	23	1	CEILING HT
2002	1	23	1	SKY COVER
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2002	1	23	7	SKY COVER
2002	1	23	13	CEILING HT
2002	1	23	13	SKY COVER
2002	1	23	19	CEILING HT
2002	1	23	19	SKY COVER
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2002	1	24	1	SKY COVER
2002	1	24	7	CEILING HT
2002	1	24	7	SKY COVER
2002	1	24	13	CEILING HT
2002	1	24	13	SKY COVER

2002	1	24	19	CEILING HT
2002	1	24	19	SKY COVER
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2002	1	25	1	SKY COVER
2002	1	25	7	CEILING HT
2002	1	25	7	SKY COVER
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2002	1	25	13	SKY COVER
2002	1	25	19	CEILING HT
2002	1	25	19	SKY COVER
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2002	1	26	1	SKY COVER
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2002	2	25	7	SKY COVER
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2002	2	25	19	CEILING HT
2002	2	25	19	SKY COVER
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2002	2	26	13	SKY COVER
2002	2	26	19	CEILING HT
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2002	2	28	1	SKY COVER
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2002	3	3	7	CEILING HT
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2002	3	6	1	SKY COVER
2002	3	6	7	CEILING HT
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2002	3	12	7	SKY COVER
2002	3	12	13	CEILING HT
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2002	3	12	19	CEILING HT
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2002	3	13	1	SKY COVER
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2002	3	15	19	CEILING HT
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2002	3	23	1	SKY COVER
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2002	4	3	1	SKY COVER
2002	4	3	7	CEILING HT
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2002	4	3	13	SKY COVER
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2002	4	7	19	CEILING HT
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2002	4	9	1	SKY COVER
2002	4	9	7	CEILING HT
2002	4	9	7	SKY COVER
2002	4	9	19	CEILING HT
2002	4	9	19	SKY COVER
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2002	4	10	19	CEILING HT
2002	4	10	19	SKY COVER
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2002	4	12	7	CEILING HT
2002	4	12	7	SKY COVER
2002	4	12	13	CEILING HT
2002	4	12	13	SKY COVER
2002	4	12	19	CEILING HT
2002	4	12	19	SKY COVER
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2002	4	13	7	SKY COVER
2002	4	13	13	CEILING HT
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2002	4	14	1	SKY COVER
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2002	4	16	19	CEILING HT
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2002	4	18	7	SKY COVER
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2002	4	18	19	SKY COVER
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2002	4	19	19	SKY COVER
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2002	5	13	1	SKY COVER
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2002	5	13	7	SKY COVER
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2002	5	13	13	SKY COVER
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2002	5	14	1	SKY COVER
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2002	6	27	7	SKY COVER
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2002	7	2	13	CEILING HT
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2002	7	10	1	SKY COVER
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2002	8	8	19	SKY COVER
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2002	8	9	1	SKY COVER
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2002	8	9	7	SKY COVER
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2002	8	10	13	SKY COVER
2002	8	10	19	CEILING HT
2002	8	10	19	SKY COVER
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2002	8	11	13	SKY COVER
2002	8	11	19	CEILING HT
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2002	8	12	7	SKY COVER
2002	8	12	13	SKY COVER
2002	8	12	19	SKY COVER
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2002	8	13	7	SKY COVER
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2002	8	18	19	SKY COVER

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2002	8	23	7	SKY COVER
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2002	8	23	19	CEILING HT
2002	8	23	19	SKY COVER
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2002	8	24	1	SKY COVER
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2002	8	24	7	SKY COVER
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2002	8	24	19	CEILING HT
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2002	8	25	1	SKY COVER
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2002	8	27	1	SKY COVER
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2002	8	31	19	SKY COVER
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2002	9	20	7	SKY COVER
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2002	9	24	19	CEILING HT
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2002	9	26	19	CEILING HT
2002	9	26	19	SKY COVER
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2002	9	27	1	SKY COVER
2002	9	27	7	CEILING HT
2002	9	27	7	SKY COVER
2002	9	27	13	CEILING HT
2002	9	27	13	SKY COVER
2002	9	27	19	CEILING HT
2002	9	27	19	SKY COVER
2002	9	28	1	CEILING HT
2002	9	28	1	SKY COVER
2002	9	28	7	SKY COVER
2002	9	28	13	SKY COVER
2002	9	28	19	CEILING HT
2002	9	28	19	SKY COVER
2002	9	29	1	CEILING HT
2002	9	29	1	SKY COVER

2002	9	29	7	CEILING HT
2002	9	29	7	SKY COVER
2002	9	29	13	CEILING HT
2002	9	29	13	SKY COVER
2002	9	29	19	CEILING HT
2002	9	29	19	SKY COVER
2002	9	30	1	CEILING HT
2002	9	30	1	SKY COVER
2002	9	30	7	CEILING HT
2002	9	30	7	SKY COVER
2002	9	30	13	CEILING HT
2002	9	30	13	SKY COVER
2002	9	30	19	CEILING HT
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2002	10	1	7	SKY COVER
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2002	10	1	16	CEILING HT
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2002	10	2	7	SKY COVER
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2002	10	3	1	SKY COVER
2002	10	3	7	SKY COVER
2002	10	3	13	CEILING HT
2002	10	3	13	SKY COVER
2002	10	3	19	SKY COVER
2002	10	3	24	CEILING HT
2002	10	4	1	SKY COVER
2002	10	4	7	SKY COVER
2002	10	4	13	SKY COVER
2002	10	4	19	SKY COVER
2002	10	5	1	CEILING HT
2002	10	5	1	SKY COVER
2002	10	5	7	CEILING HT
2002	10	5	7	SKY COVER
2002	10	5	13	CEILING HT
2002	10	5	13	SKY COVER
2002	10	5	19	CEILING HT
2002	10	5	19	SKY COVER
2002	10	6	1	SKY COVER
2002	10	6	7	SKY COVER
2002	10	6	13	SKY COVER
2002	10	6	19	CEILING HT
2002	10	6	19	SKY COVER
2002	10	7	1	CEILING HT
2002	10	7	1	SKY COVER
2002	10	7	7	CEILING HT
2002	10	7	7	SKY COVER
2002	10	7	19	CEILING HT
2002	10	7	19	SKY COVER
2002	10	8	1	CEILING HT
2002	10	8	1	SKY COVER
2002	10	8	7	CEILING HT
2002	10	8	7	SKY COVER
2002	10	8	13	SKY COVER

2002	10	8	15	CEILING HT
2002	10	8	15	SKY COVER
2002	10	8	19	SKY COVER
2002	10	9	1	CEILING HT
2002	10	9	1	SKY COVER
2002	10	9	7	CEILING HT
2002	10	9	7	SKY COVER
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2002	10	9	19	SKY COVER
2002	10	10	1	CEILING HT
2002	10	10	1	SKY COVER
2002	10	10	7	CEILING HT
2002	10	10	7	SKY COVER
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2002	10	11	1	SKY COVER
2002	10	11	7	CEILING HT
2002	10	11	7	SKY COVER
2002	10	11	13	CEILING HT
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2002	10	11	19	CEILING HT
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2002	10	12	7	SKY COVER
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2002	10	12	19	CEILING HT
2002	10	12	19	SKY COVER
2002	10	13	1	CEILING HT
2002	10	13	1	SKY COVER
2002	10	13	7	CEILING HT
2002	10	13	7	SKY COVER
2002	10	13	13	CEILING HT
2002	10	13	13	SKY COVER
2002	10	13	19	CEILING HT
2002	10	13	19	SKY COVER
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2002	10	14	1	SKY COVER
2002	10	14	7	CEILING HT
2002	10	14	7	SKY COVER
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2002	10	14	19	CEILING HT
2002	10	14	19	SKY COVER
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2002	10	15	1	SKY COVER
2002	10	15	7	CEILING HT
2002	10	15	7	SKY COVER
2002	10	15	13	CEILING HT
2002	10	15	13	SKY COVER
2002	10	15	19	CEILING HT
2002	10	15	19	SKY COVER
2002	10	16	1	CEILING HT
2002	10	16	1	SKY COVER

2002	10	16	7	SKY COVER
2002	10	16	13	SKY COVER
2002	10	16	19	SKY COVER
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2002	10	17	1	SKY COVER
2002	10	17	7	CEILING HT
2002	10	17	7	SKY COVER
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2002	10	17	19	CEILING HT
2002	10	17	19	SKY COVER
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2002	10	18	1	SKY COVER
2002	10	18	7	CEILING HT
2002	10	18	7	SKY COVER
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2002	10	18	19	SKY COVER
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2002	10	19	1	SKY COVER
2002	10	19	7	CEILING HT
2002	10	19	7	SKY COVER
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2002	10	19	13	SKY COVER
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2002	10	20	1	SKY COVER
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2002	10	20	13	SKY COVER
2002	10	20	19	CEILING HT
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2002	10	21	1	SKY COVER
2002	10	21	7	SKY COVER
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2002	10	21	13	SKY COVER
2002	10	21	19	CEILING HT
2002	10	21	19	SKY COVER
2002	10	22	1	CEILING HT
2002	10	22	1	SKY COVER
2002	10	22	7	CEILING HT
2002	10	22	7	SKY COVER
2002	10	22	13	SKY COVER
2002	10	22	18	CEILING HT
2002	10	22	19	SKY COVER
2002	10	23	1	SKY COVER
2002	10	23	7	SKY COVER
2002	10	23	13	SKY COVER
2002	10	23	19	SKY COVER
2002	10	24	1	SKY COVER
2002	10	24	4	CEILING HT
2002	10	24	4	SKY COVER
2002	10	24	7	SKY COVER
2002	10	24	13	SKY COVER
2002	10	24	17	CEILING HT

2002	10	24	17	SKY COVER
2002	10	24	19	SKY COVER
2002	10	25	1	SKY COVER
2002	10	25	7	CEILING HT
2002	10	25	7	SKY COVER
2002	10	25	13	SKY COVER
2002	10	25	19	CEILING HT
2002	10	25	19	SKY COVER
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2002	10	26	1	SKY COVER
2002	10	26	19	CEILING HT
2002	10	26	19	SKY COVER
2002	10	27	1	CEILING HT
2002	10	27	1	SKY COVER
2002	10	27	7	CEILING HT
2002	10	27	7	SKY COVER
2002	10	27	13	CEILING HT
2002	10	27	13	SKY COVER
2002	10	27	19	CEILING HT
2002	10	27	19	SKY COVER
2002	10	28	1	CEILING HT
2002	10	28	1	SKY COVER
2002	10	28	7	CEILING HT
2002	10	28	7	SKY COVER
2002	10	28	13	CEILING HT
2002	10	28	13	SKY COVER
2002	10	28	19	CEILING HT
2002	10	28	19	SKY COVER
2002	10	29	1	SKY COVER
2002	10	29	7	SKY COVER
2002	10	29	14	CEILING HT
2002	10	29	14	SKY COVER
2002	10	30	1	SKY COVER
2002	10	30	7	SKY COVER
2002	10	30	13	SKY COVER
2002	10	30	19	SKY COVER
2002	10	31	1	SKY COVER
2002	10	31	7	SKY COVER
2002	10	31	13	SKY COVER
2002	10	31	19	SKY COVER
2002	11	1	1	SKY COVER
2002	11	1	7	SKY COVER
2002	11	1	13	SKY COVER
2002	11	1	19	CEILING HT
2002	11	1	19	SKY COVER
2002	11	2	1	CEILING HT
2002	11	2	1	SKY COVER
2002	11	2	7	SKY COVER
2002	11	2	13	SKY COVER
2002	11	2	19	CEILING HT
2002	11	2	19	SKY COVER
2002	11	3	1	CEILING HT
2002	11	3	1	SKY COVER
2002	11	3	7	CEILING HT
2002	11	3	7	SKY COVER
2002	11	3	13	CEILING HT
2002	11	3	13	SKY COVER
2002	11	3	19	CEILING HT
2002	11	3	19	SKY COVER

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2002	11	4	1	SKY COVER
2002	11	4	7	CEILING HT
2002	11	4	7	SKY COVER
2002	11	4	13	CEILING HT
2002	11	4	13	SKY COVER
2002	11	4	19	CEILING HT
2002	11	4	19	SKY COVER
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2002	11	5	1	SKY COVER
2002	11	5	7	CEILING HT
2002	11	5	7	SKY COVER
2002	11	5	13	CEILING HT
2002	11	5	13	SKY COVER
2002	11	5	19	CEILING HT
2002	11	5	19	SKY COVER
2002	11	6	1	CEILING HT
2002	11	6	1	SKY COVER
2002	11	6	7	CEILING HT
2002	11	6	7	SKY COVER
2002	11	6	13	CEILING HT
2002	11	6	13	SKY COVER
2002	11	6	19	CEILING HT
2002	11	6	19	SKY COVER
2002	11	7	1	CEILING HT
2002	11	7	1	SKY COVER
2002	11	7	7	CEILING HT
2002	11	7	7	SKY COVER
2002	11	7	13	CEILING HT
2002	11	7	13	SKY COVER
2002	11	7	19	CEILING HT
2002	11	7	19	SKY COVER
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2002	11	8	1	SKY COVER
2002	11	8	7	CEILING HT
2002	11	8	7	SKY COVER
2002	11	8	13	CEILING HT
2002	11	8	13	SKY COVER
2002	11	8	19	SKY COVER
2002	11	9	1	CEILING HT
2002	11	9	1	SKY COVER
2002	11	9	7	SKY COVER
2002	11	9	13	CEILING HT
2002	11	9	13	SKY COVER
2002	11	9	19	CEILING HT
2002	11	9	19	SKY COVER
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2002	11	10	1	SKY COVER
2002	11	10	7	CEILING HT
2002	11	10	7	SKY COVER
2002	11	10	13	CEILING HT
2002	11	10	13	SKY COVER
2002	11	10	19	CEILING HT
2002	11	10	19	SKY COVER
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2002	11	11	7	SKY COVER
2002	11	11	13	SKY COVER
2002	11	11	19	CEILING HT
2002	11	11	19	SKY COVER

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2002	11	12	1	SKY COVER
2002	11	12	7	CEILING HT
2002	11	12	7	SKY COVER
2002	11	12	13	CEILING HT
2002	11	12	13	SKY COVER
2002	11	12	19	CEILING HT
2002	11	12	19	SKY COVER
2002	11	13	1	CEILING HT
2002	11	13	1	SKY COVER
2002	11	13	7	SKY COVER
2002	11	13	13	CEILING HT
2002	11	13	13	SKY COVER
2002	11	13	19	CEILING HT
2002	11	13	19	SKY COVER
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2002	11	14	7	SKY COVER
2002	11	14	13	SKY COVER
2002	11	14	19	SKY COVER
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2002	11	15	1	SKY COVER
2002	11	15	7	SKY COVER
2002	11	15	13	SKY COVER
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2002	11	15	16	SKY COVER
2002	11	15	19	SKY COVER
2002	11	16	1	CEILING HT
2002	11	16	1	SKY COVER
2002	11	16	7	CEILING HT
2002	11	16	7	SKY COVER
2002	11	16	13	CEILING HT
2002	11	16	13	SKY COVER
2002	11	16	19	CEILING HT
2002	11	16	19	SKY COVER
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2002	11	17	1	SKY COVER
2002	11	17	7	CEILING HT
2002	11	17	7	SKY COVER
2002	11	17	13	CEILING HT
2002	11	17	13	SKY COVER
2002	11	17	19	CEILING HT
2002	11	17	19	SKY COVER
2002	11	18	1	SKY COVER
2002	11	18	7	CEILING HT
2002	11	18	7	SKY COVER
2002	11	18	13	CEILING HT
2002	11	18	13	SKY COVER
2002	11	18	19	CEILING HT
2002	11	18	19	SKY COVER
2002	11	19	1	CEILING HT
2002	11	19	1	SKY COVER
2002	11	19	7	CEILING HT
2002	11	19	7	SKY COVER
2002	11	19	13	CEILING HT
2002	11	19	13	SKY COVER
2002	11	19	19	CEILING HT
2002	11	19	19	SKY COVER
2002	11	20	1	CEILING HT
2002	11	20	1	SKY COVER

2002	11	20	7	CEILING HT
2002	11	20	7	SKY COVER
2002	11	20	13	CEILING HT
2002	11	20	13	SKY COVER
2002	11	20	19	CEILING HT
2002	11	20	19	SKY COVER
2002	11	21	1	CEILING HT
2002	11	21	1	SKY COVER
2002	11	21	7	CEILING HT
2002	11	21	7	SKY COVER
2002	11	21	13	CEILING HT
2002	11	21	13	SKY COVER
2002	11	21	19	CEILING HT
2002	11	21	19	SKY COVER
2002	11	22	1	CEILING HT
2002	11	22	1	SKY COVER
2002	11	22	7	CEILING HT
2002	11	22	7	SKY COVER
2002	11	22	13	CEILING HT
2002	11	22	13	SKY COVER
2002	11	22	19	CEILING HT
2002	11	22	19	SKY COVER
2002	11	23	1	CEILING HT
2002	11	23	1	SKY COVER
2002	11	23	7	SKY COVER
2002	11	23	13	SKY COVER
2002	11	23	19	SKY COVER
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2002	11	24	7	SKY COVER
2002	11	24	13	SKY COVER
2002	11	24	19	SKY COVER
2002	11	24	23	CEILING HT
2002	11	24	23	SKY COVER
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2002	11	25	7	SKY COVER
2002	11	25	13	SKY COVER
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2002	11	25	19	SKY COVER
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2002	11	26	1	SKY COVER
2002	11	26	7	CEILING HT
2002	11	26	7	SKY COVER
2002	11	26	13	CEILING HT
2002	11	26	13	SKY COVER
2002	11	26	19	CEILING HT
2002	11	26	19	SKY COVER
2002	11	27	1	CEILING HT
2002	11	27	1	SKY COVER
2002	11	27	7	SKY COVER
2002	11	27	13	CEILING HT
2002	11	27	13	SKY COVER
2002	11	27	19	SKY COVER
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2002	11	28	1	SKY COVER
2002	11	28	7	CEILING HT
2002	11	28	7	SKY COVER
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2002	11	28	13	SKY COVER
2002	11	28	19	CEILING HT

2002	11	28	19	SKY COVER
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2002	11	29	1	SKY COVER
2002	11	29	7	CEILING HT
2002	11	29	7	SKY COVER
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2002	11	30	1	SKY COVER
2002	11	30	13	CEILING HT
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2002	11	30	19	SKY COVER
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2002	12	1	1	SKY COVER
2002	12	1	7	CEILING HT
2002	12	1	7	SKY COVER
2002	12	1	13	CEILING HT
2002	12	1	13	SKY COVER
2002	12	1	19	CEILING HT
2002	12	1	19	SKY COVER
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2002	12	2	1	SKY COVER
2002	12	2	7	CEILING HT
2002	12	2	7	SKY COVER
2002	12	2	13	CEILING HT
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2002	12	3	19	SKY COVER
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2002	12	4	7	SKY COVER
2002	12	4	13	SKY COVER
2002	12	4	19	SKY COVER
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2002	12	5	2	SKY COVER
2002	12	5	7	SKY COVER
2002	12	5	13	SKY COVER
2002	12	5	19	CEILING HT
2002	12	5	19	SKY COVER
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2002	12	6	1	SKY COVER
2002	12	6	7	CEILING HT
2002	12	6	7	SKY COVER
2002	12	6	13	CEILING HT
2002	12	6	13	SKY COVER
2002	12	6	19	CEILING HT
2002	12	6	19	SKY COVER
2002	12	7	1	CEILING HT
2002	12	7	1	SKY COVER
2002	12	7	7	CEILING HT
2002	12	7	7	SKY COVER
2002	12	7	13	CEILING HT

2002	12	7	13	SKY COVER
2002	12	7	19	CEILING HT
2002	12	7	19	SKY COVER
2002	12	8	1	CEILING HT
2002	12	8	1	SKY COVER
2002	12	8	7	CEILING HT
2002	12	8	7	SKY COVER
2002	12	8	13	CEILING HT
2002	12	8	13	SKY COVER
2002	12	8	19	CEILING HT
2002	12	8	19	SKY COVER
2002	12	9	1	CEILING HT
2002	12	9	1	SKY COVER
2002	12	9	7	CEILING HT
2002	12	9	7	SKY COVER
2002	12	9	13	CEILING HT
2002	12	9	13	SKY COVER
2002	12	9	19	CEILING HT
2002	12	9	19	SKY COVER
2002	12	10	1	CEILING HT
2002	12	10	1	SKY COVER
2002	12	10	7	CEILING HT
2002	12	10	7	SKY COVER
2002	12	10	13	CEILING HT
2002	12	10	13	SKY COVER
2002	12	10	19	CEILING HT
2002	12	10	19	SKY COVER
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2002	12	11	1	SKY COVER
2002	12	11	7	CEILING HT
2002	12	11	7	SKY COVER
2002	12	11	13	CEILING HT
2002	12	11	13	SKY COVER
2002	12	11	19	CEILING HT
2002	12	11	19	SKY COVER
2002	12	12	1	SKY COVER
2002	12	12	7	CEILING HT
2002	12	12	7	SKY COVER
2002	12	12	13	CEILING HT
2002	12	12	13	SKY COVER
2002	12	12	19	CEILING HT
2002	12	12	19	SKY COVER
2002	12	13	1	SKY COVER
2002	12	13	7	CEILING HT
2002	12	13	7	SKY COVER
2002	12	13	13	CEILING HT
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2002	12	14	1	SKY COVER
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2002	12	14	7	SKY COVER
2002	12	14	13	CEILING HT
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2002	12	14	19	CEILING HT
2002	12	14	19	SKY COVER
2002	12	15	1	CEILING HT
2002	12	15	1	SKY COVER
2002	12	15	7	CEILING HT
2002	12	15	7	SKY COVER

2002	12	15	13	CEILING HT
2002	12	15	13	SKY COVER
2002	12	15	19	CEILING HT
2002	12	15	19	SKY COVER
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2002	12	16	1	SKY COVER
2002	12	16	7	CEILING HT
2002	12	16	7	SKY COVER
2002	12	16	13	CEILING HT
2002	12	16	13	SKY COVER
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2002	12	17	1	SKY COVER
2002	12	17	7	SKY COVER
2002	12	17	13	SKY COVER
2002	12	17	19	CEILING HT
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2002	12	18	7	SKY COVER
2002	12	18	19	SKY COVER
2002	12	19	1	SKY COVER
2002	12	19	7	CEILING HT
2002	12	19	7	SKY COVER
2002	12	19	13	CEILING HT
2002	12	19	13	SKY COVER
2002	12	20	1	CEILING HT
2002	12	20	1	SKY COVER
2002	12	20	7	CEILING HT
2002	12	20	7	SKY COVER
2002	12	20	13	CEILING HT
2002	12	20	13	SKY COVER
2002	12	20	19	CEILING HT
2002	12	20	19	SKY COVER
2002	12	21	1	SKY COVER
2002	12	21	7	SKY COVER
2002	12	21	13	SKY COVER
2002	12	21	19	CEILING HT
2002	12	21	19	SKY COVER
2002	12	22	1	SKY COVER
2002	12	22	7	SKY COVER
2002	12	22	13	SKY COVER
2002	12	22	19	CEILING HT
2002	12	22	19	SKY COVER
2002	12	23	1	CEILING HT
2002	12	23	1	SKY COVER
2002	12	23	7	CEILING HT
2002	12	23	7	SKY COVER
2002	12	23	13	CEILING HT
2002	12	23	13	SKY COVER
2002	12	23	19	CEILING HT
2002	12	23	19	SKY COVER
2002	12	24	1	SKY COVER
2002	12	24	7	CEILING HT
2002	12	24	7	SKY COVER
2002	12	24	13	SKY COVER
2002	12	24	19	CEILING HT
2002	12	24	19	SKY COVER
2002	12	25	1	CEILING HT

2002	12	25	1	SKY COVER
2002	12	25	7	CEILING HT
2002	12	25	7	SKY COVER
2002	12	25	13	CEILING HT
2002	12	25	13	SKY COVER
2002	12	25	19	CEILING HT
2002	12	25	19	SKY COVER
2002	12	26	1	CEILING HT
2002	12	26	1	SKY COVER
2002	12	26	7	CEILING HT
2002	12	26	7	SKY COVER
2002	12	26	13	CEILING HT
2002	12	26	13	SKY COVER
2002	12	26	19	CEILING HT
2002	12	26	19	SKY COVER
2002	12	27	1	CEILING HT
2002	12	27	1	SKY COVER
2002	12	27	7	CEILING HT
2002	12	27	7	SKY COVER
2002	12	27	13	CEILING HT
2002	12	27	13	SKY COVER
2002	12	27	19	CEILING HT
2002	12	27	19	SKY COVER
2002	12	28	1	CEILING HT
2002	12	28	1	SKY COVER
2002	12	28	7	CEILING HT
2002	12	28	7	SKY COVER
2002	12	28	13	CEILING HT
2002	12	28	13	SKY COVER
2002	12	28	19	CEILING HT
2002	12	28	19	SKY COVER
2002	12	29	1	CEILING HT
2002	12	29	1	SKY COVER
2002	12	29	7	CEILING HT
2002	12	29	7	SKY COVER
2002	12	29	13	CEILING HT
2002	12	29	13	SKY COVER
2002	12	29	19	CEILING HT
2002	12	29	19	SKY COVER
2002	12	30	1	CEILING HT
2002	12	30	1	SKY COVER
2002	12	30	7	CEILING HT
2002	12	30	7	SKY COVER
2002	12	30	13	CEILING HT
2002	12	30	13	SKY COVER
2002	12	30	19	CEILING HT
2002	12	30	19	SKY COVER
2002	12	31	1	CEILING HT
2002	12	31	1	SKY COVER
2002	12	31	7	CEILING HT
2002	12	31	7	SKY COVER
2002	12	31	13	SKY COVER
2002	12	31	19	SKY COVER

Table B-2. Filled Onsite Meteorological Data

<u>Year</u>	<u>Month</u>	<u>Day</u>	<u>Hour</u>	<u>Temperature Filled Deg. C</u>	<u>Wind Speed Filled m/s</u>	<u>Wind Direction Filled Degrees</u>
2000	4	26	900	N/A	5.9295	322
2000	4	26	1000	11.195	5.9295	322
2000	6	25	600	14.21	5.132	336
2000	6	25	700	13.81	4.5665	320
2000	6	25	1100	15.015	3.2345	4
2000	6	27	2300	10.635	1.2	28
2000	6	27	2400	10.635	1.2	18
2000	6	28	100	10.635	1.2	8
2000	6	28	200	10.635	1.2	358
2000	6	28	300	10.635	1.2	348
2000	6	28	400	10.635	1.2	338
2000	6	28	500	10.635	1.2	328
2000	6	28	600	10.635	1.2	318
2000	6	30	400	10	1.4	35
2000	6	30	500	11	1.4	355
2000	6	30	600	12	1.4	315
2000	7	1	100	12.72	1.2	285
2000	7	1	200	11.51	1.2	282
2000	7	1	300	10.36	1.2	279
2000	7	1	400	9.64	1.2	276
2000	7	1	500	8.48	1.2	273
2000	7	1	600	10.25	1.2	270
2000	7	1	900	25.445	7.651	236
2000	7	1	2300	18.33	1.2	311
2000	7	1	2400	18.33	1.2	325
2000	7	2	100	18.33	1.2	338
2000	7	2	200	18.33	1.2	352
2000	7	2	300	18.33	1.2	5
2000	7	2	400	18.33	1.2	19
2000	7	2	500	18.33	1.2	32
2000	7	2	600	18.33	1.2	46
2000	7	2	2000	25.02	3.012	179
2000	7	2	2100	26.09	4.627	186
2000	7	2	2200	21.35	1.824	193
2000	7	2	2300	19.3	1.6	199
2000	7	2	2400	18.49	1.6	206
2000	7	3	100	18.32	1.6	212
2000	7	3	200	17.45	1.6	219
2000	7	3	300	17.06	1.6	226
2000	7	3	400	15.25	1.6	232
2000	7	3	500	15.215	1.6	239
2000	7	3	600	15.18	1.6	245
2000	7	3	700	17.35	2.655	252
2000	7	4	500	15.215	2.1925	292
2000	7	5	100	12.31	3.482	293
2000	7	5	300	13.165	1.6	293

2000	7	5	400	13.165	1.6	288
2000	7	5	500	13.165	1.6	283
2000	7	5	600	13.165	1.6	278
2000	7	5	2100	24.955	4.627	155
2000	7	5	2200	21.88	1.824	163
2000	7	5	2300	20.65	2.258	170
2000	7	5	2400	20.445	2.771	178
2000	7	6	100	20.02	1.76	185
2000	7	6	200	19.33	3.443	192
2000	7	6	300	19.155	3.074	200
2000	7	6	400	18.245	1.816	207
2000	7	6	500	17.5575	1.752	215
2000	7	6	600	17.525	1.617	222
2000	7	6	700	19.19	2.655	229
2000	7	6	800	20.505	2.742	237
2000	7	6	2100	24.955	4.627	257
2000	7	6	2200	21.88	1.824	261
2000	7	6	2300	20.65	2.258	265
2000	7	6	2400	20.445	2.771	269
2000	7	7	100	20.02	1.76	273
2000	7	7	200	19.33	3.443	277
2000	7	7	300	19.155	3.074	281
2000	7	7	400	18.245	1.816	285
2000	7	7	500	17.5575	1.752	289
2000	7	7	600	17.525	1.617	293
2000	7	7	2000	24.77	3.012	134
2000	7	7	2100	23.82	4.627	146
2000	7	7	2200	22.41	1.824	158
2000	7	7	2300	22	2.258	170
2000	7	7	2400	22.4	2.771	182
2000	7	8	100	21.72	1.76	194
2000	7	8	200	21.21	3.443	206
2000	7	8	300	21.25	3.074	218
2000	7	8	400	21.24	1.816	230
2000	7	8	500	19.9	1.752	242
2000	7	8	600	19.87	1.617	254
2000	7	8	700	21.03	2.655	266
2000	7	9	2100	21.525	4.372	256
2000	7	9	2200	20.115	2.131	274
2000	7	9	2300	19.43	1.356	292
2000	7	9	2400	18.83	1.706	310
2000	7	10	100	17.795	2.251	328
2000	7	10	200	16.9	2.275	346
2000	7	10	300	16.61	1.518	4
2000	7	10	400	15.68	2.447	22
2000	7	10	500	14.98	1.752	40
2000	7	10	600	15.14	1.617	58
2000	7	10	700	17.535	3.045	76
2000	7	11	300	12.6	1.6	278
2000	7	11	400	12.6	1.6	281
2000	7	11	500	12.6	1.6	283
2000	7	11	600	12.6	1.6	286

2000	7	12	2100	23.82	1.4	131
2000	7	12	2200	22.41	1.4	137
2000	7	12	2300	22	1.4	144
2000	7	12	2400	22.4	1.4	150
2000	7	13	100	21.72	1.4	157
2000	7	13	200	21.21	1.4	163
2000	7	13	300	21.25	1.4	170
2000	7	13	400	21.24	1.4	176
2000	7	13	500	19.9	1.4	183
2000	7	13	600	19.87	1.4	189
2000	7	13	700	21.03	1.4	196
2000	7	13	800	22.74	1.4	202
2000	7	13	2000	24.77	1.4	119
2000	7	13	2100	23.82	1.4	128
2000	7	13	2200	22.41	1.4	137
2000	7	13	2300	22	1.4	147
2000	7	13	2400	22.4	1.4	156
2000	7	14	100	21.72	1.4	166
2000	7	14	200	21.21	1.4	175
2000	7	14	300	21.25	1.4	184
2000	7	14	400	21.24	1.4	194
2000	7	14	500	19.9	1.4	203
2000	7	14	600	19.87	1.4	213
2000	7	14	700	21.03	1.4	222
2000	7	14	800	22.74	1.4	231
2000	7	14	1900	26.52	1.6	347
2000	7	14	2000	24.77	1.6	344
2000	7	14	2100	23.82	1.6	341
2000	7	14	2200	22.41	1.6	338
2000	7	14	2300	22	1.6	335
2000	7	14	2400	22.4	1.6	332
2000	7	15	100	21.72	1.6	329
2000	7	15	200	21.21	1.6	326
2000	7	15	300	21.25	1.6	322
2000	7	15	400	21.24	1.6	319
2000	7	15	500	19.9	1.6	316
2000	7	15	600	19.87	1.6	313
2000	7	15	700	21.03	1.6	310
2000	7	15	800	22.74	1.6	307
2000	7	15	900	23.69	1.6	304
2000	7	15	1000	25.06	1.6	301
2000	7	15	1700	29.075	1.4	300
2000	7	15	1800	27.885	1.4	309
2000	7	15	1900	24.47	1.4	319
2000	7	15	2000	21.63	1.4	328
2000	7	15	2100	19.36	1.4	337
2000	7	15	2200	18.18	1.4	347
2000	7	15	2300	17.185	1.4	356
2000	7	15	2400	15.86	1.4	5
2000	7	16	100	14.195	1.4	14
2000	7	16	200	12.805	1.4	24
2000	7	16	300	16.61	1.4	33

2000	7	16	400	15.68	1.4	42
2000	7	16	500	14.98	1.4	52
2000	7	16	600	15.14	1.4	61
2000	7	16	700	17.335	4.475	70
2000	7	16	800	20.02	3.437	80
2000	7	16	900	21	5.938	89
2000	7	16	1000	22	6.369	98
2000	7	16	1100	22.7	5.251	107
2000	7	16	1900	24.47	5.334	130
2000	7	16	2000	21.63	2.537	127
2000	7	16	2100	19.36	3.739	123
2000	7	16	2200	18.18	2.621	120
2000	7	16	2300	17.185	1.356	116
2000	7	16	2400	15.86	1.706	113
2000	7	17	100	14.195	1.17	109
2000	7	17	200	12.805	1.503	106
2000	7	17	300	16.61	1.518	102
2000	7	17	400	15.68	2.447	99
2000	7	17	500	14.98	1.752	95
2000	7	17	600	15.14	1.617	92
2000	7	17	700	17.335	4.475	88
2000	7	17	2300	16	1.4	246
2000	7	17	2400	15.86	1.4	252
2000	7	18	100	14.195	1.4	258
2000	7	18	200	12.805	1.4	265
2000	7	18	300	16.61	1.4	271
2000	7	18	400	15.68	1.4	277
2000	7	18	500	14.98	1.4	283
2000	7	18	600	15.14	1.4	289
2000	7	18	700	17.335	1.4	296
2000	7	18	800	20.02	1.4	302
2000	7	18	2100	17.7	1.6	108
2000	7	18	2200	17.5	1.6	93
2000	7	18	2300	17.185	1.6	78
2000	7	18	2400	15.86	1.6	63
2000	7	19	100	14.195	1.6	48
2000	7	19	200	12.805	1.6	33
2000	7	19	300	16.61	1.6	18
2000	7	19	400	15.68	1.6	3
2000	7	19	500	14.98	1.6	348
2000	7	19	600	15.14	1.6	333
2000	7	19	700	17.335	1.6	318
2000	11	13	900	N/A	N/A	287
2000	11	13	1000	-10.2635	N/A	287
2000	11	13	1100	-10.2635	N/A	N/A
2001	3	16	100	-4.564	0.433	304
2001	3	16	200	-5.074	0.637	324
2001	3	16	300	-6.016	0.981	298
2001	3	16	400	-6.11	1.64	280
2001	3	16	500	-6.57	1.24	292
2001	3	16	600	-6.408	0.66	287
2001	3	16	700	-5.94	1.214	277

2001	3	16	800	-0.154	3.699	280
2001	3	16	900	2.289	4.211	285
2001	3	16	1000	3.738	5.26	315
2001	3	16	1100	3.989	4.258	321
2001	3	16	1200	5.569	3.611	291
2001	3	16	1300	7.08	4.068	288
2001	3	16	1400	7.34	3.387	338
2001	3	16	1500	7.73	4.353	299
2001	3	16	1600	6.895	2.16	18
2001	3	16	1700	7	2.896	336
2001	3	16	1800	5.636	3.196	12
2001	3	16	1900	2.209	2.034	358
2001	3	16	2000	0.479	0.912	267
2001	3	16	2100	-1.156	0.928	280
2001	3	16	2200	-2.562	1.002	287
2001	3	16	2300	-3.263	0.667	253
2001	3	16	2400	-4.088	0.583	270
2001	3	17	100	-4.564	0.433	291
2001	3	17	200	-5.074	0.637	312
2001	3	17	300	-6.016	0.981	334
2001	3	17	400	-6.11	1.64	355
2001	3	17	500	-6.57	1.24	17
2001	3	17	600	-6.408	0.66	38
2001	3	17	700	-5.94	1.214	59
2001	5	22	900	12.19	7.3545	320
2001	11	7	1000	5.3395	3.416	319
2002	4	24	900	0.536	5.135	285
2002	11	5	1400	7.9	10.395	274

Table B-3. Filled Mixing Height Data

<u>Year</u>	<u>Month</u>	<u>Day</u>	<u>AM Mixing</u>	<u>PM Mixing</u>
1998	1	3	349	847
1998	1	9	303	N/A
1998	1	10	188	608
1998	1	11	N/A	465
1998	1	12	200	N/A
1998	1	16	208	N/A
1998	1	20	N/A	508
1998	3	7	522	N/A
1998	4	22	393	N/A
1998	4	23	225	N/A
1998	4	25	120	N/A
1998	4	26	120	N/A
1998	4	27	120	N/A
1998	4	29	N/A	3530
1998	5	1	57	3308
1998	5	2	57	3308
1998	5	3	57	3308
1998	5	4	57	3308
1998	5	5	57	3308
1998	5	6	384	3218
1998	5	7	384	3218
1998	5	8	384	3218
1998	5	9	384	3218
1998	5	10	384	3218
1998	5	19	N/A	3590
1998	5	22	N/A	3620
1998	5	24	866	N/A
1998	5	26	58	3734
1998	5	28	546	N/A
1998	5	29	546	3758
1998	5	30	1179	2721
1998	5	31	1179	1684
1998	6	2	1450	N/A
1998	6	6	912	1439
1998	6	7	912	1439
1998	6	8	586	1701
1998	6	9	260	1964
1998	6	10	260	1964
1998	6	15	1687	2327
1998	6	19	514	2234
1998	6	20	408	2234
1998	6	21	302	3218
1998	6	22	196	3218
1998	6	26	312	N/A
1998	6	29	95	2842
1998	7	1	N/A	2276
1998	7	6	156	3920
1998	7	9	N/A	3615

1998	7	10	N/A	3615
1998	7	11	N/A	4547
1998	7	12	377	4547
1998	7	14	N/A	4547
1998	7	16	22	4104
1998	7	19	16	4188
1998	7	22	113	N/A
1998	8	6	59	N/A
1998	8	10	90	N/A
1998	8	22	N/A	3208
1998	8	23	176	2965
1998	9	4	55	N/A
1998	9	5	88	N/A
1998	9	8	232	N/A
1998	9	16	16	N/A
1998	9	29	42	N/A
1998	10	9	132	N/A
1998	10	10	181	N/A
1998	10	13	181	N/A
1998	10	14	454	N/A
1998	10	15	727	N/A
1998	10	16	N/A	1870
1998	10	17	N/A	1108
1998	12	15	236	N/A
1998	12	18	N/A	598
1998	12	19	N/A	359
1998	12	20	562	N/A
1998	12	23	578	N/A
1998	12	29	508	N/A
2000	1	4	644	N/A
2000	1	9	337	N/A
2000	1	10	213	1416
2000	1	14	358	1270
2000	1	23	256	N/A
2000	2	4	386	N/A
2000	2	12	N/A	1154
2000	2	27	162	1892
2000	3	2	62	N/A
2000	3	28	836	N/A
2000	4	5	252	N/A
2000	4	6	371	N/A
2000	4	9	80	N/A
2000	4	15	N/A	1439
2000	4	18	88	1883
2000	4	19	59	N/A
2000	4	27	39	N/A
2000	4	29	N/A	3412
2000	4	30	126	N/A
2000	5	2	70	N/A
2000	5	3	22	N/A
2000	5	5	N/A	3317
2000	5	6	549	N/A

2000	5	16	746	N/A
2000	5	17	N/A	2471
2000	5	23	398	N/A
2000	5	28	36	N/A
2000	6	3	N/A	2954
2000	6	5	580	N/A
2000	6	6	N/A	2563
2000	6	7	N/A	2563
2000	6	8	N/A	3313
2000	6	10	N/A	3688
2000	6	11	N/A	3056
2000	6	12	73	N/A
2000	6	15	N/A	2595
2000	6	17	N/A	3268
2000	6	21	1340	N/A
2000	6	22	17	N/A
2000	6	29	18	N/A
2000	7	2	N/A	3926
2000	7	3	N/A	3926
2000	7	4	N/A	4707
2000	7	5	32	4707
2000	7	7	N/A	4814
2000	7	9	N/A	4384
2000	7	11	N/A	4182
2000	7	12	216	N/A
2000	7	13	216	4432
2000	7	14	110	N/A
2000	7	15	110	N/A
2000	7	18	N/A	2005
2000	7	19	115	3141
2000	7	20	60	4277
2000	7	22	23	N/A
2000	7	23	23	4447
2000	7	24	23	N/A
2000	7	25	23	4525
2000	7	26	N/A	4416
2000	7	27	N/A	4308
2000	7	28	27	N/A
2000	7	29	27	N/A
2000	7	30	27	4778
2000	8	1	N/A	5072
2000	8	2	20	4107
2000	8	3	90	N/A
2000	8	6	N/A	4300
2000	8	7	N/A	4373
2000	8	8	8	N/A
2000	8	9	91	4445
2000	8	10	91	4170
2000	8	11	N/A	3895
2000	8	13	N/A	3954
2000	8	15	118	N/A
2000	8	17	114	N/A

2000	8	19	N/A	2513
2000	8	20	N/A	3191
2000	8	21	N/A	3870
2000	8	23	N/A	3957
2000	8	24	54	N/A
2000	8	29	354	N/A
2000	9	3	390	3846
2000	9	4	N/A	3879
2000	9	5	28	3913
2000	9	11	94	N/A
2000	9	14	33	3097
2000	9	15	22	N/A
2000	9	17	108	N/A
2000	9	19	N/A	3036
2000	10	1	31	N/A
2000	10	2	178	N/A
2000	10	7	829	N/A
2000	10	8	467	N/A
2000	10	9	105	2105
2000	10	11	210	N/A
2000	10	24	1149	1254
2000	10	31	N/A	1564
2000	11	5	N/A	480
2000	11	9	N/A	554
2000	11	11	634	N/A
2000	11	13	396	474
2000	11	14	396	474
2000	11	16	762	N/A
2000	12	2	178	500
2000	12	10	N/A	690
2000	12	11	222	N/A
2000	12	13	384	647
2000	12	16	496	N/A
2000	12	20	174	384
2000	12	21	340	N/A
2001	1	27	300	N/A
2001	2	7	N/A	306
2001	2	8	347	N/A
2001	2	14	472	N/A
2001	3	20	44	N/A
2001	3	23	320	N/A
2001	4	2	376	N/A
2001	4	7	1608	1302
2001	4	15	304	N/A
2001	4	19	684	N/A
2001	4	23	365	2002
2001	4	26	22	N/A
2001	4	28	364	N/A
2001	5	1	1408	N/A
2001	5	7	472	N/A
2001	5	8	352	2543
2001	5	9	232	3369

2001	5	11	67	N/A
2001	5	13	N/A	3495
2001	5	14	N/A	3209
2001	5	15	N/A	2924
2001	5	19	N/A	2672
2001	5	20	130	3354
2001	5	23	21	N/A
2001	5	24	150	N/A
2001	5	25	279	3506
2001	5	29	N/A	2439
2001	5	31	228	N/A
2001	6	2	364	N/A
2001	6	6	49	N/A
2001	6	8	28	N/A
2001	6	9	N/A	3934
2001	6	10	N/A	4075
2001	6	11	N/A	4215
2001	6	12	836	N/A
2001	6	16	N/A	4041
2001	6	17	N/A	1961
2001	6	20	917	N/A
2001	6	21	12	N/A
2001	6	22	N/A	3973
2001	6	23	N/A	3973
2001	6	25	45	3966
2001	6	26	158	N/A
2001	7	1	N/A	3633
2001	7	2	N/A	4451
2001	7	3	16	N/A
2001	7	4	16	N/A
2001	7	5	N/A	4211
2001	7	6	59	N/A
2001	7	7	89	N/A
2001	7	8	N/A	3660
2001	7	16	N/A	3089
2001	7	17	N/A	3089
2001	7	18	N/A	3089
2001	7	19	7	3310
2001	7	20	N/A	3310
2001	7	21	N/A	3310
2001	7	22	60	3532
2001	7	23	N/A	3532
2001	7	24	N/A	3532
2001	7	27	134	2696
2001	7	30	N/A	4694
2001	8	1	559	4568
2001	8	2	N/A	4090
2001	8	3	N/A	3612
2001	8	5	N/A	3708
2001	8	8	N/A	2660
2001	8	10	N/A	2358
2001	8	11	N/A	2968

2001	8	12	N/A	3579
2001	8	13	408	N/A
2001	8	17	N/A	4106
2001	8	18	104	N/A
2001	8	19	187	N/A
2001	8	25	36	N/A
2001	8	28	N/A	3271
2001	8	29	18	N/A
2001	9	3	79	N/A
2001	9	4	107	4176
2001	9	12	79	N/A
2001	9	21	21	N/A
2001	9	22	10	N/A
2001	9	24	7	N/A
2001	9	25	29	3648
2001	9	26	29	N/A
2001	9	27	29	N/A
2001	10	1	17	N/A
2001	10	3	122	N/A
2001	10	4	N/A	1337
2001	10	8	392	N/A
2001	10	19	117	N/A
2001	10	20	117	N/A
2001	10	21	117	N/A
2001	10	23	N/A	2468
2001	11	7	N/A	2063
2001	11	18	162	1273
2001	11	24	930	N/A
2001	11	26	N/A	448
2001	11	27	418	N/A
2001	12	18	N/A	729
2001	12	30	197	N/A
2002	1	9	N/A	690
2002	1	24	136	N/A
2002	2	12	270	577
2002	3	2	357	N/A
2002	3	3	357	N/A
2002	3	6	113	N/A
2002	3	7	56	N/A
2002	3	8	N/A	1861
2002	3	16	63	N/A
2002	3	17	123	N/A
2002	3	20	N/A	996
2002	3	24	N/A	632
2002	4	4	247	N/A
2002	4	5	180	N/A
2002	4	6	N/A	2816
2002	4	9	763	N/A
2002	4	17	N/A	2067
2002	4	22	N/A	2860
2002	5	1	N/A	3030
2002	5	4	N/A	2912

2002	5	5	N/A	2376
2002	5	14	73	N/A
2002	5	20	90	N/A
2002	5	21	894	N/A
2002	5	23	1168	3098
2002	5	25	312	N/A
2002	5	27	9	N/A
2002	5	28	N/A	3786
2002	5	31	73	N/A
2002	6	1	102	N/A
2002	6	5	N/A	2251
2002	6	6	N/A	1331
2002	6	7	170	N/A
2002	6	8	N/A	1558
2002	6	14	0	N/A
2002	6	15	0	N/A
2002	6	16	N/A	0
2002	6	17	0	0
2002	6	18	0	0
2002	6	19	0	0
2002	6	20	N/A	0
2002	6	23	N/A	0
2002	6	24	N/A	0
2002	6	25	0	0
2002	6	26	0	0
2002	6	27	0	N/A
2002	6	28	N/A	0
2002	6	29	N/A	0
2002	6	30	98	0
2002	7	3	774	N/A
2002	7	4	N/A	4196
2002	7	8	N/A	2832
2002	7	10	0	N/A
2002	7	11	0	N/A
2002	7	12	0	N/A
2002	7	13	0	N/A
2002	7	14	0	0
2002	7	15	0	0
2002	7	16	0	0
2002	7	24	N/A	1792
2002	7	25	203	N/A
2002	7	29	N/A	3985
2002	7	30	26	N/A
2002	7	31	N/A	3068
2002	8	4	N/A	3176
2002	8	8	162	N/A
2002	8	14	106	N/A
2002	8	18	0	N/A
2002	8	19	0	N/A
2002	8	21	N/A	4420
2002	8	23	194	N/A
2002	8	25	182	0

2002	8	26	N/A	0
2002	8	30	N/A	0
2002	8	31	N/A	0
2002	9	1	0	0
2002	9	2	0	0
2002	9	3	0	0
2002	9	5	N/A	4204
2002	9	6	421	N/A
2002	9	14	0	N/A
2002	9	15	0	N/A
2002	9	23	0	N/A
2002	9	24	0	N/A
2002	9	26	0	N/A
2002	9	27	0	N/A
2002	10	1	N/A	2198
2002	10	8	5	N/A
2002	10	10	0	N/A
2002	10	11	0	3036
2002	10	13	0	N/A
2002	10	14	0	N/A
2002	10	15	0	N/A
2002	10	18	27	N/A
2002	10	20	21	N/A
2002	10	22	378	1337
2002	10	26	36	N/A
2002	10	29	N/A	606
2002	11	19	115	N/A
2002	11	24	0	0
2002	11	25	0	0
2002	11	26	0	N/A
2002	12	23	106	N/A